

SOCIJALISTIČKA FEDERATIVNA REPUBLIKA JUGOSLAVIJA — RÉPUBLIQUE SOCIALISTE FÉDÉRATIVE DE YOUGOSLAVIE
HIDROMETEOROLŠKA SLUŽBA — SERVICE HYDRO-MÉTÉOROLOGIQUE

METEOROLOŠKI GODIŠNJAK I

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O B J A Š N J E N J A

Meteorološki godišnjak I ima dva dela: A) Dnevna osmatranja i B) Mesečni i godišnji pregled. U delu A) objavljuju se podaci 10 odabranih stanica, i to: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Novi Sad-Rimski Šančevi, Priština, Titograd i Skopje-Petrovac. u delu B) nalaze se podaci svih meteoroloških stanica osnovnih mreža.

Značenje upotrebljenih oznaka je sledeće:

φ = geografska širina, λ = geografska dužina od Griniča, ΔG = vremenska razlika u odnosu na Grinič, H_g = nadmorska visina podnožja termometarskog zaklona, H_b = nadmorska visina rezervoara barometra, h_t = visina rezervoara termometra iznad tla, h_r = visina otvora kišomera iznad tla.

Oznake pojedinih elemenata su upotrebljene prema međunarodnim konvencijama, a vrednosti su date u ovim jedinicama:

P = vazdušni pritisak u hPa na nivou stanice; T = temperatura u °C; e = pritisak vodene pare u hPa; U = relativna vlažnost u procentima; D = pravac vetra po ruži vetra od 16 do 8 pravaca; F = jačina vetra po Boforovoj skali (0-12); v = brzina vetra u m/s; V = vidljivost u km; N = oblačnost (0-10); insolacija = trajanje osunčavanja u satima; R = padavine u mm; h_s = snežni pokrivač u cm; W = razvoj vremena (vrsta pojave, intenzitet i trajanje) opisan međunarodnim simbolima.

U rubrici "razvoj vremena" su upotrebljene ove skraćenice:

n = u toku noći; rj = rano jutro; dp = do podne; pp = po podne; kv = kasno veče; i = s prekidima.

Srednje dnevne i mesečne vrednosti temperature vazduha izmerene u 7, 14, i 21 h po lokalnom vremenu računane su po formuli:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

a za ostale elemente (P, e, U, N) srednje dnevne i mesečne vrednosti dobijene su kao proste aritmetičke sredine terminskih vrednosti.

Ekstremni termometri su očitavani i uređivani u 21 h i vrednosti ubeležavane na dan merenja.

Dnevne vrednosti padavina se odnose na protekla 24 sata, od 7 h prethodnog dana do 7 h dana merenja u koji su zabeležene.

Visina snežnog pokrivača je merena u 7 h.

U tablicama A podvučene su vrednosti maksimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare, jačine vetra kad ona iznosi najmanje 6 po Boforu, i padavina, kao i vrednosti minimuma vazdušnog pritiska, temperature vazduha, pritiska vodene pare i relativne vlažnosti.

U tablicama B za srednje mesečne ekstremne temperature vazduha upotrebljene su oznake \overline{Max} i \overline{Min} ; za rubrike broj dana sa \bullet ili \circ , \ast ili Δ i \ast prebrojani su samo dani kad je visina naznačenih padavina iznosila najmanje 0.1 mm.

Broj stanica (kolona 2 Azbučnog spiska) je ustvari redni broj niza stanica sa podacima u tablicama dela B).

Na kraju knjige nalazi se karta SFRJ sa naznačenim klimatološkim stanicama u 1985. godini čiji brojevi odgovaraju brojevima stanica sa podacima u tablicama B.

NOTICE EXPLICATIVE

L'Annuaire météorologique I a deux parties: A) Observations journalières et: B) Résumés mensuels et annuels. Dans la partie A) sont publiées les données de huit stations choisies, à savoir: Ljubljana-Bežigrad, Zagreb-Grič, Split-Marjan, Bjelašnica, Sarajevo, Beograd, Novi Sad-Rimski Šančevi, Priština, Titograd et Skopje-Petrovac. Dans la partie B) figurent les données de toutes les stations météorologiques des réseaux de base.

La signification des symboles utilisés est la suivante:

φ = latitude, λ = longitude E de Greenwich, ΔG = différence entre l'heure locale et l'heure de Greenwich, H_s = altitude du pied de l'abri météorologique, H_b = altitude de la cuvette du baromètre, h_t = hauteur, au-dessus du sol, du réservoir du thermomètre, h_r = hauteur, au-dessus du sol, de l'ouverture de l'entonnoir du pluviomètre.

Les désignations des éléments météorologiques particuliers sont conformés aux conventions internationales. Leur valeurs sont données en unités de mesure suivantes:

P = pression atmosphérique en hPa à la station; T = température en °C; e = tension de vapeur d'eau en hPa; U = humidité relative en %; D = direction du vent en rose des vents de 8 ou de 16 directions; F = force du vent d'après l'échelle Beaufort (0-12); v = vitesse du vent en m/s; V = visibilité en km; N = nébulosité (0-10); insolation = durée d'insolation en heures; R = précipitations en mm; h_s = épaisseur de la couche de neige en cm; W = évolution du temps (genre du phénomène, son intensité et sa durée) décrite par des symboles internationaux

Dans la colonne "Razvoj vremena" (évolution du temps) les abréviations suivantes sont utilisées:

n = au cours de la nuit; rj = tôt le matin; dp = avant midi; pp = après midi; kv = tard le soir; i = avec intermittence.

Les valeurs moyennes journalières et mensuelles de la température - à 7 h, 14 h et 21 h, heure locale, sont calculées d'après la formule:

$$\frac{t_7 + t_{14} + 2 \times t_{21}}{4}$$

et pour les autres éléments (P, e, U, N) on a calculé les moyennes arithmétiques simples pour obtenir les valeurs moyennes journalières et mensuelles des observations de 7 h, 14 h et 21 h

Les lectures des thermomètres à maxima et minima suivies de leur amorçage, ont été faites à 21 h et les valeurs inscrites le même jour.

Les valeurs journalières de précipitations relevées à 7 h se rapportent aux 24 heures précédentes, c'est-à-dire de 7 h la veille à 7 h du jour de la lecture.

L'épaisseur de la couche de neige est mesurée à 7 h.

Dans les tableaux A sont soulignées les valeurs maxima de la pression atmosphérique de la température de l'air, de la tension de vapeur d'eau, de la force du vent $F \geq 6$ (de l'échelle Beaufort) et des précipitations, ainsi que les valeurs minima de la pression atmosphérique de la température de l'air, de la tension de vapeur d'eau et de l'humidité relative.

Dans les tableaux B pour les extrêmes moyennes mensuelles de la température de l'air les indications $\overline{\text{Max}}$ et $\overline{\text{Min}}$ ont été utilisées: dans les colonnes "Broj dana sa" (Nombre de jours avec) • ou ♣, ✕ ou ⚡ et ⚡ sont indiqués seulement les jours avec une hauteur de précipitation en question de 0.1 mm au moins.

Le numéro de la station (colonne 2 de la Liste alphabétique) est en effet le numéro d'ordre de la série des stations dont les données figurent dans les tableaux de la partie B).

A la fin de la publication on trouvera la carte de la R.S.F. de Yougoslavie donnant les stations climatologiques de l'année 1985; les numéros de ces stations correspondent aux numéros des stations dont les données figurent dans les tableaux de la partie B.

ABUČNI SPISAK STANICA

PO SOCIJALISTIČKIM REPUBLIKAMA
 Inak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

III

STANICA	Broj stanice	Nadorna visina H, m	Geografska širina Y°N	Geografska dužina X°E Gr.	Red stanice	Vazdušni pritisak	Temperatura vanjska	Vlagaost vanjska	Vetar	Oblačnost	Inzolucija	Padavine	Broj karak-terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Topusko	57	128	45°18'	15°59'	ob		x	x	x	x		x	x
Varaždin	38	167	46°16'	16°23'	gl	x	x	x	x	x	x	x	x
Vela Luka	91	30	42°58'	16°43'	ob		x	x	x	x		x	x
Zadar	78	8	44°08'	15°13'	ob	x	x	x	x	x	x	x	x
Zagreb-Grič	86	157	45°49'	15°58'	gl	x	x	x	x	x	x	x	x
Zagreb-Maksimir	58	123	45°49'	16°02'	gl	x	x	x	x	x	x	x	x
Zalesina	48	790	45°23'	14°53'	ob		x	x	x	x		x	x
Zavišan	76	1594	44°49'	14°59'	gl	x	x	x	x	x	x	x	x
SOCIJALISTIČKA REPUBLIKA BOSNA I HERCEGOVINA													
Banja Luka	108	153	44°47'	17°13'	gl	x	x	x	x	x	x	x	x
Berkovići	133	537	43°08'	18°11'	ob		x	x	x	x		x	x
Bihać	100	246	44°49'	15°53'	gl	x	x	x	x	x	x	x	x
Bijeljina	123	90	44°47'	19°16'	ob		x	x	x	x	x	x	x
Bileća	143	491	42°53'	18°27'	ob		x	x	x	x		x	x
Bjelašnica	134	2067	43°43'	18°16'	gl	x	x	x	x	x	x	x	x
Bos. Dubice	98	98	45°13'	16°54'	ob		x	x	x	x		x	x
Bos. Krupa	101	176	44°53'	16°10'	ob		x	x	x	x		x	x
Bos. Novi	97	119	45°03'	18°23'	ob		x	x		x		x	x
Brčko	121	96	44°53'	18°50'	ob		x	x	x	x		x	x
Bugojno	112	562	44°04'	17°28'	gl	x	x	x	x	x	x	x	x
Čapljina-Klepci	128	5	43°05'	17°43'	ob		x	x	x	x		x	x
Čemerno	139	1305	43°14'	18°38'	gl	x	x	x	x	x	x	x	x
Derventa	99	108	45°00'	17°55'	ob		x	x	x	x		x	x
Doboj	117	146	44°44'	18°06'	ob		x	x	x	x	x	x	x
Domanovići	130	146	43°09'	17°47'	ob		x	x	x	x		x	x
Drinić	103	730	44°31'	16°28'	ob		x	x	x	x		x	x
Gacko	138	940	43°10'	18°33'	ob	x	x	x	x	x	x	x	x
Glamoč	107	1000	44°04'	16°52'	ob		x	x	x	x		x	x
Goražde	141	345	43°40'	18°59'	ob		x	x	x	x		x	x
Ivan Sedlo	132	970	43°46'	18°02'	ob		x	x	x	x		x	x
Jablanica	129	195	43°40'	17°46'	ob		x	x	x	x		x	x
Jajce	109	431	44°21'	17°16'	ob		x	x	x	x	x	x	x
Kalinovik	137	1073	43°31'	18°27'	ob	x	x	x	x	x		x	x
Kotor Varoš	111	266	44°38'	17°23'	ob		x	x		x		x	x
Kupres	110	1190	44°00'	17°17'	ob		x	x	x	x		x	x
Lastva	144	310	42°43'	18°29'	ob		x	x	x	x		x	x
Lištica	126	270	43°23'	17°36'	ob		x			x		x	x
Livno	124	724	43°50'	17°01'	gl	x	x	x	x	x	x	x	x
Ljubinja	142	450	42°58'	18°06'	ob		x		x	x		x	x
Maoča	119	335	44°18'	18°26'	ob		x	x	x	x		x	x
Mlinište	106	970	44°16'	16°51'	ob		x		x	x		x	x
Modriča	118	115	44°50'	18°18'	ob		x	x	x	x		x	x
Mostar	131	99	43°21'	17°48'	gl	x	x	x	x	x	x	x	x
Prijedor	105	135	44°59'	16°44'	ob		x	x		x		x	x

AERUČNI SPISAK STANICA
PO SOCIJALISTIČKIM REPUBLIKAMA

Znak x pokazuje da stanica raspolaže odgovarajućim podacima meteoroloških elemenata navedenih u kolonama 7-14

S T A N I C A	Broj stanice	Najviša visina m	Geografska širina °'N	Geografska dužina °'E Gr.	Red stanice	Vazdušni pritisak	Temperatura u vazduhu	Vlažnost u vazduhu	Vetar	Oblakost	Inzuelacija	Padavine	Broj karak- terističnih dana
1	2	3	4	5	6	7	8	9	10	11	12	13	14
Prnjavor	114	185	44°52'	17°42'	ob		x	x	x	x		x	x
Prozor	127	800	43 50	17 37	ob		x		x	x		x	x
Rakitno	125	915	43 33	17 27	ob		x		x	x		x	x
Sanaki Most	104	158	44 46	16 42	ob		x	x	x	x	x	x	x
Sarajevo	136	630	43 52	18 26	gl	x	x	x	x	x	x	x	x
Sarajevo-aerodrom	135	510	43 49	18 20	gl	x	x	x	x	x		x	x
Sokolac	140	872	43 57	18 49	ob		x	x	x	x	x	x	x
Titov Drvar	102	485	44 23	16 24	gl	x	x	x	x	x	x	x	x
Trevnik	113	581	44 14	17 41	ob		x	x	x	x		x	x
Tuzla	120	305	44 33	18 40	gl	x	x	x	x	x	x	x	x
Vlasenica	122	670	44 11	18 57	ob		x	x	x	x		x	x
Vučica-Tešić	115	225	44 36	17 52	ob		x		x	x		x	x
Zenica	116	345	44 13	17 54	gl	x	x	x	x	x	x	x	x
S O C I J A L I S T I Č K A R E P U B L I K A S R B I J A													
T E R I T O R I J A S R B I J E V A N S A P													
Aleksandrovac	172	360	43°27'	21°04'	ob		x			x		x	x
Babušnica	183	495	43 04	22 26	ob		x			x		x	x
Beograd	190	132	44 48	20 28	gl	x	x	x	x	x	x	x	x
Bor	161	386	44 04	22 06	ob		x	x	x	x	x	x	x
Bošiljgrad	196	830	42 30	22 28	ob		x			x		x	x
Bujanovac	188	400	42 27	21 47	ob		x			x		x	x
Bukovička Banja	183	265	44 18	20 33	ob		x	x	x	x		x	x
Čačak	168	250	43 53	20 19	ob		x			x		x	x
Čuprija	177	123	43 56	21 23	gl	x	x	x	x	x	x	x	x
Debeli Lug	160	290	44 22	21 55	ob		x			x		x	x
Dimitrovgrad	188	446	43 01	22 45	gl	x	x	x	x	x	x	x	x
Gornji Milanovac	181	385	44 03	20 29	ob		x	x	x	x		x	x
Ivanjica	167	465	43 35	20 14	ob		x	x	x	x		x	x
Knjaševac	181	280	43 34	22 16	ob		x			x		x	x
Kragujevac	158	181	44 02	20 56	ob	x	x	x	x	x	x	x	x
Kraljevo	170	219	43 44	20 41	gl	x	x	x	x	x	x	x	x
Kruševac	174	166	43 34	21 21	gl	x	x	x	x	x	x	x	x
Kukavica	191	1250	42 45	21 59	ob		x			x		x	x
Kuršumlija	175	380	43 08	21 16	gl	x	x	x	x	x	x	x	x
Leskovac	190	230	42 59	21 57	gl	x	x	x	x	x	x	x	x
Lesnica	145	121	44 33	19 14	gl	x	x	x	x	x	x	x	x
Ljubovija	146	170	44 11	19 23	ob		x	x	x	x		x	x
Negošín	163	42	44 14	22 33	gl	x	x	x	x	x	x	x	x
Niš	180	202	43 20	21 54	gl	x	x	x	x	x	x	x	x
Novi Pazar	169	545	43 08	20 31	ob		x			x		x	x
Petrovac	157	120	44 23	21 25	ob		x			x		x	x
Pirot	184	370	43 09	22 36	ob		x			x		x	x
Predejane	193	318	42 50	22 08	ob		x	x	x	x		x	x
Prokuplje	178	765	43 14	21 36	ob		x	x	x	x		x	x
Rekovac	173	230	42 57	21 06	ob		x	x	x	x		x	x

A) Dnevna osmatranja

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T °C					Napon vodene pare e hPa			Relativna vlažnost u%				Privoć i jačina veta D, f (0-12)								
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	779.9	776.3	773.2	-15.0	-10.6	-12.0	-12.4	-09.0	-15.0	-	01.7	02.5	02.2	86	90	89	88	E	4	SSW	4	SSW	7	
2	770.6	767.4	766.4	-10.0	-10.0	-13.8	-11.9	-08.2	-13.8	-	02.6	02.6	31.8	91	91	87	90	SSW	3	NE	4	NF	6	
3	766.7	768.0	770.1	-14.5	-15.2	-17.0	-15.9	-13.8	-17.0	-	01.7	01.7	01.4	87	89	88	88	NNE	7	NE	6	NNE	3	
4	770.6	770.1	769.5	-15.3	-11.0	-11.5	-12.3	-11.0	-17.6	-	01.6	02.4	02.3	86	90	92	89	NNW	1	SW	4	SW	6	
5	764.6	761.5	765.6	-10.0	-08.0	-13.0	-11.0	-07.2	-13.0	-	02.5	03.1	02.0	88	92	91	90	SSW	8	SW	6	SW	6	
6	769.6	768.2	768.4	-13.5	-17.1	-10.8	-13.1	-10.8	-18.0	-	02.0	01.4	02.4	93	88	90	90	WSW	2	NE	2	SSE	3	
7	768.4	769.2	771.8	-10.3	-11.7	-11.5	-11.3	-09.2	-12.0	-	02.5	02.3	02.3	90	92	92	91	SSW	4	SSW	6	SW	5	
8	775.7	774.3	773.3	-12.4	-11.3	-11.5	-11.7	-11.2	-12.4	-	02.2	02.3	02.3	91	89	92	91	SW	5	VE	2	ESE	2	
9	773.5	771.7	771.1	-09.8	-08.2	-08.9	-09.0	-08.2	-11.8	-	02.7	03.0	02.9	93	92	92	92	SSE	3	SE	2	S	4	
10	771.9	774.0	776.6	-11.1	-11.4	-13.5	-12.4	-08.9	-13.5	-	02.4	02.4	02.0	92	92	93	92	SSW	4	S	3	NNE	4	
11	778.4	782.4	783.3	-18.7	-19.0	-20.4	-19.6	-13.5	-20.4	-	01.3	01.2	01.2	91	87	82	87	NNE10	N	7	N	6		
12	784.2	785.0	785.3	-20.2	-17.5	-15.0	-16.9	-15.0	-20.7	-	01.1	01.3	21.7	86	84	77	82	NE	5	NNE	3	SSW	4	
13	783.7	785.5	785.9	-11.8	-11.1	-11.2	-11.3	-11.5	-15.0	-	02.3	02.2	01.0	92	82	34	69	SSW	8	N	1	NW	1	
14	782.4	782.3	785.3	-10.4	-06.3	-06.4	-07.4	-05.4	-11.3	-	01.5	02.6	03.3	55	67	78	67	E	1	SW	4	SW	5	
15	788.6	791.9	791.8	-07.4	-05.4	-05.4	-05.9	-05.0	-07.4	-	03.3	03.9	03.9	95	95	95	95	SW	8	SW	6	SSW	6	
16	790.9	789.6	787.9	-03.7	-04.1	-04.5	-04.2	-03.6	-05.6	-	04.5	04.3	02.0	96	96	46	79	SSW	4	ESE	3	ESE	3	
17	782.4	780.2	779.1	-06.6	-05.5	-05.9	-06.0	-04.5	-08.8	-	01.9	01.7	01.0	51	42	25	39	ESE	6	ESE	7	SE	5	
18	775.7	774.3	780.0	-02.4	-05.0	-07.4	-05.6	-02.4	-07.4	-	04.1	03.3	03.3	80	79	95	85	SSW	7	SSW	8	SSW	7	
19	775.0	775.9	777.5	-05.6	-04.2	-04.3	-04.6	-04.1	-08.4	-	03.8	04.3	04.3	95	96	96	96	SSW	7	W	2	N	3	
20	779.1	779.3	780.8	-04.8	-03.8	-04.5	-04.4	-03.3	-04.8	-	04.1	04.4	04.2	95	96	96	96	NE	2	SSW	4	SW	4	
21	782.7	783.5	784.3	-05.2	-04.6	-04.2	-04.6	-03.4	-05.2	-	03.9	04.2	04.3	95	96	96	96	W	2	SW	7	SSW	7	
22	783.7	784.2	783.4	-02.8	-00.2	00.2	-00.7	00.2	-04.2	-	04.8	06.0	06.2	97	100	100	99	SSW	9	SSW	9	SSW12		
23	786.7	786.6	785.9	00.4	00.6	-00.4	00.1	01.0	-00.4	-	06.3	06.4	05.9	100	100	100	100	SSW11	SSW10	SSW	9			
24	776.8	780.0	792.8	-01.4	-01.8	-08.0	-04.8	-09.4	-08.0	-	05.5	05.3	03.1	100	98	92	97	SSW14	S	10	NNE	7		
25	783.9	781.6	782.0	-09.3	-06.5	-06.8	-07.4	-06.2	-11.9	-	02.8	03.2	03.3	91	86	90	89	SSW	3	SW	8	SW	7	
26	781.9	778.7	778.3	-06.1	-04.6	-04.2	-04.8	-04.2	-06.9	-	03.4	03.9	04.1	88	90	91	90	SW	9	SSW10	SSW10			
27	779.1	780.3	782.6	-03.8	-03.2	-02.9	-03.2	-02.9	-04.2	-	04.2	04.6	04.5	91	95	92	93	SSW	8	S	7	SSW	3	
28	784.3	784.6	785.1	-07.4	-05.3	-07.9	-07.1	-02.9	-07.9	-	03.2	03.8	03.1	91	93	93	92	N	2	ESE	2	ESE	2	
29	786.0	789.2	792.2	-07.2	-07.4	-08.4	-07.9	-07.0	-09.9	-	03.0	03.0	02.8	85	87	88	87	NE	3	ESE	2	ESE	2	
30	793.0	791.9	791.1	-06.4	-05.0	-05.2	-05.5	-04.8	-08.5	-	02.7	03.2	02.8	70	77	64	70	E	1	NE	2	N	6	
31	789.6	791.1	791.0	-08.8	-08.5	-05.0	-06.8	-05.0	-09.2	-	02.9	03.0	02.0	92	92	48	77	NE	7	NNE	6	N	4	
M.																								
VR	779.4	779.3	780.6	-08.8	-07.8	-06.4	-08.4	-06.5	-10.6	-	03.0	03.2	02.9	88	88	83	86	S.4	S.1	S.1				

1	787.3	787.9	788.3	-05.8	-05.2	-02.0	-03.8	-02.0	-05.8	-	02.9	03.4	03.8	73	82	72	76	NNE	9	NNE	8	NNW	7
2	787.8	786.6	784.7	00.0	-00.4	-02.5	-01.4	00.3	-02.5	-	04.1	03.8	05.0	67	65	98	77	N	7	W	3	WNW	4
3	784.8	785.2	787.1	-06.2	-05.0	-11.0	-08.3	-02.5	-11.0	-	03.6	03.0	02.4	94	71	90	85	N	7	W	8	NNE	9
4	783.3	785.7	785.7	-18.3	-16.0	-14.6	-15.8	-11.0	-18.4	-	01.2	00.7	01.0	84	42	50	59	NNE12	NNE11	NNE12			
5	787.2	789.0	789.1	-08.4	-06.0	-06.0	-06.6	-05.0	-14.6	-	00.9	02.6	03.2	22	67	83	60	N	8	W	4	W	4
6	787.9	787.1	786.3	-04.8	-03.6	-03.9	-04.1	-03.6	-06.0	-	03.7	04.3	04.2	86	91	91	89	WSW	7	WSW	6	NW	2
7	784.7	784.0	785.0	-04.6	-02.6	-04.6	-04.1	-02.5	-04.7	-	03.9	03.7	03.5	90	73	81	81	N	3	W	3	N	5
8	785.0	785.3	782.3	-05.0	-04.0	-03.0	-03.8	-03.0	-06.1	-	03.3	03.8	04.4	78	84	90	84	WSW	6	SW	6	SSW	9
9	781.1	781.5	778.9	-01.0	-00.1	-00.1	-00.1	-00.1	-03.0	-	05.5	05.9	05.9	97	97	97	97	SW	10	S	7	SSW	7
10	774.0	774.3	771.9	-00.6	-00.6	-01.0	-00.8	03.0	-01.2	-	05.8	05.9	05.6	98	100	99	99	SSW10	SSW	9	SSW	9	
11	769.6	770.0	771.7	-02.4	-04.0	-05.5	-04.4	-01.0	-06.1	-	05.0	04.4	03.8	98	96	95	96	SSW	8	SSW	5	SSW	6
12	769.3	768.4	770.4	-17.0	-20.2	-19.8	-19.2	-05.0	-20.8	-	01.4	01.0	01.1	85	82	82	83	NNE	7	NE	9	NE	4
13	773.4	771.8	774.0	-18.1	-18.8	-19.0	-18.7	-18.1	-20.0	-	01.1	01.2	01.1	72	83	83	79	NNE	6	N	8	NNE10	
14	777.2	780.6	783.4	-17.8	-12.2	-09.0	-12.0	-09.0	-19.5	-	01.3	01.6	01.7	84	65	55	68	NE	8	NE	4	NW	3
15	783.2	779.0	782.6	-10.2	-06.8	-11.0	-09.8	-04.9	-11.0	-	01.8	03.4	02.4	65	94	92	84	SW	11	SSW10	NNE	5	
16	787.3	786.4	786.4	-18.0	-18.8	-19.4	-18.9	-11.0	-20.2	-	01.3	01.2	01.1	88	83	83	85	NE	7	NE	7	NE	6
17	787.8	785.1	784.0	-09.6	-09.6	-11.2	-10.4	-09.0	-19.4	-	01.3	02.5	02.2	45	84	85	71	W	2	WSW	4	NNE	5
18	779.5	779.8	779.9	-19.2	-20.5	-23.7	-21.8	-11.2	-23.7	-	01.1	00.9	00.7	83	77	79	80	NNE	7	YNE	8	NNE10	
19	779.9	781.0	779.3	-23.1	-20.7	-21.0	-21.5	-20.4	-24.4	-	00.8	01.0	00.9	80	82	81	81	NE	6	NNE	7	NNE11	
20	782.4	787.1	787.9	-21.2	-18.4	-18.2	-19.0	-18.2	-21.2	-	00.9	01.2	01.2	81	84	84	83	NE	10	NNE	8	NE	8
21	787.9	789.0	789.7	-18.6	-15.2	-12.8	-14.9	-12.8	-19.0	-	00.9	01.4	01.1	63	73	50	62	NNE	8	NNE	5	NW	3
22	789.1	790.6	790.6	-15.0	-13.4	-14.8	-14.5	-12.6	-15.0	-	00.9	01.9	01.7	44	85	86	72	NNE	5	NE	4	NE	5
23	789.9	789.3	789.6	-15.3	-15.5	-17.0	-16.1	-14.8	-17.0	-	01.7	01.6	01.4	86	86	85	86	NE	7	NE	8	NE	10
24	789.0	785.9	786.3	-14.3	-10.2	-12.7	-12.5	-10.0	-17.1	-	01.8	02.6	02.3	87	90	88	88	NE	9	NNE11	NE	11	
25	792.2	794.7	796.6	-13.2	-07.0	-02.8	-06.5	-02.8	-14.5	-	01.9	01.9	03.8	88	51	77	72	NE	10	NNE	7	NNE	8
26	785.9	797.3	797.6	-02.4	-02.2	-02.2	-02.3	-02.2	-03.4	-	03.7	04.0	03.8	73	76	73	74	NNE	8	NNE	4	NNE	3
27	796.4	796.6	796.4	-02.6	-01.2	-03.4	-02.7	-01.0	-03.4	-	03.5	03.9	01.6	69	69	34	57	NNE	2	NNF	2	SW	3
28	795.5	795.5	795.0	-03.4	-01.6	-03.4	-03.0	-01.3	-03.6	-	03.5	04.5	04.5	75	82	95	83	W	3	W	2	WSW	2
29			785.0	-10.6	-09.3																		

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$H_a = 2067 = H_b = 2070.4 = h_c = 3.0 = h_f = 1.5 m$

Dan	Vidljivost 0-9		Oblačnost N (0-10)			Inzolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
	14	7	14	21	Sred Dias				
1	1	10	10	10	10.0	04.8	07.7	29	Y0-24, F-0-9 ³⁰ 12 ²⁰ 24, F-0-5, 16 ²⁰ 24, *0-4 ⁵⁰ 23 ²⁰ 24, ☐
2	0	10*	10*	10*	10.0	00.0	03.4	33	Y0-24, F-0-4 ²⁰ 20 ²⁰ 24, = 0-24, *0-24, ☐
3	1	10	10*	00	06.7	00.0	16.2	46	Y0-24, = 0-05 ¹⁰ * 0-23 ²⁰ 7 ¹⁰ 14 ²⁰ F-0-17 ²⁰ * 23 ²⁰ 24, ☐
4	8	04	08	09	06.3	03.5	02.9	43	Y0-19 ²⁰ * 20 ²⁰ * 11 ²⁰ 15 ²⁰ F-0-16 ²⁰ 24, ☐
5	0	10*	10*	10	10.0	00.0	03.7	41	F-0-24, = 2 ²⁰ 20 ²⁰ * 4-13 ²⁰ 14 ²⁰ 5 ²⁰ * 4-1 ²⁰ 23 ²⁰ * 13 ²⁰ 14 ²⁰ 15 ²⁰ , ☐
6	1	10*	10*	10*	10.0	00.0	14.7	62	Y0-24, F0-1 ²⁰ * 4 ²⁰ 24, = 5 ²⁰ 24, ☐
7	0	10	10*	10*	10.0	00.0	05.8	66	Y0-24, = 0-24 * 0-2, 9-17 ²⁰ 24, F-0-9 ²⁰ 24 * 13-23 ²⁰ , ☐
8	0	04	10*	10*	08.0	00.0	01.6	66	Y0-24, = 0-24 ²⁰ 13 ²⁰ 24 * 0-2 ²⁰ 14 ²⁰ 24, F0-7 ²⁰ , ☐
9	0	10	10*	10*	10.0	00.0	01.3	65	Y0-24, = 0-24, *0-24, ☐
10	8	04	00*	10*	04.7	03.5	02.0	66	Y0-24, = 0-24, *0-3, *11-14 ²⁰ 15 ²⁰ 22 ²⁰ 24, ☐
11	3	10*	10	10	10.0	00.2	00.6	67	Y0-24, = 0-24, F0-24 * 5-7, * 5-11, ☐
12	9	00	00	00	00.0	08.5	00.0	66	F0-24, F0-9 ²⁰ 24 = 0-5 ²⁰ 16-20 ²⁰ 11 ²⁰ 18-24, ☐
13	9	02	00	00	00.7	08.5	.	64	F0-0-11 ²⁰ Y0-20 ²⁰ * 0-24, = 9 ²⁰ 11 ²⁰ , ☐
14	9	09	06	03	06.0	03.6	.	66	*11-0-0-24, F0-20 ²⁰ 24, ☐
15	1	10	10	10	10.0	00.0	.	66	F0-24, = 6-24, VY6 ²⁰ 24, * 21-24, ☐
16	9	10	08	00	06.0	02.7	00.7	65	F0-5, Y0-23, = 0-11 ²⁰ * 0-4, * 20-22 ²⁰ 24, ☐
17	9	10	09	04	07.7	02.1	.	65	*11-0-0-24, F0-5 ²⁰ 24 ²⁰ , ☐
18	8	10	04	10	08.0	04.4	.	60	*11-0-0-20 ²⁰ F-0-0 ²⁰ 24, = 20 ²⁰ 24, V20 ²⁰ 24, ☐
19	7	10	05	10	08.3	00.9	.	60	F-0-0-11 ²⁰ = 0-23, VY0-24, * 17 ²⁰ 19 ²⁰ * 13-20, ☐
20	1	10	10*	10	10.0	00.4	00.8	60	*11-0-3, Y0-24, = 3-22 ²⁰ * 17 ²⁰ 17 ²⁰ , ☐
21	0	10	10*	10	10.0	00.0	01.8	59	Y0-24, F0-1 ²⁰ 5 ²⁰ 8 ²⁰ 24, = 6 ²⁰ 24 * 7 ²⁰ 14, 23-24, * 13 ²⁰ 17, 23 ²⁰ 24, ☐
22	0	10	10*	10*	10.0	00.0	02.3	57	Y0-13, = 0-24, F0-0-24, * 0-3, * 0-4, * 10 ²⁰ 13 ²⁰ , * 13 ²⁰ 24, ☐
23	0	10	10	10	10.0	00.0	01.9	35	= 0-24, F0-0-24, * 0-2 ²⁰ 13-18, Y23 ²⁰ 24, ☐
24	0	10	10*	10*	10.0	00.0	00.8	32	= 0-24, F0-0-24, * 10-22 ²⁰ * 10-20 ²⁰ F-17 ²⁰ 20 ²⁰ , ☐
25	8	00	09	00	03.0	06.1	14.3	46	= 0-3 ²⁰ 19 ²⁰ 24, Y0-24, F0-0-2 ²⁰ , 8-24, * 1 ²⁰ 2 ²⁰ * 5 ²⁰ 14, * 12 ²⁰ 24, ☐
26	0	10	10	10	10.0	00.0	.	45	Y0-24, F0-0-24, = 0-24, * 0-24, ☐
27	0	10	10	10	10.0	00.0	.	43	Y0-24, = 0-24, F-0-16 ²⁰ * 0-1 ²⁰ * 12-16, 21 ²⁰ 24, ☐
28	0	10*	10	09	09.7	00.0	02.6	45	Y0-24, = 0-20 ²⁰ * 0-8 ²⁰ * 0-4 ²⁰ 16 ²⁰ 20 ²⁰ 25, ☐
29	0	10	10	00	06.7	00.4	00.1	45	Y0-24, = 5 ²⁰ 20 ²⁰ * 14 ²⁰ 20 ²⁰ 24, ☐
30	9	00	01	02	01.3	09.1	.	44	Y0-24, * 16-16-0-11, F-13 ²⁰ 24, * 17 ²⁰ 24, ☐
31	8	10*	02	01	04.3	05.0	01.8	45	Y0-24, F-0-13 ²⁰ , * 0-10 ²⁰ , = 1-13 ²⁰ , * 4 ²⁰ 8 ²⁰ , ☐
M.									
VP.	08.1	07.8	07.0	07.6	63.7	85.0			

1	8	10	07	10	09.0	05.1	00.1	45	Y0-24, F-0-2 ²⁰ 24, = 7 ²⁰ 9 ²⁰ , ☐
2	8	09	09	10*	09.3	00.3	.	45	Y0-6 ²⁰ 22 ²⁰ 24, F-0-13 ²⁰ * 13 ²⁰ 24, = 20 ²⁰ 24, ☐
3	8	04	05	10*	06.3	07.2	03.8	48	Y0-24, = 0-3 ²⁰ 14 ²⁰ 24, * 0-3 ²⁰ 20 ²⁰ 24, F-0-24, * 2 ²⁰ 24, ☐
4	9	02	02	00	01.3	09.1	01.9	47	= 0-24, F-0-1 ²⁰ * 0-4 ²⁰ F-0-24, * 0-24, * 0-24, ☐
5	9	09	08	10	09.0	05.5	.	45	Y0-24, F-0-12, 23-24, * 0-6, = 20 ²⁰ 24, ☐
6	0	10	10	10	10.0	00.0	.	40	F0-24, = 0-24, Y0-24, ☐
7	9	00	03	00	01.0	08.1	.	40	Y0-24, = 0-1 ²⁰ 15 ²⁰ 24, * 11-14 ²⁰ 15 ²⁰ * 17-18 ²⁰ F-21-24, ☐
8	1	03	10	10	07.7	01.3	00.2	37	F-0-24, Y0-24, = 0-1 ²⁰ 9 ²⁰ 24, * 13-17 ²⁰ 19 ²⁰ 9, ☐
9	0	10	10	10	10.0	00.0	00.7	37	= 0-24, Y0-24, F-0-24, * 0-17 ²⁰ 18 ²⁰ 22 ²⁰ 23 ²⁰ 24, ☐
10	0	10*	10*	10*	10.0	00.0	03.0	30	F-0-24, = 0-24, * 1 ²⁰ 24, * 2 ²⁰ 3, * 3-24, * 9 ²⁰ 10, ☐
11	1	10*	10*	10*	10.0	00.0	16.0	40	= 0-24, F-0-11 ²⁰ 15-24, * 0-24, Y0-24, ☐
12	2	10*	10	00	06.7	00.0	43.4	97	= 0-24, Y0-24, * 0-12 ²⁰ F-0-13 ²⁰ , * 8 ²⁰ 16 ²⁰ , * 20 ²⁰ 24, ☐
13	9	00	00	00	00.0	09.5	02.1	96	Y0-24, * 0-13 ²⁰ 20 ²⁰ 24, F-0-5 ²⁰ 24, * 10-24, ☐
14	9	00	01	00	00.3	05.6	.	96	Y0-24, F-0-13, * 0-15 ²⁰ * 11-14 ²⁰ 6, ☐
15	0	09	10*	10*	09.7	00.0	.	94	F-0-11 ²⁰ 16 ²⁰ 15 ²⁰ 24, * 5 ²⁰ 18, = 8 ²⁰ 24, VY8 ²⁰ 24, * 10-24, ☐
16	8	04	00	00	01.3	08.7	04.7	95	= 0-5 ²⁰ * 0-2 ²⁰ Y0-24, * 0-23, F-0-23 ²⁰ * 5 ²⁰ 11 ²⁰ , ☐
17	3	10	10*	10*	10.0	00.0	.	90	Y0-24, * 9 ²⁰ 23 ²⁰ * 11-13 ²⁰ 20 ²⁰ 24, = 10 ²⁰ 23 ²⁰ * 23 ²⁰ 24, ☐
18	8	10	05	10	09.3	03.0	02.3	91	Y0-24, F-0-24, * 0-5 ²⁰ 8 ²⁰ 17 ²⁰ , = 5 ²⁰ 8 ²⁰ 17 ²⁰ 24, * 15-24, ☐
19	0	10	10	10	10.0	00.0	.	88	Y0-24, = 0-24, * 0-24, F-0-24, ☐
20	1	10	10	00	06.7	00.0	.	86	Y0-24, F-0-24, = 0-13 ²⁰ , * 0-24, ☐
21	9	00	02	01	01.0	05.6	.	85	Y0-24, F-0-11 ²⁰ * 10-10 ²⁰ * 10-10 ²⁰ , ☐
22	9	04	02	00	02.0	09.2	.	82	Y0-24, F-0-10 ²⁰ 17 ²⁰ 24, ☐
23	0	10	10*	10	10.0	00.0	.	80	Y0-24, F-0-24, = 2 ²⁰ 23 ²⁰ , * 8 ²⁰ 24, * 13 ²⁰ 19 ²⁰ , ☐
24	0	05	10*	10*	08.3	00.0	01.5	82	Y0-24, F-0-24, * 0-24, = 7 ²⁰ 24, * 10 ²⁰ 24, ☐
25	9	01	01	00	00.7	09.2	04.5	85	Y0-24, F-0-24, * 0-11 ²⁰ , = 0-10 ²⁰ * 0-11 ²⁰ 11 ²⁰ 16 ²⁰ 24, ☐
26	8	01	05	06	04.0	08.8	.	85	Y0-24, F-0-16 ²⁰ * 16-16-0-24, = 0 ²⁰ 16 ²⁰ , ☐
27	8	09	19	06	08.3	00.0	.	85	Y0-8 ²⁰ * 10-24, ☐
28	2	05	10	10*	07.3	04.5	.	83	*0-19 ²⁰ , = 11 ²⁰ 24, VY19 ²⁰ 24, * 20 ²⁰ 23 ²⁰ , ☐
M.									
VP.	06.3	06.8	06.2	06.4	108.7	84.2			

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$$H_a = 2067 \text{ m } H_b = 2070.4 \text{ m } h_c = 3.0 \text{ m } h_r = 1.5 \text{ m}$$

Dan	Vidljivost 0-10	Oblačnost N (0-10)				Inzolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21				
1	2	10	10	10	10.0	00.0	07.3	75	0-24, V0-24, *8 ⁰⁰ H ²⁰ , 21 ⁰⁰ 22 ⁰⁰ , F 22-24, ☐
3	0	10	10	10	10.0	00.0	09.3	76	0-24, V0-24, F 0-24, *10 ⁰⁰ 21 ⁰⁰ , † 22-24, ☐
3	0	10	10	10	10.0	00.0	03.7	80	0-24, V0-24, F 0-24, *0.16 ⁰⁰ 21 ⁰⁰ 22 ⁰⁰ , † * 0-14, ☐
4	9	10	02	00	00.7	10.2	04.2	82	V0-24, ☐ 0-14 ⁰⁰ , F 0-3, 10 ⁰⁰ 21 ⁰⁰ , † 5-H ⁰⁰ , ☐
5	9	08	04	08	06.7	09.3	.	78	V0-24, F 0-24, † 18-20 ⁰⁰ 10 ⁰⁰ , ☐
6	9	08	08	02	06.0	07.9	.	73	F 0-24, † 18-20 ⁰⁰ 5 ⁰⁰ 24 ⁰⁰ , ☐
7	8	06	08	06	06.7	08.4	.	67	F 0-15, 23 ⁰⁰ 24 ⁰⁰ , ☐
8	8	10	10	10	10.0	00.2	.	60	F 0-5 ⁰⁰ , ☐
9	0	10	10	10	10.0	00.0	00.3	56	*15 ⁰⁰ 21 ⁰⁰ 22 ⁰⁰ 24 ⁰⁰ , † 15 ⁰⁰ 24 ⁰⁰ , ☐
10	2	10	10	10	10.0	00.0	16.2	66	0-24, *0-24, VV0-24, ☐
11	0	10	10	10	10.0	00.0	17.0	80	0-24, V0-24, *0-24, F 13-15, ☐
12	0	10	10	10	10.0	00.0	20.0	95	0-22 ⁰⁰ Y0-24, *0-22, † 22 ⁰⁰ 24 ⁰⁰ , ☐
13	9	14	00	00	01.3	10.1	05.8	96	VV0-24, † 17-19 ⁰⁰ 20 ⁰⁰ , ☐
14	0	10	10	10	10.0	00.0	00.2	90	VV0-24, *0-24, *G ⁰⁰ 24, F 9-24, ☐
15	0	10	10	10	10.0	00.0	06.0	94	*0-16 ⁰⁰ , 0-24, V0-24, F 0-24, ☐
16	0	10	10	10	10.0	00.0	05.3	95	F 0-24, ☐ 0-24, V0-24, *3-24, † 3 ⁰⁰ 4 ⁰⁰ , ☐
17	0	10	10	10	10.0	00.0	12.0	102	*0-1 ⁰⁰ 22 ⁰⁰ 24 ⁰⁰ , 0-24, V0-24, F 0-24, † 9 ⁰⁰ 24 ⁰⁰ , † 14 ⁰⁰ 15 ⁰⁰ , ☐
18	0	05	10	10	08.3	00.0	10.8	106	V0-24, *0-5 ⁰⁰ 24 ⁰⁰ , F 0-23 ⁰⁰ , *0-5, 9 ⁰⁰ 24 ⁰⁰ , † 7-24, ☐
19	1	10	10	10	10.0	00.0	03.3	110	V0-H, † 0-1 ⁰⁰ , 0-24, *0-19 ⁰⁰ , ☐
20	8	01	05	10	05.3	08.4	00.7	111	0-5, 18 ⁰⁰ 24 ⁰⁰ , V 1 ⁰⁰ 9, 19 ⁰⁰ 24 ⁰⁰ , † 5-13 ⁰⁰ , F 8 ⁰⁰ 24 ⁰⁰ , † 8 ⁰⁰ 11 ⁰⁰ , ☐
21	0	10	10	10	10.0	00.0	.	110	0-24, F 0-24, V0-24, *8 ⁰⁰ 14 ⁰⁰ , ☐
22	8	10	10	10	10.0	00.7	00.5	108	0-9, 17 ⁰⁰ 24 ⁰⁰ , F 0-24, ☐
23	0	10	10	10	10.0	00.0	00.2	106	0-18, 21 ⁰⁰ 24 ⁰⁰ , F 0-15 ⁰⁰ 19 ⁰⁰ , *5 ⁰⁰ 17 ⁰⁰ 20 ⁰⁰ 22 ⁰⁰ 17 ⁰⁰ 21 ⁰⁰ , ☐
24	8	10	08	10	09.3	02.0	00.7	107	0-H ⁰⁰ 17 ⁰⁰ 24 ⁰⁰ , V 2 ⁰⁰ 15 ⁰⁰ 20-24 ⁰⁰ , *10 ⁰⁰ H ⁰⁰ 14 ⁰⁰ 18 ⁰⁰ 17 ⁰⁰ 15 ⁰⁰ 24 ⁰⁰ , ☐
25	8	08	08	00	05.3	03.9	00.4	108	F 0-16 ⁰⁰ , 0-24, 10 ⁰⁰ 12 ⁰⁰ , V 6-9, † 18-20 ⁰⁰ 11 ⁰⁰ 17 ⁰⁰ 9 ⁰⁰ H ⁰⁰ , *10 ⁰⁰ 12 ⁰⁰ , ☐
26	9	09	10	00	06.3	00.2	02.7	110	F 9 ⁰⁰ 17 ⁰⁰ , ☐
27	9	00	06	00	02.0	11.5	.	109	*07-06 G-H, F 12-24, ☐
28	1	10	10	10	10.0	00.0	00.3	100	F 0-24, ☐ 2 ⁰⁰ 24, V 5-24, *6 ⁰⁰ 24, † 9-H, † 7-20-24, ☐
29	1	10	10	00	06.7	00.2	24.0	125	V0-24, 0-19 ⁰⁰ , *0-5, F 0-15, † 7-20-24, ☐
30	9	02	00	05	02.3	11.4	.	125	V0-H ⁰⁰ , F 6 ⁰⁰ 20, ☐
31	9	04	04	08	05.3	11.2	.	120	F 8 ⁰⁰ 24, ☐
M.		07.9	08.2	07.4	07.8	95.6	135.0		
VR.									

1	8	10	08	00	06.0	03.7	.	112	F 0-24, ☐ G-13 ⁰⁰ V 7 ⁰⁰ 19, ☐
2	9	06	04	05	05.0	11.2	.	111	F 0-2, 15-18, ☐
3	1	10	10	10	10.0	00.0	04.8	102	F 0 ⁰⁰ 24, *0 ⁰⁰ 14 ⁰⁰ , ☐ 1 ⁰⁰ 22 ⁰⁰ V 1 ⁰⁰ 12 ⁰⁰ 19 ⁰⁰ 24 ⁰⁰ , † 7-9 ⁰⁰ 10 ⁰⁰ 22 ⁰⁰ 24 ⁰⁰ , ☐
4	9	02	02	00	01.3	11.7	00.4	98	F 0-24, V0-2 ⁰⁰ , † 18-20 ⁰⁰ 0-7 ⁰⁰ , ☐
5	9	00	00	00	00.0	11.8	.	90	F 0-24, ☐
6	3	04	10	10	08.0	01.1	.	82	F 0-24, ☐ 7 ⁰⁰ 24, VV 17 ⁰⁰ 24 ⁰⁰ , † 13-18 ⁰⁰ , ☐
7	8	10	09	00	06.3	04.5	01.0	80	0-12 ⁰⁰ V0-15, F 0-24, *G-15, † 7-12 ⁰⁰ , ☐
8	9	03	03	05	03.7	11.1	04.7	83	F 0-24, ☐
9	8	04	09	05	06.0	09.3	.	75	F 0-24, † 2 ⁰⁰ G-8, ☐
10	8	09	09	04	07.3	05.4	.	62	F 0-24, † 19 ⁰⁰ 24 ⁰⁰ , ☐
11	9	04	06	09	06.3	09.4	.	60	F 0-5, † 16-18 ⁰⁰ , ☐ 16 ⁰⁰ 18 ⁰⁰ 21-24 ⁰⁰ , *16 ⁰⁰ 18 ⁰⁰ V 16 ⁰⁰ 24 ⁰⁰ , ☐
12	0	10	10	10	10.0	00.0	01.7	62	0-21 ⁰⁰ V0-24, F 1 ⁰⁰ 12 ⁰⁰ 13 ⁰⁰ 24 ⁰⁰ , † 13-19 ⁰⁰ , ☐
13	8	10	06	00	05.3	03.1	04.1	65	V0-24, ☐ 0 ⁰⁰ 15 ⁰⁰ 17 ⁰⁰ 24 ⁰⁰ , *0 ⁰⁰ 5 ⁰⁰ 13 ⁰⁰ 15 ⁰⁰ 12 ⁰⁰ , ☐
14	8	06	10	10	08.7	03.3	.	63	V0-3, F 1 ⁰⁰ 24 ⁰⁰ , ☐ 14 ⁰⁰ 16 ⁰⁰ 18-24 ⁰⁰ , ☐
15	0	10	10	10	10.0	00.0	.	61	F 0-5, ☐ 0-24, VV 1 ⁰⁰ 24 ⁰⁰ , *15 ⁰⁰ 24 ⁰⁰ , ☐
16	0	10	10	10	10.0	00.0	03.1	64	0-24, V0-24, *0-24, F 14 ⁰⁰ 24 ⁰⁰ , † 7-13-24 ⁰⁰ , ☐
17	0	10	10	10	10.0	00.0	15.6	83	0-24, V0-24, *0-24, F 0-24, † 7-24 ⁰⁰ , ☐
18	0	10	10	10	10.0	00.0	07.2	87	0-24, V0-24, *0-24, F 0-24, † 7-24 ⁰⁰ , ☐
19	0	10	10	10	10.0	00.0	00.3	85	0-24, V0-24, F 0-24, ☐
20	2	10	10	10	10.0	01.9	.	84	0-23 ⁰⁰ V0-24, F 0-2, † 15-13 23 ⁰⁰ 24 ⁰⁰ , ☐
21	8	00	05	00	01.7	11.4	.	83	V 0-15, † 18-19 ⁰⁰ 12 ⁰⁰ , ☐
22	8	01	08	00	03.0	12.3	.	80	*10 ⁰⁰ 5 ⁰⁰ 9, 17-24 ⁰⁰ , ☐
23	8	05	05	08	06.0	10.3	.	75	*10 ⁰⁰ 12 ⁰⁰ 23-24 ⁰⁰ , ☐
24	8	09	08	10	09.0	05.5	.	70	*10 ⁰⁰ 3, ☐ 17 ⁰⁰ 24 ⁰⁰ V 20 ⁰⁰ 24 ⁰⁰ , *23-24 ⁰⁰ , ☐
25	9	00	03	01	01.3	11.3	03.8	65	V0-9, ☐ 0-24, *0-24, † 13 ⁰⁰ 15 ⁰⁰ 24 ⁰⁰ , F 18-24, ☐
26	8	10	10	10	10.0	01.1	00.7	59	F 0-24, ☐ 5 ⁰⁰ 12 ⁰⁰ 18 ⁰⁰ 24 ⁰⁰ , *5 ⁰⁰ 24 ⁰⁰ , † 21 ⁰⁰ 24 ⁰⁰ , † 16 ⁰⁰ 22 ⁰⁰ 24 ⁰⁰ , ☐
27	8	10	08	10	09.3	03.4	04.7	57	0-H ⁰⁰ 15-24 ⁰⁰ , 0-21 ⁰⁰ 17 ⁰⁰ 24 ⁰⁰ , † 18-19 ⁰⁰ F 0-24, † 8-24 ⁰⁰ , *2 ⁰⁰ 24 ⁰⁰ , ☐
28	8	10	08	10	09.3	04.7	03.4	52	F 0-24, ☐ 0-H ⁰⁰ , 0-3 ⁰⁰ 18 ⁰⁰ 24 ⁰⁰ , ☐ 17 ⁰⁰ 24 ⁰⁰ , † 20-20 ⁰⁰ , † 20 ⁰⁰ 24 ⁰⁰ , ☐
29	0	10	10	02	07.3	01.3	05.9	53	F 0-5, † 8 ⁰⁰ 24 ⁰⁰ , ☐ 0-17 ⁰⁰ , *0-6 ⁰⁰ VV 2-18, *2 ⁰⁰ 14 ⁰⁰ , ☐
30	9	04	04	00	02.7	11.9	02.3	52	F 0-24, ☐
M.		06.9	07.5	06.0	06.8	160.7	63.7		
VR.									

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 7h 13 min.$

BP. ST. 134

Dan	Vazdušni pritisak hPa			Temperatura vazduha T °C					Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)								
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	793.9	793.9	794.0	-03.6	-02.4	-03.6	-03.3	-02.3	-03.6	-	04.4	04.8	04.5	95	94	97	95	WSW	4	W	3	SW	5	
2	793.2	790.3	788.4	-04.2	-03.2	-03.0	-03.4	-03.0	-04.7	-	04.1	04.4	04.5	92	92	92	97	WSW	6	SSW	11	S	9	
3	784.0	785.2	787.4	-03.4	-02.9	-03.4	-03.3	-07.2	-03.6	-	04.4	04.6	04.4	93	94	93	93	S	10	S	7	SSW	6	
4	790.4	791.7	793.2	-04.4	-02.8	-02.5	-03.1	-02.0	-04.5	-	04.1	04.4	04.3	92	89	84	88	-	0	SSW	5	SW	7	
5	794.6	796.8	797.9	-02.5	-01.0	-01.5	-01.6	-00.4	-02.7	-	04.0	04.7	04.6	79	83	84	82	SW	9	SSW	7	SSW	8	
6	797.0	799.4	799.5	-01.8	-00.6	-00.8	-01.0	00.0	-02.1	-	04.6	04.9	04.9	87	84	85	85	SSW	10	SW	8	S	7	
7	798.1	798.3	797.6	-01.8	-00.1	-01.0	-01.0	00.3	-01.8	-	04.6	05.4	04.5	85	89	80	85	SSW	7	S	4	S	4	
8	797.3	797.9	791.6	-01.9	-01.3	-01.4	-01.4	-03.6	-02.0	-	04.1	04.3	04.5	77	75	81	78	S	3	NE	3	NE	1	
9	797.0	795.7	795.4	-02.2	-01.5	-05.0	-03.4	-01.3	-05.0	-	04.4	05.2	04.3	85	95	95	92	-	0	SSW	2	E	2	
10	793.9	793.5	792.4	-07.4	-04.2	-05.0	-05.4	-04.0	-07.4	-	03.3	04.1	03.9	93	92	91	92	E	2	S	3	S	3	
11	790.3	789.3	790.4	-04.4	-02.8	-02.8	-03.2	-07.6	-05.1	-	04.1	04.8	04.8	94	97	97	96	S	3	S	6	SSE	3	
12	791.0	792.8	793.9	-03.3	-01.3	-02.2	-02.3	01.2	-03.3	-	04.6	05.4	05.1	97	97	98	97	SSE	2	S	3	SSW	3	
13	791.9	790.7	786.3	-02.5	-00.3	-01.0	-01.2	00.2	-03.2	-	05.0	05.8	05.3	98	97	93	96	S	3	SSW	3	SSW	5	
14	784.3	782.1	780.8	-02.6	-02.3	-03.5	-03.0	-01.0	-03.5	-	04.8	05.0	04.5	94	96	95	95	S	5	S	6	S	6	
15	777.5	778.9	779.1	-03.8	-02.7	-03.2	-03.2	-02.6	-03.8	-	04.4	04.8	04.6	95	96	95	95	SSW	7	SSW	7	SSW	7	
16	778.9	778.0	777.7	-04.2	-04.5	-05.1	-04.7	-03.2	-05.2	-	04.2	04.1	04.0	94	94	95	94	S	7	S	7	SSE	7	
17	774.3	771.5	766.0	-05.8	-04.4	-06.6	-05.9	-04.0	-06.6	-	03.8	04.2	03.5	94	96	94	95	S	7	S	7	S	6	
18	767.8	767.9	767.5	-09.4	-06.2	-04.0	-05.9	-04.0	-09.4	-	02.8	03.7	04.4	93	96	96	95	SSE	6	SE	5	SE	5	
19	768.2	770.1	773.5	-06.6	-03.2	-03.4	-04.2	-03.0	-06.6	-	03.6	04.6	04.5	96	95	95	95	SSW	2	NNE	2	SW	1	
20	775.7	777.5	777.7	-05.2	-05.7	-04.7	-04.8	-03.4	-05.7	-	04.2	03.6	04.1	94	91	95	93	SSW	3	SSW	5	SSW	7	
21	776.7	774.8	776.4	-03.1	-02.0	-01.8	-02.2	-01.5	-05.6	-	04.6	05.1	05.1	95	96	95	95	SSW	8	S	7	SSE	7	
22	777.1	779.7	776.3	-01.8	-01.1	-01.5	-01.6	-03.9	-02.2	-	04.9	05.1	05.1	95	91	94	93	SSW	8	S	6	SSW	7	
23	777.1	779.0	779.9	-02.3	-01.5	-01.0	-01.5	-01.0	-02.3	-	04.9	05.1	05.4	94	94	94	94	SSW	3	SW	4	SW	3	
24	781.5	782.6	783.9	-02.8	-02.2	-02.5	-02.5	-01.0	-02.8	-	04.7	04.7	04.7	94	91	93	93	SW	4	SW	6	SW	5	
25	785.2	786.6	788.8	-03.7	-02.3	-03.1	-03.1	-02.1	-03.7	-	04.2	04.9	04.5	91	94	92	92	SSW	5	N	4	W	2	
26	788.6	787.9	787.7	-03.7	-03.8	-04.0	-03.9	-03.1	-04.1	-	04.2	04.3	04.1	91	93	91	92	S	4	SSW	5	SW	2	
27	786.1	784.2	782.0	-03.5	-00.3	-02.0	-02.0	-00.1	-04.0	-	03.6	03.3	03.2	76	55	60	64	NW	1	SSW	6	SSW	6	
28	778.7	779.9	782.0	-02.9	-02.4	-06.4	-04.5	-02.0	-06.4	-	04.6	04.8	03.6	94	94	94	94	SSW	7	SSW	7	N	5	
29	784.6	787.0	789.2	-11.7	-09.0	-09.0	-09.7	-06.4	-11.7	-	02.2	02.8	02.8	89	92	92	91	NE	7	NNE	5	NE	4	
30	789.9	790.7	791.9	-08.0	-04.6	-03.4	-04.9	-03.4	-09.6	-	02.6	02.6	02.0	77	60	43	60	NNE	6	NE	5	NE	5	
31	791.8	791.4	790.9	-00.4	-00.1	-00.2	-00.2	00.8	-03.4	-	01.8	02.6	02.7	30	43	45	39	SW	4	SSW	7	W	7	
M.																								
VR	785.7	786.0	786.3	-04.0	-02.6	-03.2	-03.3	-02.0	-04.7	-	04.0	04.4	04.3	89	88	88	88	4.9	5.4	5.0				

1	786.7	791.1	792.2	-03.0	-02.0	-02.6	-02.6	-00.1	-03.6	-	04.7	05.2	04.9	95	98	97	97	N	14	NNE	9	NNE	7
2	791.4	792.6	792.4	-01.8	03.0	02.6	01.6	03.2	-02.9	-	02.7	05.6	05.4	51	74	74	66	NE	8	NE	2	E	3
3	792.4	794.3	795.3	-02.0	-00.2	03.6	-00.3	02.6	-02.0	-	05.2	05.8	05.1	98	97	80	92	NE	6	NE	5	E	5
4	794.6	794.6	793.2	00.4	02.2	01.8	01.6	03.0	-00.6	-	04.7	05.5	05.1	74	76	73	74	SW	7	SW	8	SW	9
5	790.3	788.8	788.2	00.6	02.6	03.3	01.0	02.6	00.3	-	05.2	05.2	05.9	82	71	94	82	SW	9	SW	13	SW	13
6	783.3	787.0	785.2	-00.8	00.0	-00.5	-00.5	00.3	-00.8	-	04.6	05.9	05.7	81	97	97	92	SW	13	SW	11	SW	11
7	786.7	787.7	788.7	-00.4	-00.2	-00.9	-00.6	00.2	-01.6	-	05.7	05.8	05.3	97	97	92	95	SSW	7	W	7	WSW	7
8	787.1	785.0	784.4	-01.1	01.6	01.5	00.9	02.4	-01.6	-	05.0	05.7	06.1	89	83	90	87	SW	9	SW	11	SW	11
9	785.0	785.5	785.9	01.6	04.2	05.1	04.0	05.2	01.4	-	06.3	06.4	05.3	91	78	61	77	SW	10	WSW	9	SW	10
10	786.1	786.3	786.6	05.3	06.3	04.0	04.9	06.4	04.0	-	05.9	05.7	06.8	66	59	84	70	SW	10	SSW	7	SSW	6
11	788.2	788.2	787.4	-01.5	02.3	-00.9	-00.3	04.0	-01.5	-	04.3	04.4	05.4	78	62	93	78	NW	2	SW	3	SSW	5
12	781.9	779.9	775.8	-03.2	-03.0	-04.1	-03.6	-00.9	-04.1	-	04.6	04.4	04.1	95	90	91	92	SSW	8	S	10	SE	4
13	775.8	782.6	784.3	-06.2	-04.3	-03.4	-04.3	-03.4	-06.5	-	03.6	04.1	04.4	94	92	91	92	NNE	9	NNW	3	SW	3
14	784.8	783.8	783.9	-03.7	-02.4	-03.8	-03.4	-01.4	-04.0	-	04.2	04.7	04.3	91	91	93	92	SSW	2	S	8	S	8
15	784.7	786.7	787.7	-02.3	-00.8	-03.6	-02.6	-00.8	-03.9	-	04.9	05.7	04.5	94	99	97	97	S	3	S	2	NE	3
16	787.0	787.5	788.4	-04.7	-05.0	-05.0	-04.9	-03.6	-05.2	-	04.2	04.0	04.0	97	95	95	96	NE	6	NNE	8	NE	8
17	785.7	784.2	785.2	-04.7	-05.0	-04.4	-04.6	-04.4	-05.3	-	04.1	04.1	04.3	95	97	98	97	NNE	9	NE	10	NE	8
18	786.6	787.7	788.0	-03.4	-02.6	-02.4	-02.7	-02.0	-04.4	-	04.6	04.9	05.0	97	97	98	97	NE	6	NE	7	ENE	6
19	787.8	788.0	788.0	-02.7	-01.5	-02.4	-02.3	-01.2	-02.9	-	04.9	05.4	05.3	97	99	98	98	ENE	6	VE	6	NE	6
20	787.3	787.7	788.6	-02.4	-01.4	-01.5	-01.7	-01.3	-03.2	-	04.9	05.3	05.1	96	95	94	95	NE	3	E	2	E	2
21	788.8	791.0	792.3	-02.1	-00.3	-00.3	-00.8	00.2	-02.3	-	04.4	04.9	04.9	85	81	83	83	ENE	2	E	1	-	0
22	792.6	792.4	789.9	-00.1	01.3	01.7	01.2	01.8	-00.6	-	04.8	05.3	05.1	78	80	74	77	N	4	SW	2	SW	2
23	786.0	785.0	784.3	00.4	02.1	00.4	00.8	02.2	-00.2	-	04.6	05.1	04.9	73	72	76	74	SW	4	SW	4	SSW	2
24	783.8	784.3	785.0	03.3	02.7	-01.5	00.0	03.0	-01.5	-	04.6	05.5	05.0	74	74	92	80	W	2	SW	4	SW	2
25	786.3	788.4	788.6	-04.6	-01.4	-00.7	-01.9	-00.2	-07.7	-	04.2	02.2	03.4	96	90	58	65	N	3	WSW	2	SW	6
26	787.3	785.1	784.4	00.4	02.1	01.3	01.3	02.6	-00.7	-	06.0	06.7	06.4	95	94	96	95	SW	7	SSE	6	S	5
27	784.4	784.4	783.9	00.9	01.9	01.1	01.3	02.0	00.9	-	06.1	05.9	05.9	94	84	90	89	SSW	4	SW	6	SW	7
28	778.3	778.3	777.0	01.0	02.2	02.7	01.9	02.6	00.7	-	05.9	06.1	06.2	90	86	87	88	SSW	10	SSW	8	SSW	8
29	774.4	777.6	780.8	-08.5	-08.5	-08.5																	

$\varphi = 43^{\circ}43' N$ $\lambda = 18^{\circ}16' E$ Gr. $\Delta G = + 1h 13 min.$

Pr. ST. 134

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T C°						Napon vodene pare hPa			Relativna vlažnost u%				Pravac i jačina vetra D, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	786.0	787.3	787.3	-02.0	-00.1	-00.8	-00.9	03.7	-04.4	-	05.1	05.7	05.7	96	94	99	96	SW	9	SW	8	SW	7	
2	783.9	780.4	780.8	-00.2	00.4	01.1	00.6	01.1	-01.9	-	06.0	06.3	06.3	100	100	95	98	SW	12	SSW	14	SSW	12	
3	777.7	778.9	781.0	00.9	02.3	00.5	01.1	02.8	00.5	-	06.5	07.2	06.3	100	100	100	100	SSW	11	SSW	9	-	0	
4	782.6	784.6	784.8	-01.0	02.2	01.4	01.0	02.6	-01.2	-	05.7	07.2	06.3	100	100	100	100	-	0	S	4	S	7	
5	784.4	785.2	787.1	01.9	03.7	03.8	03.3	04.2	00.4	-	07.0	08.0	07.2	100	100	89	96	S	8	S	6	S	6	
6	785.1	784.0	783.4	02.8	04.5	04.3	04.0	04.8	02.8	-	07.5	08.4	08.3	100	100	100	100	NE	2	S	4	SSE	6	
7	782.0	783.7	787.5	03.7	01.6	-00.6	01.0	04.3	-00.6	-	08.0	06.9	05.9	100	100	100	100	SSE	5	SSE	10	SE	6	
8	787.9	790.3	789.7	-00.6	00.2	00.2	00.0	00.3	-00.6	-	05.9	06.2	06.2	100	100	100	100	SSE	7	S	6	S	7	
9	789.0	788.6	788.3	00.6	01.6	01.2	01.2	02.1	00.2	-	06.4	06.9	06.7	100	100	100	100	S	6	SSE	5	S	3	
10	788.0	789.2	789.6	00.8	03.4	03.5	02.8	04.8	00.2	-	06.5	07.5	07.3	100	96	93	96	NNE	7	ENE	2	ENE	2	
11	789.6	790.0	791.5	03.4	06.0	05.9	05.3	06.8	03.4	-	07.6	09.0	08.5	97	96	91	95	E	2	NE	2	E	1	
12	792.3	794.1	795.5	07.0	10.9	08.9	08.9	11.0	05.2	-	08.1	07.9	08.8	81	60	77	73	N	2	NE	1	NNE	2	
13	795.4	795.4	794.4	09.1	11.8	10.2	10.3	12.1	08.6	-	06.9	06.9	08.4	60	50	67	59	NNE	4	NNE	1	SSE	4	
14	792.0	792.7	791.7	09.8	12.3	09.7	10.4	12.6	08.6	-	05.9	08.7	06.3	40	61	52	54	SW	6	S	4	S	6	
15	791.0	791.3	791.3	09.3	11.9	08.0	09.3	12.7	08.0	-	05.6	07.8	08.2	48	56	76	60	S	4	NE	1	NNE	4	
16	791.1	792.2	792.8	07.0	08.8	07.3	07.6	09.2	05.1	-	07.5	09.8	08.8	74	87	86	82	NNE	4	NNE	2	-	0	
17	793.6	795.0	795.7	08.2	12.4	07.8	09.1	12.5	06.7	-	08.2	07.2	09.2	75	50	87	71	WSW	3	WSW	3	W	5	
18	795.7	796.7	796.4	08.7	11.2	06.7	08.3	11.2	06.7	-	06.2	10.0	08.9	55	76	90	74	SW	5	SSW	5	SSW	6	
19	795.3	796.4	796.4	06.0	09.6	07.4	07.6	09.7	05.6	-	09.1	09.6	09.4	97	80	92	90	SSW	7	SW	6	SW	5	
20	795.7	795.4	795.0	07.2	13.0	09.2	09.7	13.2	06.0	-	09.8	09.6	10.2	96	64	88	83	WNW	4	SW	3	SSW	2	
21	791.8	790.1	789.2	08.6	12.3	08.8	09.6	12.7	07.5	-	09.1	09.0	08.8	81	63	78	74	SW	6	SSW	6	SSW	5	
22	786.1	787.0	786.0	05.5	08.1	06.1	06.5	08.8	05.5	-	08.9	09.7	08.4	99	90	89	93	SSW	7	SSW	6	SSW	7	
23	787.7	789.2	789.9	05.4	09.2	06.9	07.1	09.2	04.4	-	07.5	07.8	08.2	84	67	82	78	SSW	3	S	5	SSW	5	
24	792.9	793.9	794.7	07.3	09.9	07.5	08.0	10.3	05.2	-	08.3	07.9	09.3	82	65	89	79	NW	3	SW	2	ENE	1	
25	795.4	796.7	796.7	08.0	09.3	06.1	07.4	11.4	06.1	-	09.6	10.2	09.1	90	87	96	91	E	1	NE	2	ESE	2	
26	794.9	795.1	795.3	06.0	09.0	06.0	06.8	09.3	05.0	-	08.8	10.1	09.4	94	88	100	94	E	3	NE	2	NE	2	
27	795.0	795.9	796.3	07.2	10.3	08.0	08.4	11.0	05.3	-	09.3	07.9	08.5	92	63	79	78	ESE	2	NE	2	SSE	1	
28	795.7	795.3	794.9	09.17	11.7	08.3	09.4	11.4	07.5	-	07.9	07.9	09.3	65	59	85	70	NNE	3	NNE	3	NNE	3	
29	793.0	792.6	792.2	07.6	09.7	06.8	07.7	09.8	06.5	-	09.3	09.8	08.3	90	82	81	84	NE	2	WSW	3	NE	2	
30	791.4	792.3	793.0	05.2	06.6	04.7	05.3	07.4	04.5	-	08.7	09.7	08.4	99	100	99	99	NE	3	NE	4	NE	7	
31	793.0	793.9	793.7	03.4	07.0	04.4	04.8	07.1	03.4	-	07.8	08.7	08.1	100	87	97	95	NE	8	NNE	5	N	6	
M.																								
VR	792.2	790.8	791.0	05.0	07.4	05.5	05.8	08.0	03.9	-	07.6	08.2	08.0	87	81	89	86	4.8	4.4	4.3				

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1	792.8	793.2	793.5	03.6	04.4	02.2	03.1	04.9	02.2	-	07.9	08.4	07.2	100	100	100	100	N	9	N	8	N	8
2	792.6	793.6	793.7	03.2	06.8	05.4	05.2	07.0	02.2	-	07.7	08.5	08.5	100	86	95	94	N	9	NNE	5	NNE	4
3	793.5	794.0	794.9	04.8	06.6	04.6	05.2	07.0	04.6	-	08.3	09.3	08.5	96	95	100	97	N	4	N	6	N	6
4	794.6	795.9	796.4	04.4	06.5	06.7	06.1	07.0	03.7	-	08.4	09.7	09.7	100	100	99	100	NE	5	NE	4	NE	3
5	796.6	797.3	797.2	08.8	10.7	09.3	09.5	11.3	05.6	-	08.6	10.1	09.4	76	78	80	78	SSW	2	NE	1	W	2
6	797.8	797.9	797.5	09.9	13.5	10.8	11.3	13.7	08.7	-	08.7	10.4	10.1	71	67	78	72	-	0	NW	2	W	2
7	797.3	797.3	796.2	12.4	16.1	11.9	13.1	16.3	10.7	-	08.4	10.5	09.5	58	58	68	61	W	5	SSW	4	SSW	6
8	793.3	792.0	791.3	10.1	12.7	08.8	10.1	12.8	08.3	-	09.4	11.1	10.8	76	76	95	82	SSW	7	SSW	7	SSW	6
9	791.5	793.3	794.9	06.2	08.2	05.8	06.5	08.8	05.2	-	07.4	08.1	08.3	78	74	90	81	SSW	6	SW	6	SW	5
10	794.9	793.9	791.4	05.6	09.2	04.4	05.9	09.4	04.4	-	08.4	08.6	07.1	92	74	84	83	SW	5	SSW	6	SSW	8
11	791.1	791.3	791.1	04.7	03.3	00.5	02.2	04.7	00.5	-	07.6	07.4	06.3	88	97	100	95	SSW	3	WSW	1	NNE	3
12	791.0	792.0	791.0	00.4	06.9	05.0	04.3	07.9	-01.7	-	05.5	06.1	06.5	87	61	75	74	E	3	SW	4	SSW	4
13	789.7	791.7	792.2	04.9	06.8	06.2	06.0	07.8	03.8	-	06.5	09.4	07.0	75	95	74	81	SSW	7	SSW	8	SW	6
14	793.3	795.1	795.5	07.1	11.0	08.8	08.9	12.2	06.0	-	09.6	10.4	09.7	95	80	85	87	SW	6	SW	5	SW	6
15	792.4	790.6	793.2	09.8	14.2	08.8	10.4	14.6	08.6	-	09.3	10.0	10.2	77	62	90	76	SSW	10	SW	8	N	2
16	793.0	793.5	793.1	01.7	08.6	08.4	06.8	09.6	01.2	-	06.9	10.9	10.4	100	98	94	97	NE	6	SW	2	SW	6
17	789.5	784.8	785.5	08.0	09.0	-00.8	03.9	09.5	-00.8	-	10.0	10.5	05.7	93	91	98	94	N	9	S	10	N	7
18	787.8	790.0	790.3	-01.8	00.6	00.3	-00.2	01.1	-02.1	-	05.3	06.3	06.0	98	98	95	97	NNE	8	VE	5	N	7
19	789.2	791.9	791.5	-02.2	04.0	04.8	02.9	05.7	-02.2	-	05.1	05.1	05.5	98	63	64	75	N	9	N	1	SW	2
20	789.0	787.0	786.7	08.8	04.8	03.6	05.2	08.8	03.6	-	05.6	07.3	07.6	50	85	96	77	SSW	4	SSW	5	NW	1
21	785.2	788.6	790.0	01.8	01.2	01.4	01.5	03.6	00.6	-	06.8	06.7	06.5	97	100	96	98	N	5	N	7	N	8
22	792.8	793.1	790.4	05.8	10.3	06.6	07.3	11.0	01.1	-	06.2	09.0	08.5	68	72	87	76	N	2	SSW	3	SW	7
23	788.4	787.8	788.3	03.8	05.5	04.1	04.4	06.6	03.7	-	07.6	08.9	07.3	95	99	89	94	SW	4	SW	7	SW	7
24	788.6	788.7	790.3	02.3	04.4	04.1	04.0	06.0	02.3	-	06.9	07.6	07.1	96	85	87	89	NW	4	NNE	3	NNW	5
25	791.0	794.6	795.5	04.2	07.6	05.3	05.6	07.6	02.4	-	07.4	08.6	08.0	89	83	90	87	NNW	6	W	3	N	5
26	796.6	796.3	798.4	02.8	08.4	08.0	06.8	09.2	02.8	-	06.9	09.8	09.0	93	89	84	89	NNE	5	N	1	WSW	3
27	796.0	796.0	795.1	10.3	12.2	08.6	09.9	12.7	07.1	-	05.9	11.4	10.0	47	80	90	72	SW	7	SW	5	S	5
28	792.4	792.7	794.0	06.0	07.4	07.0	07.1	08.6	06.7	-	09.4	08.9	09.3	95	86	89	90	S	2	WSW	3	W	4
29	795.5	797.8	797.3	03.0	07.7	06.4	05.9	08.4	02.5														

Razvojni elementi								D	R	P	S	M	M	M	M	M	M	
1	2	3	4	5	6	7	8											
1	8	10	06	10	08.7	04.0	.	50										
2	2	10	10	10	10.0	01.3	.	49										
3	7	10	10	10	10.0	00.0	.	46										
4	4	05	10	10	08.3	01.3	17.8	43										
5	7	10	09	08	09.0	03.8	.	39										
6	0	10	10	10	10.0	00.0	04.2	33										
7	0	10	10	10	10.0	00.0	08.4	27										
8	8	10	10	10	10.0	01.8	18.4	30										
9	1	10	10	10	10.0	00.0	00.3	29										
10	8	10	08	08	08.7	05.8	06.7	27										
11	8	10	09	00	06.3	05.2	00.1	26										
12	9	02	05	00	02.3	07.0	00.0	25										
13	8	02	09	03	04.7	10.3	.	22										
14	8	04	08	04	05.3	09.3	.	19										
15	8	08	09	04	07.0	09.5	.	16										
16	8	09	08	04	07.0	04.3	00.3	12										
17	8	01	05	04	02.3	09.4	13.8	.										
18	8	01	08	00	03.7	11.8	04.1	.										
19	8	09	04	04	07.3	04.4	.	.										
20	8	07	08	05	06.7	08.2	.	.										
21	8	05	06	09	06.7	07.7	02.5	.										
22	8	10	09	10	09.7	05.0	07.1	.										
23	8	10	06	00	05.3	09.2	03.8	.										
24	8	02	09	08	06.3	05.5	.	.										
25	8	02	10	10	07.3	06.9	.	.										
26	8	06	08	10	08.0	06.8	02.0	.										
27	8	00	01	00	00.3	13.5	06.6	.										
28	8	00	06	05	03.7	08.7	.	.										
29	8	02	09	05	05.3	05.7	00.7	.										
30	1	10	10	10	10.0	01.5	00.1	.										
31	8	10	08	10	09.3	04.3	02.0	.										
N.																		
VR.	06.6	08.2	06.5	07.1	172.2	98.9												

F. #0-24 \equiv $6^{\circ} 13^{\circ} 18^{\circ} 24^{\circ} VC^{\circ} 13^{\circ}$
F. #0-24 \equiv $0-24, V 1-7^{\circ}$
F. #0-19 \equiv $0-24, 10^{\circ} 20^{\circ}, H^{\circ} 13^{\circ}, 19^{\circ} 20^{\circ}, 14^{\circ} 13^{\circ}, 19^{\circ} 23^{\circ}$
 \equiv $0-21, F. #19-24$
 \equiv $0-13^{\circ}, F. #0-24, 17^{\circ} H^{\circ}, 10^{\circ} H^{\circ}$
F. #0-3 \equiv $3^{\circ} 14^{\circ} \equiv 5^{\circ} 24^{\circ}$
F. #0-24 \equiv $0-24, 0^{\circ} 14^{\circ}, 14^{\circ}, 14^{\circ}, 14^{\circ}, 23^{\circ}, 18^{\circ}, 22^{\circ}, V 19-24$
 \equiv $0-24, F. #0-24, 10^{\circ} 20^{\circ}, 2^{\circ} 10^{\circ}$
 \equiv $0-23, F. #0-17, 2^{\circ} 10^{\circ}, 15^{\circ}, 17^{\circ}$
 \equiv $2-10^{\circ}, 17^{\circ}, 2^{\circ}, 13^{\circ}$
 \equiv $0-11^{\circ}, 17^{\circ}, 20^{\circ}, 2^{\circ}, 3^{\circ}, 17^{\circ}, 17^{\circ}, 19^{\circ}, 19^{\circ}, 3-5^{\circ}$
F. #2 \equiv 24°
F. #0-24 \equiv 24°
F. #0-24 \equiv $22^{\circ}, 24^{\circ}, 16^{\circ}, 19^{\circ}, 17^{\circ}, 19^{\circ}, 23^{\circ}, 24^{\circ}, 19^{\circ}, 23^{\circ}, 22^{\circ}, 24^{\circ}$
 \equiv $0-2^{\circ}, 0-1^{\circ}, 7^{\circ}, 15^{\circ}, 18^{\circ}, 0-2^{\circ}, 16^{\circ}, 16^{\circ}, 15^{\circ}, 15^{\circ}, 16^{\circ}, 16^{\circ}$
 \equiv $15^{\circ}, 16^{\circ}, 19-19^{\circ}, 16^{\circ}, 16^{\circ}, 19^{\circ}, 15^{\circ}, 15^{\circ}, 15^{\circ}$
F. #4 \equiv 24°
F. #0-23
 \equiv $3-5, 20-24, 1^{\circ}, 5^{\circ}, 15^{\circ}, 15^{\circ}, 15^{\circ}, 15^{\circ}$
F. #0-20, 23 \equiv $24, 2^{\circ}, 2^{\circ}, 2^{\circ}, 2^{\circ}, 2^{\circ}$
F. #0-24 \equiv $3^{\circ}, 10^{\circ}, 20^{\circ}, 23^{\circ}, 6^{\circ}, 11^{\circ}, 8^{\circ}, 13^{\circ}$
 \equiv $0-24, 5^{\circ}, 20-24$
 \equiv $0-24, 0-1, 19^{\circ}, 24^{\circ}$
 \equiv $0-0, 5^{\circ}, 14^{\circ}, 7^{\circ}, 2^{\circ}, 19^{\circ}, 13^{\circ}, 15^{\circ}, 20^{\circ}, 24^{\circ}, 15^{\circ}, 17^{\circ}, 15^{\circ}, 17^{\circ}$
 \equiv $0-2^{\circ}, 16^{\circ}, 18^{\circ}, 19^{\circ}, 19^{\circ}, 10^{\circ}, 6^{\circ}, 11^{\circ}, 16^{\circ}, 19^{\circ}, 23^{\circ}, 24^{\circ}, 16^{\circ}, 16^{\circ}$
 \equiv $0-5^{\circ}, 10^{\circ}, 2^{\circ}, 19^{\circ}, 16^{\circ}, 16^{\circ}, 16^{\circ}$
 \equiv $21-22, 17, 22^{\circ}, 24^{\circ}, 23^{\circ}, 24^{\circ}$
 \equiv $16-25, 10^{\circ}, 13^{\circ}, 0-1^{\circ}, 1^{\circ}, 1^{\circ}, 1^{\circ}, 13^{\circ}, 14^{\circ}, 16^{\circ}, 16^{\circ}, 16^{\circ}$
 \equiv $2^{\circ}, 24^{\circ}, 5^{\circ}, 27^{\circ}, 15^{\circ}, 13^{\circ}, F. #6-24$
 \equiv $0-10^{\circ}, 16-24, F. #0-24, 4-5^{\circ}$

1	1	10	10	10	10.0	10.4	01.2	.										
2	8	10	06	10	08.7	05.0	07.2	.										
3	1	10	10	10	10.0	01.5	03.4	.										
4	2	10	10	10	10.0	00.6	04.6	.										
5	8	00	09	00	03.0	06.2	.	.										
6	8	00	08	00	02.7	12.5	00.2	.										
7	8	06	05	02	04.3	12.0	.	.										
8	8	09	08	10	09.0	06.9	.	.										
9	8	10	05	03	06.0	04.7	11.8	.										
10	8	10	04	03	04.7	08.9	04.1	.										
11	9	10	10	10	10.0	10.0	00.4	.										
12	9	00	06	00	02.0	11.3	03.0	.										
13	8	01	09	01	03.7	06.9	.	.										
14	8	10	06	03	06.3	06.3	.	.										
15	8	06	06	10	07.3	08.0	07.0	.										
16	2	10	10	10	10.0	03.6	07.7	.										
17	3	10	10	10	10.0	01.4	.	.										
18	8	10	09	00	06.3	06.1	24.4	.										
19	8	10	04	08	07.3	06.2	.	.										
20	8	10	10	10	10.0	00.7	.	.										
21	0	10	10	00	06.7	01.1	26.2	.										
22	8	00	06	10	05.3	03.9	.	.										
23	1	10	10	05	06.3	00.2	.	.										
24	2	09	10	08	09.0	04.5	14.6	.										
25	2	04	10	10	08.0	04.7	.	.										
26	9	10	08	00	06.0	05.2	.	.										
27	8	02	08	10	06.7	11.7	.	.										
28	1	10	10	00	06.7	06.8	.	.										
29	8	00	06	02	07.3	11.1	02.1	.										
30	9	00	07	09	00.7	14.2	.	.										
N.																		
VP.	06.9	07.9	05.4	06.7	181.9	126.8												

φ = 43°43' N λ = 18°18' E Op. Δ0 = + 1h 13 min.

BR. ST. 134

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T °C						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina veta- ro, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	797.9	796.8	794.9	11.4	13.0	09.4	10.8	13.5	09.0	-	08.7	08.1	09.5	64	54	81	66	SW	4	SSW	6	SW	7	
2	794.3	794.1	793.6	09.0	11.8	04.6	07.5	12.0	04.6	-	07.6	10.4	08.5	66	75	100	80	N	6	S	3	N	11	
3	793.9	797.2	797.2	01.6	05.1	03.6	03.5	05.4	01.6	-	06.9	07.7	07.7	100	87	97	95	N	10	N	7	N	8	
4	797.6	798.6	798.1	02.7	07.0	05.6	05.2	07.4	02.2	-	07.4	07.9	07.7	100	79	85	88	N	6	NNE	6	N	4	
5	795.7	795.4	795.3	05.6	08.6	05.4	06.3	09.1	04.3	-	07.7	08.4	07.8	85	76	87	83	N	3	NNE	4	N	5	
6	794.1	795.0	795.7	04.4	05.9	05.0	05.1	06.7	03.7	-	07.9	08.0	08.4	95	86	96	92	NE	6	NNE	5	NNE	5	
7	795.4	797.2	797.6	03.7	08.0	05.2	05.5	08.2	03.2	-	08.0	07.5	07.6	100	70	86	85	N	9	NNE	8	N	7	
8	797.9	798.1	796.8	05.9	10.4	08.2	08.2	10.5	04.8	-	09.2	08.5	08.2	99	67	75	80	N	7	N	1	SW	6	
9	795.3	795.4	795.3	07.0	10.4	08.6	08.7	10.5	06.0	-	09.9	11.3	10.4	99	89	93	94	SW	6	WSW	4	SW	4	
10	794.1	793.9	794.4	08.0	07.5	07.2	07.5	09.0	07.0	-	09.0	09.9	09.4	84	95	93	91	SW	6	W	2	NNW	2	
11	794.6	795.4	796.4	04.4	05.7	05.9	05.5	07.2	04.4	-	08.3	09.0	09.2	99	99	99	99	N	4	NNE	4	NNE	2	
12	797.1	798.7	798.4	04.3	08.0	06.8	06.5	08.4	04.2	-	08.2	09.6	08.7	99	90	88	92	NNE	4	NNE	2	NNE	4	
13	798.4	800.4	800.7	06.1	09.3	07.5	07.6	09.6	05.6	-	08.8	09.4	09.4	94	80	91	88	NE	2	NE	2	NE	2	
14	800.0	800.3	800.6	06.8	10.2	09.0	08.8	11.3	05.4	-	09.4	09.9	10.1	95	80	88	88	NNE	3	NE	2	E	1	
15	797.8	800.6	800.3	09.7	13.2	11.8	11.6	13.8	07.3	-	09.7	08.5	09.5	81	56	68	68	-	0	NE	2	-	0	
16	800.6	801.2	801.2	11.6	14.2	13.0	13.0	15.0	10.0	-	10.8	11.8	11.9	79	73	80	77	NNE	5	NE	2	SW	3	
17	801.0	801.5	800.8	14.0	15.0	12.0	13.3	15.3	11.0	-	12.8	13.5	09.4	80	79	67	75	MNW	5	NNE	4	SSW	4	
18	799.3	798.7	798.0	12.4	15.8	13.3	13.7	15.8	11.8	-	11.7	10.7	12.0	81	60	79	73	WSW	3	SW	2	SSW	3	
19	796.2	796.8	797.1	12.8	14.0	13.9	13.7	15.3	10.8	-	10.4	11.8	11.9	70	74	75	73	HNN	2	N	1	-	0	
20	797.1	797.6	797.6	14.2	17.9	14.7	15.4	18.1	12.0	-	13.0	12.2	12.2	80	60	73	71	-	0	WSW	2	SW	3	
21	793.6	799.0	800.2	14.2	16.7	11.8	13.6	17.0	11.8	-	12.7	16.3	12.8	79	86	93	86	SW	5	S	5	N	4	
22	800.8	801.7	801.2	03.7	08.2	06.3	06.1	11.8	01.4	-	06.2	07.7	08.1	77	71	85	78	NE	7	NE	6	NNE	6	
23	800.2	801.2	801.7	09.9	12.6	11.2	11.2	13.2	06.3	-	03.4	10.1	09.8	28	69	74	57	NE	7	NNE	5	NNE	3	
24	801.3	801.7	801.0	11.6	14.8	12.1	12.7	15.0	10.2	-	08.1	11.0	12.0	59	65	85	70	E	2	NNE	2	NNW	2	
25	799.4	799.7	799.4	11.9	14.2	12.8	12.9	15.0	09.9	-	11.8	11.3	12.4	85	70	84	80	N	3	NNE	4	-	0	
26	797.5	798.0	797.9	11.8	15.0	14.2	13.8	15.2	10.8	-	09.7	10.7	12.1	70	63	75	69	N	6	N	3	NW	2	
27	797.6	798.3	798.3	15.6	20.1	15.9	16.9	20.2	13.0	-	06.2	11.6	09.5	35	50	53	46	NNE	2	S	3	S	5	
28	798.1	798.9	798.6	15.5	18.2	16.0	16.4	19.6	14.4	-	10.6	10.4	11.3	60	50	62	57	NNW	4	-	0	SW	4	
29	797.7	796.7	795.3	16.0	19.0	14.2	15.9	19.2	14.2	-	11.3	11.5	07.7	62	52	47	54	SW	6	SSW	9	SSW	9	
30	795.3	796.4	796.3	14.6	19.6	15.7	16.4	19.8	12.9	-	08.0	08.5	06.2	48	37	35	40	SSW	9	SSW	8	SSW	9	
31	794.6	793.9	793.6	13.9	17.8	14.4	15.1	18.7	13.6	-	07.3	07.6	07.8	46	37	47	43	SSW	8	SSW	10	SSW	6	
M.																								
VR	797.3	798.0	797.9	09.5	12.5	10.2	10.6	13.1	08.0	-	09.0	10.0	09.6	77	70	79	75		4.8		4.0		4.2	

1	793.7	795.3	794.7	07.4	12.4	13.0	11.5	13.1	07.2	-	08.7	10.1	09.0	85	70	60	72	N	5	NNE	2	SSW	3
2	794.4	794.3	795.5	12.6	09.5	07.3	09.2	13.2	07.3	-	06.5	09.6	10.0	45	81	98	75	SSW	5	SSW	3	NNE	7
3	795.5	796.8	796.0	04.0	09.8	11.0	09.0	11.4	03.4	-	07.0	08.5	08.6	87	70	66	74	NNE	8	NNE	3	NW	4
4	794.0	793.3	794.3	11.7	14.0	08.5	10.7	14.1	08.5	-	06.9	09.0	10.6	50	56	95	67	NW	4	SW	5	N	4
5	794.1	795.5	794.9	09.7	15.0	14.4	13.4	16.3	06.2	-	05.5	06.0	08.5	46	35	52	44	NNE	4	NE	2	SSW	6
6	792.8	789.9	786.0	13.5	18.6	12.5	14.3	18.7	11.4	-	08.6	10.9	06.7	56	51	46	51	SSW	7	S	11	S	11
7	781.9	784.3	784.7	05.8	06.0	00.7	03.3	12.5	00.7	-	09.0	07.9	06.3	97	84	98	93	S	3	SSW	6	N	11
8	788.6	791.7	792.4	02.4	04.2	04.6	03.5	04.6	00.0	-	06.2	05.8	06.1	98	70	72	80	N	8	NNW	7	SW	2
9	791.7	792.7	793.1	05.0	08.8	06.9	06.9	09.6	04.6	-	07.0	08.6	09.4	80	76	94	83	N	7	SW	2	SW	5
10	794.3	796.3	798.7	08.8	13.0	10.1	10.5	13.0	06.2	-	07.5	11.1	09.6	67	74	78	73	WSW	3	SW	5	-	0
11	797.9	801.5	801.3	10.7	15.0	13.0	12.9	15.4	09.9	-	05.0	10.0	09.0	39	59	60	53	N	4	-	0	N	2
12	801.2	802.3	802.0	13.0	16.3	14.3	14.5	17.0	11.4	-	10.1	11.0	11.8	68	59	72	66	NE	2	-	0	E	2
13	801.7	802.3	802.6	15.4	17.3	14.6	15.5	17.8	13.8	-	05.1	08.7	08.2	22	44	50	41	ENE	3	E	2	-	0
14	802.3	802.4	802.9	14.1	18.2	14.6	15.4	18.2	12.0	-	05.5	08.7	12.5	34	42	75	50	E	3	E	3	E	3
15	802.0	802.0	801.5	15.1	16.9	14.7	15.4	17.4	13.7	-	12.7	12.4	09.6	74	65	58	66	-	0	NE	3	-	0
16	799.9	799.8	798.9	13.8	16.2	14.8	14.9	17.0	13.0	-	09.7	10.8	11.0	62	59	65	62	ENE	2	E	2	E	2
17	798.0	797.5	797.0	14.8	17.4	14.8	15.5	17.7	13.6	-	09.7	10.6	10.8	58	53	64	58	-	0	NE	2	S	4
18	796.2	796.0	796.4	13.4	15.8	13.0	13.8	16.0	13.0	-	10.6	13.3	10.0	69	74	67	70	SW	5	SSW	3	SSW	5
19	795.7	797.3	797.1	08.8	15.6	12.8	12.8	16.2	08.8	-	06.0	07.7	09.1	53	43	61	52	NW	5	SW	4	SW	5
20	797.8	797.9	798.7	11.6	13.1	11.4	11.9	14.2	11.4	-	12.1	12.7	11.0	89	84	82	85	NNE	5	NNE	3	NNE	2
21	798.9	800.8	800.6	07.0	11.7	09.4	09.4	12.2	06.5	-	09.4	09.7	09.6	94	70	81	82	NNE	7	NNE	6	N	6
22	800.8	801.7	801.3	13.2	18.0	15.7	15.7	18.1	09.4	-	09.0	08.8	09.2	59	43	52	51	ENE	2	ENE	2	S	3
23	803.2	800.6	800.8	15.2	19.6	14.0	15.7	19.6	14.0	-	08.6	09.4	11.8	50	41	74	55	S	2	N	2	NNE	4
24	799.5	799.7	799.4	14.5	19.1	15.6	16.2	19.3	13.1	-	11.7	07.3	08.2	71	33	46	50	SSW	3	S	3	S	5
25	797.7	798.7	797.7	13.9	18.5	14.3	15.3	18.6	12.1	-	05.3	10.3	08.8	33	48	54	45	SSW	4	S	4	SW	9
26	796.0	795.1	792.0	13.7	18.6	11.0	13.6	19.0	11.0	-	09.4	11.2	11.6	60	52	89	67	SW	7	S	6	SSE	7
27	789.6	789.0	789.0	07.2	02.2	02.6	03.7	11.0	02.0	-	09.3	07.0	07.2	92	97	97	95	NNE	2	N	7	NNE	7
28	786.6	788.8	790.4	02.0	03.0	04.1	03.3	04.1	02.0	-	07.1	07.4	08.2	100	97	100	99	NNE	11	NNE	11	NNE	11
29	788.7	790.1	792.6	03.2	03.6	05.0	04.2	05.0	03.2	-	07.6	07.9	08.7	99									

$\varphi = 43^{\circ}43' N$ $\lambda = 16^{\circ}16' E$ Gr. $\Delta G = + 1h 13min.$

BR. ST. 134

Dan	Vazdušni pritisak PhPa			Temperatura vazduha T C°						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)				
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21	
1	797.3	797.9	797.5	09.2	13.2	10.9	11.1	14.2	06.8	-	09.3	10.0	09.2	80	66	70	72	SSW 3	SSW 2	SW 2	
2	797.5	798.9	799.9	09.7	12.5	10.7	10.9	12.7	09.3	-	09.8	11.5	10.3	82	79	80	80	NNE 3	NNE 2	- 0	
3	799.3	799.3	797.1	10.0	13.6	10.7	11.3	13.8	09.6	-	09.8	10.5	09.4	80	67	73	73	SSW 5	SW 6	SSW 9	
4	796.7	796.4	796.6	10.3	01.9	02.8	04.5	10.7	01.7	-	10.4	06.7	26.5	83	96	87	89	SSW 9	W 5	NNE 7	
5	796.8	797.6	796.0	02.0	04.4	04.8	04.0	05.1	01.2	-	06.8	07.2	06.4	96	86	74	85	NNE 8	NNE 4	NNE 8	
6	795.9	795.5	795.5	08.7	12.4	09.2	09.9	12.5	04.8	-	08.5	09.9	10.2	76	69	88	78	SW 5	SW 4	SW 3	
7	795.7	795.8	795.5	-01.5	03.0	02.8	01.8	09.2	-02.2	-	05.0	06.4	05.7	92	85	76	84	NNE 7	NNE 3	N 2	
8	794.9	794.9	793.5	04.0	10.3	08.2	07.7	10.6	02.2	-	03.2	05.3	06.0	39	42	55	45	NNE 2	SSW 4	SSW 4	
9	791.3	791.1	791.9	06.5	07.0	-00.2	03.3	08.3	-00.2	-	07.3	07.9	05.9	75	79	98	84	SW 5	W 2	NNE 6	
10	791.9	795.3	797.9	-02.6	-00.2	-00.3	-00.9	00.3	-02.6	-	04.9	05.7	05.8	97	95	97	96	N 9	ENE 6	NE 3	
11	799.3	801.2	800.7	02.3	06.5	07.9	06.2	08.0	-00.3	-	06.2	06.7	01.9	86	69	18	58	SE 2	- 0	NNE 5	
12	798.4	798.3	797.1	06.1	06.5	04.1	05.2	07.9	04.1	-	05.3	08.9	08.2	56	91	100	82	NE 6	NE 6	NE 6	
13	793.3	795.7	795.3	-01.0	02.9	01.6	01.83	04.1	-01.0	-	05.7	06.5	06.3	100	86	91	92	NE 9	NE 4	NF 4	
14	794.7	796.4	797.0	02.7	05.1	04.7	04.3	05.2	01.6	-	03.2	07.8	06.4	43	88	74	85	NE 4	NE 2	- 0	
15	796.0	796.2	795.8	06.8	10.2	08.2	08.4	10.8	04.7	-	00.8	08.4	08.3	08	68	76	51	NNW 2	NNE 2	NNW 1	
16	795.5	797.1	798.7	07.4	08.5	06.8	07.4	08.9	06.0	-	08.1	08.9	09.5	79	80	96	85	ENE 1	E 1	NE 2	
17	799.5	801.7	802.3	07.0	09.7	08.2	08.3	10.2	06.1	-	07.8	08.2	09.3	78	68	85	77	ENE 1	NE 1	NE 5	
18	803.4	806.3	805.6	07.9	10.4	08.3	08.7	10.4	07.1	-	09.8	10.5	10.7	92	83	98	91	ENE 3	NE 2	- 0	
19	804.3	804.2	803.5	08.2	13.3	12.1	11.4	14.5	07.7	-	09.6	11.3	09.8	88	74	70	77	E 2	SSW 1	SW 2	
20	801.6	801.1	800.0	12.1	13.4	10.2	11.5	13.8	10.2	-	07.2	10.3	11.2	51	67	90	69	NNW 1	NE 2	NNE 3	
21	799.9	799.1	799.3	11.0	12.2	09.8	10.7	12.9	09.6	-	09.3	09.9	09.4	70	70	78	73	ENE 3	E 3	NE 4	
22	798.9	799.1	799.7	11.4	13.0	11.7	12.0	13.1	09.3	-	05.3	08.8	10.0	39	59	73	57	ESE 3	E 2	NE 2	
23	799.3	799.8	799.5	10.5	12.3	09.6	10.5	12.4	09.6	-	08.4	07.9	10.3	66	55	84	68	NE 4	NE 3	SE 3	
24	798.7	798.6	798.9	09.2	12.8	11.3	11.2	13.2	07.8	-	08.1	09.2	07.1	70	62	53	62	E 3	NE 2	S 2	
25	798.1	799.0	799.0	10.9	12.9	10.0	11.0	12.9	10.0	-	07.5	07.6	10.2	57	51	83	64	NNE 2	ENE 2	NE 3	
26	799.0	800.4	800.8	06.2	06.8	03.9	05.2	10.0	03.9	-	08.3	08.9	07.3	88	90	91	90	ENE 4	ENE 2	ENE 5	
27	799.0	801.0	801.3	01.7	03.5	01.9	02.3	04.0	01.7	-	06.8	06.8	06.2	99	86	88	91	ENE 5	ENE 6	ENE 4	
28	798.4	798.7	798.4	05.5	08.1	05.7	06.3	08.4	01.6	-	01.1	01.7	05.2	12	16	57	28	NE 4	NE 5	NE 7	
29	798.9	799.5	799.9	03.6	05.9	03.9	04.3	06.0	03.6	-	06.8	07.2	06.9	86	78	85	83	NE 4	NE 6	NE 7	
30	799.0	801.3	803.1	01.2	04.4	02.4	02.6	04.5	01.2	-	06.2	06.9	06.2	92	83	86	87	NE 10	NE 9	NE 6	
M.	797.7	798.6	798.5	06.2	08.6	06.7	07.1	09.6	04.5	-	06.9	08.1	07.8	72	73	79	75	4.3	3.3	3.8	
VR																					

1985 OKTOBAR

BJELAŠNICA

1	803.7	805.1	805.2	06.3	09.4	07.8	07.8	09.4	02.4	-	05.3	07.5	06.3	55	64	60	60	NE 4	ESE 3	NW 2	
2	804.2	804.7	804.4	08.5	10.4	09.4	09.4	10.5	07.5	-	03.8	06.1	05.6	34	48	47	43	NNE 5	NE 2	NE 3	
3	803.3	803.3	802.6	08.2	12.0	10.7	10.4	12.3	08.2	-	05.9	06.4	06.0	54	46	47	49	NE 2	SSW 2	NNW 2	
4	801.1	800.4	799.7	08.8	12.2	10.6	10.6	12.6	08.8	-	05.0	07.0	04.6	44	49	36	43	- 0	NNE 2	- 0	
5	797.9	797.9	798.0	09.4	12.4	09.8	10.4	13.0	09.4	-	04.7	05.4	04.5	40	37	37	38	SW 2	- 0	SSW 3	
6	797.9	799.4	800.4	08.9	11.2	09.5	09.8	12.0	08.9	-	03.6	03.6	06.6	31	27	55	38	SSW 6	NE 2	NE 4	
7	800.8	800.7	799.5	07.6	10.2	07.5	08.2	11.0	07.5	-	08.4	08.1	08.2	80	65	86	77	NE 5	NE 5	NE 5	
8	796.4	793.6	792.8	08.8	09.7	09.3	09.3	10.2	07.4	-	02.4	06.3	03.9	21	52	33	35	N 2	NNE 2	NNE 3	
9	793.1	794.1	795.9	05.6	10.2	07.6	07.8	10.4	05.6	-	07.2	06.9	07.0	79	56	67	67	S 2	SSW 3	SSW 3	
10	797.0	798.6	800.7	06.3	10.4	04.6	06.5	10.5	04.6	-	06.1	07.2	07.9	64	57	93	71	SSW 4	SSW 5	NE 3	
11	801.5	801.9	802.1	00.7	01.4	00.2	00.6	04.6	-00.4	-	06.3	06.6	05.8	98	97	94	96	NE 6	NE 5	ENE 5	
12	800.8	801.6	800.0	02.6	05.6	04.0	04.1	05.7	00.2	-	05.6	07.8	07.5	76	86	92	85	NE 8	NE 4	NE 6	
13	796.4	796.4	794.3	-03.6	-03.0	-05.2	-04.3	04.0	-05.2	-	04.4	04.5	03.9	95	92	93	93	NE 10	NE 9	NE 10	
14	792.2	792.6	793.6	-06.6	-06.1	-06.3	-06.3	-05.2	-06.9	-	03.5	03.7	03.6	94	94	94	94	NE 10	NE 9	NE 7	
15	788.6	788.6	788.2	-07.0	-02.0	-03.2	-03.9	-02.0	-07.0	-	03.4	05.1	04.7	93	96	97	95	NE 8	NE 10	E 8	
16	786.7	788.6	791.1	-06.3	-05.6	-05.2	-05.6	-03.2	-06.4	-	03.6	03.8	03.9	94	95	95	95	NE 8	NE 9	NE 10	
17	793.9	794.4	795.3	-06.2	-04.6	-06.2	-05.8	-04.6	-06.2	-	03.6	04.2	03.6	94	96	94	95	ENE 7	NE 7	NE 10	
18	795.8	795.5	794.0	-00.5	00.0	00.2	00.0	00.2	-06.3	-	05.7	06.0	06.1	96	98	98	97	NE 6	NE 5	NE 5	
19	791.9	791.1	791.1	-00.3	-01.0	-02.2	-01.4	-01.4	-02.2	-	04.2	05.4	04.9	71	96	94	87	NE 7	NE 7	NE 10	
20	791.4	793.9	796.6	-03.2	-02.5	-02.5	-02.7	-02.0	-03.2	-	04.6	05.0	05.3	95	98	98	97	NNE 11	NE 5	NNE 5	
21	797.6	799.3	799.3	-02.4	01.0	02.0	00.7	02.0	-02.5	-	05.0	06.4	07.1	98	97	100	98	NE 3	SE 3	SSW 3	
22	798.7	798.4	797.3	01.9	02.7	02.0	02.2	03.0	01.9	-	07.0	07.4	07.1	100	100	100	100	SSW 4	SE 2	SE 4	
23	793.9	792.4	794.3	-01.7	-04.8	-04.9	-04.1	02.0	-05.2	-	05.3	04.1	04.1	98	95	95	96	NNE 9	NE 8	NE 4	
24	795.5	797.2	798.9	-04.2	-03.0	-04.4	-04.0	-02.4	-04.9	-	04.2	04.7	04.1	94	95	94	94	N 3	ENE 3	E 2	
25	799.7	799.9	799.7	-06.7	-02.8	-02.0	-03.4	-02.0	-06.7	-	03.4	04.0	04.0	92	80	75	82	ESE 5	E 4	NE 4	
26	799.5	799.5	799.3	-00.3	01.0	00.1	00.2	01.4	-02.2	-	01.3	04.5	04.2	21	69	68	53	NE 3	S 5	SW 5	
27	797.7	797.9	797.6	00.6	02.1	00.8	01.1	02.2	00.1	-	04.5	05.6	05.3	71	79	82	77	NNW 2	SSW 3	SW 5	
28	796.3	796.3	795.7	00.1	02.5	02.1	01.7	02.8	00.0	-	04.8	05.3	03.1	78	73	43	65	HW 2	SSW 3	SW 5	
29	793.1	794.3	795.0	01.9	02.6	02.8	02.5	02.8	01.0	-	06.7	07.2	07.2	96	97	96	96	SW 6	SSW 5	SW 6	
30	794.4	794.4	793.9	03.0	03.8	02.3	02.9	04.2	02.3	-	07.6	07.3	06.9	100	91	96	96	SSW 6	SW 7	SSW 8	
31	790.3	788.8	789.2	03.0	04.6	03.1	03.5	04.7	02.1	-	07.6	08.5	07.6	100	100	100	100	S 8	SSW 10	SSW 8	
M.	796.5	796.7	797.0	01.4	03.2	02.1	02.2	04.2	00.4	-	05.0	05.8	05.5	76	78	79	79	5.3	4.8	5.0	
VR																					

Dan	Vrijevost 0-9		Oblačnost N (0-10)			Insolucija broj sati	Padavine R mm	Snežni pokrivač h cm	Razvoj vremena w
	14	7	14	21	Sred. Dles				
1	9	02	05	10	05.7	10.4	.	.	F.F. 8 ⁰⁰ 24, 13 ⁰⁰ 19 ⁰⁰ F.F. 0-8 ⁰⁰ 16 ⁰⁰ 24, 12 ⁰⁰ 21 ⁰⁰ 6 ⁰⁰ 14 ⁰⁰ 20 ⁰⁰ , 15 ⁰⁰ 24, 16 ⁰⁰ 17 ⁰⁰ , 16 ⁰⁰ 16 ⁰⁰ 0-10 ⁰⁰ 18 ⁰⁰ 24, F.F. 0-24, 2 ⁰⁰ 5 ⁰⁰ 0-9 22 ⁰⁰ 24, F.F. 0-17 ⁰⁰ 0-1 ⁰⁰ 8 ⁰⁰ 9 ⁰⁰ , 14 ⁰⁰ 8 ⁰⁰ 11, F.F. 14 ⁰⁰ 21
2	8	02	09	10	07.0	06.0	01.4	.	.
3	8	10	07	10	09.0	06.6	18.1	.	.
4	8	10	06	02	06.0	09.9	.	.	.
5	8	06	08	09	07.7	10.4	.	.	.
6	8	00	09	10	06.3	03.5	.	.	F.F. 4-24, 6 ⁰⁰ 10 ⁰⁰ , 15 ⁰⁰ 24
7	8	10	06	09	08.3	08.9	00.1	.	F.F. 0-24, 0-10 ⁰⁰ 22 ⁰⁰ 24
8	8	10	05	02	05.7	07.8	.	.	F.F. 0-4, 15-24, 0-7 ⁰⁰ 16 ⁰⁰ 16 ⁰⁰ , 16 ⁰⁰ 16 ⁰⁰
9	2	10	09	00	06.3	01.9	01.1	.	F.F. 0-4, 5 ⁰⁰ 17 ⁰⁰ , 6 ⁰⁰ 10 ⁰⁰ 7-7 ⁰⁰ , 7 ⁰⁰ 7 ⁰⁰ , 13-11 17 ⁰⁰ 21 ⁰⁰ 13-11 2-18 ⁰⁰ , F.F. 5-12 ⁰⁰ , 6 ⁰⁰ 15 ⁰⁰ , 12 ⁰⁰ 23 ⁰⁰
10	8	10	10	10	10.0	01.3	09.6	.	.
11	0	10	10	10	10.0	00.7	13.1	.	2 ⁰⁰ 24, 6-8
12	8	10	08	10	09.3	08.8	00.0	.	0-11 ⁰⁰ 19 ⁰⁰ 24
13	7	10	06	10	08.7	07.2	.	.	0-11 ⁰⁰ 20 ⁰⁰ 23
14	8	10	08	01	06.3	07.6	.	.	3 ⁰⁰ 8 ⁰⁰ 21 ⁰⁰ 24, 2-24 7 ⁰⁰ 12, 17-20
15	8	00	01	00	00.3	13.5	.	.	0-2, 2-6, 2-6 12 ⁰⁰
16	8	00	01	00	00.3	13.6	.	.	F.F. 2 ⁰⁰ 8 ⁰⁰
17	8	00	08	10	06.0	05.6	.	.	F.F. 6 ⁰⁰ 8 ⁰⁰ 14 ⁰⁰ 17 ⁰⁰ , 10 ⁰⁰ 13 ⁰⁰ , 21 ⁰⁰ 22 ⁰⁰ , 16 ⁰⁰ 20 ⁰⁰ , 23 ⁰⁰
18	8	04	06	00	03.3	07.8	01.2	.	F.F. 1 ⁰⁰ 6 ⁰⁰ 15 ⁰⁰ 12, 6-20-24
19	8	00	06	00	02.0	08.7	.	.	0-2 11-10 2-9
20	8	03	04	00	02.3	12.1	.	.	11-22 2-5 ⁰⁰
21	8	00	09	10	06.3	11.6	.	.	F.F. 7 ⁰⁰ 20, 22 ⁰⁰ 24, 11-10 11 ⁰⁰ 20 ⁰⁰ , 20 ⁰⁰ 24, 20 ⁰⁰ 24
22	9	00	00	00	00.0	14.0	00.3	.	0-0 ⁰⁰ F.F. 0-24, 0-6
23	9	00	01	00	00.3	14.2	.	.	F.F. 0-14 ⁰⁰
24	9	00	04	00	01.3	14.0	.	.	.
25	8	00	02	01	01.0	13.1	.	.	.
26	8	00	02	00	00.7	13.6	.	.	F.F. 0 ⁰⁰ 8 ⁰⁰
27	8	00	04	00	01.3	13.3	.	.	20 ⁰⁰ 23
28	8	00	04	00	01.3	13.1	.	.	.
29	8	01	00	00	00.3	13.8	.	.	F.F. 2 ⁰⁰ 24
30	8	00	00	00	00.0	13.4	.	.	F.F. 0-24
31	8	02	05	04	03.7	08.0	.	.	F.F. 0-24, 15 ⁰⁰ 15 ⁰⁰
M.									
VR.	03.9	05.3	04.1	04.4	294.4	44.9			

1	8	10	05	00	05.0	10.3	.	.	F.F. 0-8 ⁰⁰ 0 ⁰⁰ 10 ⁰⁰
2	8	01	10	10	07.0	02.5	.	.	F.F. 0 ⁰⁰ 8 ⁰⁰ 12 ⁰⁰ 13 ⁰⁰ 16 ⁰⁰ 24, 10 ⁰⁰ 20 ⁰⁰ , 14 ⁰⁰ 24
3	8	00	01	00	00.3	13.4	09.4	.	F.F. 0-13 ⁰⁰ 0-2 ⁰⁰ 14 ⁰⁰ 2 ⁰⁰ 11 ⁰⁰
4	8	05	09	10	08.0	07.4	.	.	F.F. 12 ⁰⁰ 15 ⁰⁰ 15 ⁰⁰ 18 ⁰⁰ , 18 ⁰⁰ 23 ⁰⁰ , 20 ⁰⁰ 20 ⁰⁰
5	9	00	01	00	00.3	13.8	00.1	.	F.F. 20 ⁰⁰ 24
6	8	00	00	01	00.3	12.5	.	.	F.F. 0-2 ⁰⁰ 6 ⁰⁰ 24
7	8	10	09	10	09.7	03.8	11.4	.	F.F. 0-24, 0 ⁰⁰ 8 ⁰⁰ 11 ⁰⁰ 12 ⁰⁰ 17 ⁰⁰ 24, 4-9 ⁰⁰ 17 ⁰⁰ 24, 17 ⁰⁰ 7 ⁰⁰ , 17 ⁰⁰ 7 ⁰⁰ 21 ⁰⁰
8	8	04	08	02	04.7	09.1	06.2	.	F.F. 0-11 ⁰⁰ 20 ⁰⁰ 24, 0-7 ⁰⁰ , 0-0 ⁰⁰
9	9	02	08	05	05.0	06.8	.	.	F.F. 0-10, 17 ⁰⁰ 23 ⁰⁰
10	9	00	04	00	01.3	11.6	.	.	F.F. 8 ⁰⁰ 18
11	9	03	04	00	02.3	11.9	.	.	.
12	9	00	01	00	00.3	13.1	.	.	.
13	9	00	00	00	00.0	13.2	.	.	.
14	9	00	00	00	00.0	13.3	.	.	11-5-9
15	8	00	04	00	01.3	12.4	.	.	.
16	8	00	00	00	00.0	13.0	.	.	.
17	9	00	01	00	00.3	12.4	.	.	.
18	2	00	04	00	01.3	10.4	.	.	F.F. 4 ⁰⁰ 8 ⁰⁰ 14 ⁰⁰ 24, 15 ⁰⁰ 16 ⁰⁰ 11-15 16 ⁰⁰ 24
19	9	00	01	00	00.3	12.9	.	.	F.F. 0-8 ⁰⁰ 14 ⁰⁰ 24, 0-11 ⁰⁰
20	8	03	09	00	04.0	07.0	.	.	F.F. 0-8 ⁰⁰
21	8	00	00	00	00.0	11.6	.	.	3 ⁰⁰ 5 ⁰⁰ F.F. 5 ⁰⁰ 14 ⁰⁰ 17 ⁰⁰ 24
22	9	00	00	00	00.0	13.1	.	.	F.F. 0-5
23	9	00	04	04	02.7	10.9	.	.	F.F. 18 ⁰⁰ 20 ⁰⁰
24	9	00	01	02	01.0	12.6	.	.	F.F. 22 ⁰⁰ 24
25	8	00	04	00	01.3	12.8	.	.	F.F. 0 ⁰⁰ 6 ⁰⁰ 15 ⁰⁰ 24
26	8	00	08	10	06.0	08.7	.	.	F.F. 0-24, 15 ⁰⁰ 24, 16 ⁰⁰ 24, 22 ⁰⁰ 24
27	0	10	10	10	10.0	00.0	12.6	.	0-24, 18-3 ⁰⁰ 0-24, F.F. 0-0 ⁰⁰ 8 ⁰⁰ 24
28	0	10	10	10	10.0	00.0	13.7	.	0-24, 0-4 ⁰⁰ 19 ⁰⁰ 24, F.F. 0-24
29	0	10	10	10	10.0	00.0	06.0	.	0-24, 0-24, F.F. 0-24
30	0	10	10	10	10.0	00.0	08.0	.	0-24, 0-11 ⁰⁰ , F.F. 0-24
31	0	10	10	00	06.7	00.0	02.5	.	0-23, F.F. 0-13 ⁰⁰ , 4 ⁰⁰ 6 ⁰⁰ , 23 ⁰⁰ 24
M.									
VR.	02.8	04.7	03.0	03.5	280.5	69.9			

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21				
1	8 00⊙	05⊙	00	01.7	11.8	.	.	0-2 ⁰⁰	
2	8 08⊙	09	09	08.7	05.3	.	.	R 14 ⁰⁵ 15 ⁰⁵	
3	8 00⊙	06⊙	05	03.7	10.1	.	.	F 12 ⁰⁵ 24	
4	8 09	10	00	06.3	02.4	.	.	F 0-24, 8 ⁰⁰ 13 ⁰⁰ , 20 ⁰⁰ 21 ⁰⁰ , 22 ⁰⁰ 9 ⁰⁰ 11 ⁰⁰ 14 ⁰⁰ 14 ⁰⁰ 15 ⁰⁰ 17 ⁰⁰ 19 ⁰⁰	
5	9 10	05⊙	00	05.0	07.1	01.7	.	F 0-13 ⁰⁰ , K ⁰⁰ 24; 1 ⁰⁰ 11 ⁰⁰ , 12 ⁰⁰ 10 ⁰⁰ 12 ⁰⁰	
6	8 00⊙	02⊙	01	01.0	11.3	.	.	F 0-3 ⁰⁰ 8 ⁰⁰ 13 ⁰⁰ , 14 ⁰⁰ 17 ⁰⁰ 22 ⁰⁰ 22-24	
7	8 10	06⊙	00	05.3	08.5	.	.	0-5 ⁰⁰ , F 12 ⁰⁰ 19 ⁰⁰ 22 ⁰⁰ 24; V 4-8 ⁰⁰ , 20 ⁰⁰ 9 ⁰⁰ 11 ⁰⁰	
8	9 01⊙	05⊙	02	02.7	11.6	.	.	F 0-4 ⁰⁰	
9	8 08⊙	10	10*	09.3	00.9	.	.	14 ⁰⁰ 15 ⁰⁰ , 14 ⁰⁰ 18 ⁰⁰ 15 ⁰⁰ 24, F 17 ⁰⁰ 24, 18 ⁰⁰ 19 ⁰⁰ , 19 ⁰⁰ 21 ⁰⁰ 19 ⁰⁰	
10	8 10	06⊙	00	05.3	04.5	06.3	.	0-20, F 0-20, V 2 ⁰⁰ 14 ⁰⁰	
11	9 00⊙	00⊙	00	00.0	11.7	.	.	17 ⁰⁰ 3-8 ⁰⁰ F 20 ⁰⁰ 24	
12	9 04⊙	04⊙	10	06.0	11.7	.	.	F 0-24, 4 ⁰⁰ 5-8 ⁰⁰ 18-24	
13	8 10	04⊙	00	04.7	07.6	.	.	0-9, F 0-11, 9-11 ⁰⁰	
14	9 00⊙	00⊙	00	00.0	11.6	.	.		
15	8 06⊙	00⊙	00	00.0	11.9	.	.	* 5 ⁰⁰ 9	
16	8 00⊙	02⊙	00	00.7	11.2	.	.		
17	8 00⊙	02⊙	00	00.7	09.8	.	.	* 00-07 5 ⁰⁰ 11 ⁰⁰ F 23 ⁰⁰ 24	
18	9 00⊙	04⊙	03	02.3	10.8	.	.	F 0-5 ⁰⁰ , * 00 5 ⁰⁰ 11, 20-24	
19	9 00⊙	00⊙	00	00.0	11.6	.	.	0-8 * 00 5-8 ⁰⁰	
20	9 08⊙	08	02	06.0	09.1	.	.	* 00-04 5-11 ⁰⁰ , F K ⁰⁰ 19 ⁰⁰	
21	9 01⊙	02⊙	00	01.0	10.3	.	.	F K ⁰⁰ 19 ⁰⁰ , K ⁰⁰ 18 ⁰⁰	
22	9 01⊙	01⊙	01	01.0	11.4	.	.		
23	9 00⊙	01⊙	00	00.3	10.9	.	.	F K ⁰⁰ 20 ⁰⁰	
24	8 00⊙	02⊙	00	00.7	11.2	.	.	F 0 ⁰⁰ 2 ⁰⁰	
25	8 00⊙	01⊙	01	00.7	10.7	.	.	22-24	
26	0 02	10	10	07.3	02.1	00.1	.	0-4 ⁰⁰ , 4 ⁰⁰ 5 ⁰⁰ , 4 ⁰⁰ 5 ⁰⁰ 8, 8-24, 15-24	
27	2 10	05	06	07.0	06.7	00.1	.	0-15, 17 ⁰⁰ 19 ⁰⁰ , F 0-24, 5 ⁰⁰ 7 ⁰⁰	
28	9 03⊙	03⊙	01	02.3	11.0	00.0	.	F 0-24	
29	8 07	05	10	07.3	09.7	.	.	F 0-24, 20 ⁰⁰ 24	
30	8 00	02	00	00.7	10.1	.	.	F 0-24, 0-7 ⁰⁰	
H.									
VR.	03.4	04.0	02.4	03.3	274.6	08.2			

1	9 01⊙	02⊙	00	01.0	10.8	.	.	F 0-2 ⁰⁰
2	9 01⊙	01⊙	01	01.0	10.9	.	.	F 6 ⁰⁰ 7 ⁰⁰
3	9 01⊙	01⊙	00	00.7	10.9	.	.	
4	9 00⊙	00⊙	00	00.0	10.8	.	.	
5	9 00⊙	00⊙	00	00.0	10.7	.	.	
6	9 00⊙	00⊙	00	00.0	10.6	.	.	F 0 ⁰⁰ 8 ⁰⁰ 22 ⁰⁰ 24
7	8 00⊙	02⊙	00	00.7	10.3	.	.	F 0-21 ⁰⁰
8	9 00⊙	01⊙	00	00.3	10.4	.	.	* 13-10 5 ⁰⁰ 11 ⁰⁰
9	8 04	04⊙	00	02.7	09.3	.	.	* 15 1 ⁰⁰ 17 ⁰⁰
10	8 02⊙	08⊙	10	06.7	07.1	.	.	* 14 ⁰⁰ 15 ⁰⁰ , 15 ⁰⁰ 24, K ⁰⁰ 20 ⁰⁰ , F 23 ⁰⁰ 24
11	8 10	09	00	06.3	02.2	03.3	.	0-11 ⁰⁰ , 18 ⁰⁰ 19 ⁰⁰ ; F 0-24, 4 ⁰⁰ 5 ⁰⁰
12	8 01⊙	06⊙	10	05.7	06.0	.	.	F 0-24, 20 ⁰⁰ 24
13	6 10	08⊙	10	09.3	03.8	.	.	0-9, K ⁰⁰ 24, F 0-24, V 4 ⁰⁰ 12, 17-24
14	0 10	10	10	10.0	00.0	.	.	0-24, F 0-24, V 0-24, * 16 ⁰⁰ 17 ⁰⁰
15	1 10	10	10	10.0	00.0	00.0	.	0-24, V 0-24, F 0-24, * 7 ⁰⁰ 24, * 17-20, 14 21 ⁰⁰ 22 ⁰⁰
16	0 10	10*	10*	10.0	00.0	02.9	02	0-24, F 0-24, * 0-23 ⁰⁰ V 0-24, * 9-24, 11
17	0 10	10	00	06.7	00.9	10.1	15	0-16, V 0-24, * 0-9, F 0-24, 11
18	2 10	01	00	03.7	01.6	.	15	V 0-12, F 0-21 ⁰⁰ , 0 ⁰⁰ 17 ⁰⁰ 11
19	1 01⊙	10	10	07.0	06.5	.	10	F 4 ⁰⁰ 24, 3 ⁰⁰ 24, * 6 ⁰⁰ 13 ⁰⁰ V 18 ⁰⁰ 24, 11
20	0 10	10*	10*	10.0	00.0	00.1	08	0-24, F 0-17 ⁰⁰ V 0-24, * 8 ⁰⁰ 21 ⁰⁰ , 11
21	1 02	10	10	07.3	02.0	06.3	15	0-8 ⁰⁰ 13 ⁰⁰ 24; V 0-12 ⁰⁰ * 8 ⁰⁰ 13 ⁰⁰ , * 15 ⁰⁰ 20 ⁰⁰ , 23 ⁰⁰ 24; F 23 ⁰⁰ 24, 11
22	0 10	10	10	10.0	00.0	02.0	05	* 0-5 ⁰⁰ 7 ⁰⁰ 12, 12 ⁰⁰ 26 ⁰⁰ 24, F 0-8, 0-24, 11
23	0 10	10*	10*	10.0	00.0	04.6	03	0-24, * 3 ⁰⁰ 4 ⁰⁰ , * 4 ⁰⁰ 13 ⁰⁰ , V 4 ⁰⁰ 24, F 5 ⁰⁰ 17 ⁰⁰ , 11
24	0 10	10	10	10.0	00.0	02.9	03	0-24, V 0-24, 11
25	9 00⊙	00⊙	00	00.0	09.7	00.2	02	0-0 ⁰⁰ V 0-24, * 0 ⁰⁰ 12 ⁰⁰ , 20 ⁰⁰ 24; F 5 ⁰⁰ 14 ⁰⁰ , 11
26	9 01	00⊙	00	00.3	09.9	.	02	V 0-9 ⁰⁰ * 0-14 ⁰⁰ , 20 ⁰⁰ 24; F 12 ⁰⁰ 14 ⁰⁰ , 21 ⁰⁰ 23 ⁰⁰ , 11
27	9 00	04⊙	00	01.3	09.9	.	01	* 10-14 ⁰⁰ , 11
28	9 00	04⊙	09	04.3	09.0	.	.	* 00-17 ⁰⁰ 24
29	0 10	10	10	10.0	00.0	00.0	.	* 00-08 0-5 F 2 ⁰⁰ 13 ⁰⁰ 20 ⁰⁰ 24; 0-5-24
30	0 10	10	10	10.0	00.0	13.2	.	0-24, F 0-24, * 2 ⁰⁰ K ⁰⁰
31	0 10	10	10	10.0	00.0	06.7	.	0-24, F 0-24, * 0 ⁰⁰ 24, 12 7 ⁰⁰ 10 ⁰⁰ , 13 ⁰⁰ 18 ⁰⁰
H.								
VR.	05.0	05.8	05.2	05.3	163.3	49.3		

$\varphi = 43^{\circ}43' N$ $\lambda = 16^{\circ}16' E$ Gr. ΔG = + 1h 13 min.

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T C°						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina veta- ro, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	789.5	789.0	786.1	02.8	03.6	02.2	02.7	03.8	02.2	-	07.5	07.9	07.2	100	100	100	100	SW	5	SW	5	SSW	8	
2	779.5	778.4	780.6	02.2	00.3	-00.6	00.3	02.3	-00.7	-	07.2	06.2	05.8	100	100	99	100	S	11	WSW	5	WSW	6	
3	782.0	783.8	785.7	-01.2	-00.1	-00.4	-00.5	00.0	-02.0	-	05.3	05.9	05.8	94	97	98	96	SW	6	S	6	SSW	6	
4	786.6	786.1	786.7	-01.0	-00.1	-00.9	-00.7	03.1	-01.3	-	05.5	05.8	05.6	97	95	97	96	E	3	NE	4	NE	6	
5	787.3	786.6	784.4	-00.1	00.6	00.0	00.1	01.4	-00.9	-	04.0	06.1	06.3	65	95	98	86	W	5	W	7	SSW	12	
6	775.3	773.0	779.0	03.5	-01.8	-05.4	-02.3	04.2	-05.4	-	07.9	05.3	03.9	100	98	95	98	SSW	12	N	13	NE	9	
7	780.4	782.9	785.6	-09.6	-06.7	-02.4	-05.3	02.4	-09.6	-	02.7	02.4	02.5	91	64	51	69	NE	8	NE	5	NNE	6	
8	789.3	790.6	791.9	-03.5	02.0	04.0	01.6	04.0	-03.6	-	03.7	04.5	03.6	77	64	45	62	NNE	4	WSW	5	SW	6	
9	792.8	794.4	794.3	01.0	06.0	06.4	05.0	06.4	01.0	-	03.9	06.7	06.3	59	71	66	65	SW	1	W	2	SW	7	
10	792.4	791.3	788.8	06.0	07.0	06.2	06.4	08.6	04.0	-	07.9	09.1	07.9	84	90	83	86	W	8	SW	9	SW	11	
11	785.6	786.4	785.6	03.4	04.4	04.6	04.3	06.2	03.2	-	07.8	08.1	08.4	100	97	99	99	WSW	12	SW	9	SW	10	
12	785.7	789.1	789.6	04.0	05.0	04.4	04.5	05.0	04.0	-	08.1	08.7	08.3	100	100	99	100	SW	11	SW	6	SSW	7	
13	785.2	786.0	786.6	03.9	04.7	04.4	04.4	05.0	03.9	-	07.3	08.2	07.9	91	96	95	94	SW	13	SW	16	SW	12	
14	780.7	789.7	792.2	03.3	00.7	-03.2	-00.6	04.4	-03.2	-	06.7	05.2	04.5	86	80	93	86	SW	13	SSW	9	NNW	3	
15	792.6	793.6	794.9	-09.7	-09.8	-10.6	-10.2	-03.2	-10.6	-	02.7	02.6	02.5	91	91	90	91	NNE	7	NNE	7	NNE	5	
16	794.7	794.0	792.8	-08.2	-03.7	-03.6	-04.8	-02.6	-10.8	-	03.0	04.3	04.4	92	93	95	93	-	0	SSW	3	SSW	6	
17	793.8	793.1	793.1	-08.0	-08.9	-09.3	-08.9	-03.3	-09.3	-	03.1	02.9	02.8	92	92	91	92	NNE	4	ENE	4	E	6	
18	791.1	789.0	787.8	-02.8	-00.9	-00.8	-01.3	-00.5	-09.3	-	04.8	05.7	05.7	96	99	99	98	S	4	S	6	S	7	
19	786.7	787.5	787.4	-01.1	00.3	00.6	00.1	03.7	-01.1	-	05.6	06.1	06.1	99	97	95	97	S	9	S	8	E	4	
20	785.0	781.7	780.8	00.5	-01.2	-02.2	-01.3	04.8	-02.2	-	06.0	05.4	05.0	95	96	96	96	SSE	6	SSE	7	S	8	
21	782.1	782.6	783.1	-02.8	-01.2	-03.8	-02.9	-01.0	-03.6	-	04.8	05.4	04.4	96	96	95	96	S	10	S	9	S	12	
22	786.6	787.9	788.3	-04.8	-03.0	-02.6	-03.3	-02.4	-05.2	-	06.1	04.6	04.8	95	94	96	95	SSW	7	SSW	6	SSW	7	
23	788.0	786.1	785.2	-02.4	-02.4	-01.8	-02.1	-01.8	-02.7	-	04.7	04.8	05.1	93	94	95	94	S	3	NNW	2	S	6	
24	784.7	783.1	780.7	-02.1	-03.2	-03.3	-03.0	-01.7	-03.3	-	05.0	04.6	04.6	95	95	95	95	S	5	NE	2	NE	2	
25	778.6	778.0	778.0	-04.6	-03.3	-04.3	-04.1	-03.3	-04.6	-	04.1	04.6	04.2	94	95	94	94	NNE	4	SW	5	SW	5	
26	776.7	774.7	776.0	-05.1	-04.0	-06.3	-05.4	-04.0	-06.4	-	03.9	04.3	03.6	93	94	94	94	SSW	4	NNE	3	-	0	
27	776.3	778.0	780.3	-06.0	-03.0	-02.5	-03.5	-02.4	-06.3	-	03.7	04.6	04.8	94	94	94	94	WSW	2	WSW	4	SW	5	
28	781.6	782.4	783.4	-04.9	-03.8	-04.5	-04.4	-02.5	-04.9	-	04.0	04.3	04.0	93	93	92	93	WSW	4	SW	3	W	2	
29	784.8	788.7	791.0	-07.4	-08.0	-07.5	-07.6	-04.4	-10.0	-	03.0	02.9	02.7	85	86	78	83	NE	5	NE	2	NE	5	
30	792.4	793.1	793.2	-01.3	-03.4	-02.9	-02.6	-01.3	-07.5	-	04.5	04.4	04.5	81	91	92	88	WSW	7	SSW	8	SSW	8	
M.																								
VR	785.8	786.0	786.4	-01.9	-01.1	-01.5	-01.5	00.5	-03.5	-	05.1	05.4	05.1	91	92	90	91	6.4	5.9	6.6				

1985 DECEMBAR

BJELASNICA

1	796.3	798.3	800.0	-01.2	-00.9	-00.4	-00.7	-00.4	-03.0	-	05.2	05.3	04.9	92	93	82	89	W	5	NNW	4	NW	3
2	800.4	801.1	801.7	01.2	04.1	06.1	04.4	06.1	-00.4	-	05.0	05.8	04.7	75	71	50	65	NW	6	NNW	6	NNW	6
3	801.1	802.0	802.6	06.3	07.7	07.6	07.3	07.9	05.0	-	04.7	04.4	04.6	49	42	44	45	NNW	6	NNW	2	SW	3
4	802.4	802.4	802.4	07.8	08.6	06.4	07.3	08.8	06.4	-	04.1	04.2	03.1	38	37	32	36	W	4	WSW	5	WSW	5
5	799.4	797.9	794.0	04.2	04.4	01.7	03.0	05.8	01.7	-	03.1	03.7	03.4	38	44	50	44	WSW	9	SW	9	SW	13
6	794.6	794.3	794.4	04.4	04.1	04.6	04.4	05.2	01.6	-	03.4	03.5	03.1	41	43	37	40	SW	7	SW	7	NW	3
7	794.4	793.5	793.5	-01.2	02.8	03.6	02.2	04.6	-01.2	-	05.2	03.3	02.6	92	45	32	56	ENE	5	SW	6	WSW	6
8	791.9	792.6	791.5	03.4	-01.0	-02.3	-01.3	03.6	-02.3	-	05.6	04.8	04.2	89	85	81	85	SW	8	SW	5	SSW	7
9	791.8	792.2	792.0	-02.6	-00.2	-02.0	-01.7	-00.1	-03.7	-	04.7	05.0	05.2	92	83	98	91	SW	6	SW	5	SW	7
10	790.0	789.6	789.1	-03.8	-00.5	-00.6	-00.6	-00.4	-02.0	-	05.7	05.8	05.6	99	98	96	98	SW	8	SSW	6	SSW	4
11	789.0	789.3	790.1	-00.8	00.0	-01.6	-01.0	00.1	-02.0	-	05.5	05.8	05.2	96	95	95	95	SW	2	SW	2	S	4
12	790.1	790.6	791.4	-01.8	-01.3	-02.9	-02.2	-01.1	-02.9	-	05.1	05.3	04.6	95	95	94	95	S	6	S	3	ESE	2
13	793.2	795.4	795.0	-02.2	-02.6	-02.8	-02.6	-02.2	-03.1	-	04.8	04.7	04.6	93	92	92	92	ENE	2	ENE	4	E	3
14	793.5	793.1	793.6	-02.5	-04.7	-06.8	-05.2	-01.7	-06.9	-	04.7	03.4	03.4	92	79	94	88	ENE	3	NNE	6	NNE	6
15	792.6	793.1	794.8	-06.4	-02.4	-01.7	-03.1	-01.3	-07.5	-	03.6	04.9	05.2	94	96	97	96	NNE	8	NNE	10	NNE	5
16	793.3	792.7	790.7	-02.2	-02.6	-03.4	-02.9	-01.2	-03.5	-	04.2	04.8	04.4	81	94	91	89	N	7	NNE	5	NNE	10
17	789.9	788.8	788.6	01.6	02.6	00.0	01.1	02.9	-03.7	-	03.6	02.5	03.4	52	34	56	47	NNW	10	NNW	9	N	8
18	787.8	789.0	789.3	-04.6	-03.9	-02.3	-03.3	03.0	-04.6	-	04.2	03.8	03.6	96	82	70	83	N	8	NNE	7	NNW	6
19	793.1	789.3	788.6	-00.5	-00.8	-05.4	-03.0	01.0	-05.4	-	04.3	04.0	03.9	73	70	95	79	N	3	SSW	4	ENE	2
20	787.0	787.7	788.6	-07.1	-09.3	-07.5	-07.9	-05.4	-10.0	-	03.4	02.8	03.2	93	91	93	92	N	9	NNE	9	NNE	9
21	789.0	791.4	793.0	-07.0	-07.5	-08.1	-07.7	-07.0	-08.1	-	03.4	03.2	03.1	93	93	92	93	NNE	9	NNE	7	NNE	7
22	794.0	794.6	794.6	-04.7	-04.0	-03.7	-04.0	-03.7	-08.2	-	04.0	04.2	04.4	94	93	95	94	NNE	7	NNE	5	NNE	3
23	792.8	791.8	791.8	-02.3	-01.6	-02.2	-02.0	-01.2	-04.0	-	01.6	01.6	00.7	30	30	13	24	NE	3	ESE	3	SSW	3
24	790.8	789.6	789.9	-02.4	-02.2	-03.0	-02.7	-01.4	-03.5	-	00.7	00.7	01.1	14	13	21	16	SSW	5	SSW	5	SSW	6
25	788.8	787.5	784.2	-05.7	-04.5	-04.0	-04.6	-03.0	-06.0	-	03.8	04.2	04.3	95	96	94	95	SSW	5	SW	9	SW	11
26	782.3	780.3	781.3	-02.1	-02.0	-02.1	-02.1	-00.6	-04.2	-	04.9	05.0	05.3	93	95	95	94	SW	11	SW	9	SW	8
27	781.5	782.0	785.2	-03.4	-03.2	-04.0	-03.7	-02.1	-04.0	-	04.4	04.6	04.3	93	95	94	94	SW	6	SW	5	W	6
28	784.6	783.9	783.4	-04.6	-03.0	-01.0	-02.4	-01.0	-05.0	-	04.0	04.8	05.4	92	97	96	95	SW	10	SW	11	SW	10
29	780.8	776.3	780.3	-03.2	00.2	00.6	00.3	00.6	-01.0	-	05.8	06.1	06.3	97	98	98	98	SW	10	SSW	11	SSW	10
30	781.7	781.7	780.7																				

Dan	Vidljivost 0-6	Oblačnost N (0-10)					Insolacija broj sati	Padavina R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21	Sred Dias				
1	7	10	09	13	04.7	01.7	67.4	.	≡ 0-24, 0-7 ²⁰ 13 ⁰⁵ 13 ⁰⁵ , F-F 0-24, 0-6 ²⁵ 15 ⁰⁵ 13 ⁰⁵ 24	
2	1	10	10	00	06.7	00.2	01.8	.	≡ 0-22 ⁰⁵ F-F 0-24, 0-7 ²⁰ 11 ⁰⁵ 11 ⁰⁵ 10 ⁰⁵ * 12 ⁰⁵ 16 ⁰⁵ 17-24, 10	
3	1	10	10	10	10.0	00.0	19.2	02	F-F 0-24, 0-4 ⁰⁵ 4 ⁰⁵ 22 ⁰⁵ 13 ⁰⁵ 13 ⁰⁵ 17 ⁰⁵ 24, 16 ⁰⁵ 17 ⁰⁵ 10	
4	1	04	13	10	08.0	00.0	01.9	02	F-F 0-4, 17 ⁰⁵ 22 ⁰⁵ V-0-12 ⁰⁵ 13 ⁰⁵ 24; ≡ 0-23 ⁰⁵ 7 ⁰⁵ 11 ⁰⁵ 10 ⁰⁵ 16 ⁰⁵ 17 ⁰⁵ 10	
5	2	04	10	10	08.0	04.2	00.1	01	* 0-10 ⁰⁵ V-0-8 ⁰⁵ F-F 3 ⁰⁵ 24, ≡ 13 ⁰⁵ 24, 9 ⁰⁵ 16 ⁰⁵ 13 ⁰⁵ 16 ⁰⁵ 24, 17 ⁰⁵ 18 ⁰⁵ 10	
6	0	10	10	10	10.0	00.0	11.6	.	≡ 0-23 ⁰⁵ F-F 0-24, V-0-1, 1 ⁰⁵ 13 ⁰⁵ * 13 ⁰⁵ 17 ⁰⁵ V 13 ⁰⁵ 24, 10	
7	9	01	01	00	00.7	09.1	14.1	01	F-F 0-23 ⁰⁵ V-0-22 ⁰⁵ 10	
8	9	01	08	02	03.7	07.8	.	01	F-F 3 ⁰⁵ 13 ⁰⁵ 16 ⁰⁵ 22 ⁰⁵ 10	
9	9	04	06	04	04.7	07.9	.	.	F-F 13 ⁰⁵ 24	
10	9	07	06	00	04.3	06.7	.	.	F-F 0-24	
11	6	10	08	10	09.3	11.4	.	.	F-F 0-24, ≡ 2 ⁰⁵ 11 ⁰⁵ 17 ⁰⁵ 24, 11 ⁰⁵ 17 ⁰⁵ 10	
12	0	10	10	10	10.0	00.0	.	.	F-F 0-24, ≡ 0-24, 23 ⁰⁵ 24	
13	7	09	10	02	07.0	00.0	00.0	.	F-F 0-24, ≡ 0-1 ⁰⁵ 9 ⁰⁵ 24	
14	8	08	09	10	09.0	04.4	01.5	.	F-F 0-18 ⁰⁵ ≡ 0-5 ⁰⁵ 15 ⁰⁵ 24; 0-5 ⁰⁵ V 16 ⁰⁵ 19 ⁰⁵ * 19 ⁰⁵ 21 ⁰⁵ 10	
15	0	10	10	10	10.0	00.0	00.3	.	≡ 0-23 ⁰⁵ V 0 ⁰⁵ 24, F-F 5 ⁰⁵ 21 ⁰⁵ 10	
16	9	02	01	10	04.3	08.1	09.6	.	V 0-12 ⁰⁵ 20 ⁰⁵ 24; 15 ⁰⁵ 10 ⁰⁵ 15 ⁰⁵ 17 ⁰⁵ 20 ⁰⁵ 24; ≡ 17 ⁰⁵ 24 * 18 ⁰⁵ 24, 10	
17	1	10	10	10	10.0	00.0	04.3	05	≡ 0-24 * 0-11 ⁰⁵ 14 ⁰⁵ 24, F-F 0-24, 0-10 ⁰⁵ 15 ⁰⁵ 24, V-0-24	
18	1	10	10	10	10.0	00.0	14.9	29	≡ 0-24 * 0-24 V-0-24, F-F 0-3 ⁰⁵ 10 ⁰⁵ 21; 13 ⁰⁵ 19 ⁰⁵ 24, < 20 ⁰⁵ 24, 10	
19	1	10	10	10	10.0	00.0	18.2	50	≡ 0-24, V-0-17, * 0-8 ⁰⁵ F-F 0-24, V-0-1, 10 ⁰⁵ < 0-0 ⁰⁵ 10	
20	0	10	10	10	10.0	00.0	05.0	40	≡ 0-24, F-F 0-24, 12 ⁰⁵ 5 ⁰⁵ 16 ⁰⁵ 16 ⁰⁵ ; 10 ⁰⁵ 17 ⁰⁵ * 2 ⁰⁵ 19 ⁰⁵ 22 ⁰⁵ V 16 ⁰⁵ 24 * + 22	
21	0	10	10	10	10.0	00.0	04.5	42	≡ 0-24, F-F 0-24, V-0-24 * + 0-5 ⁰⁵ 23 ⁰⁵ 24, 13 ⁰⁵ 14 ⁰⁵ * 15 ⁰⁵ 20 ⁰⁵ 24, < 23 ⁰⁵ 25 ⁰⁵ 10	
22	9	04	04	00	02.7	04.0	02.1	42	≡ 0-5 ⁰⁵ 17 ⁰⁵ 24, F-F 0-24, V-0-24 * + 0-13 ⁰⁵ 14 ⁰⁵ 5 ⁰⁵ 10 ⁰⁵ , 10	
23	0	08	10	10	09.3	00.0	.	42	F-F 0-5 ⁰⁵ 19 ⁰⁵ 24; ≡ 0-3 ⁰⁵ 8 ⁰⁵ 24, V-0-24, 10	
24	9	10	08	10	09.3	04.7	26.1	73	≡ 0-8 ⁰⁵ 16 ⁰⁵ 24; * 0-6 ⁰⁵ V-0-24, F-F 0-9 ⁰⁵ 10	
25	1	10	10	10	10.0	04.4	.	68	≡ 0-8 ⁰⁵ 12 ⁰⁵ 24; V-0-24, 12 ⁰⁵ 18 ⁰⁵ 12 ⁰⁵ , F-F 15-23 ⁰⁵ 10	
26	1	10	10	10	10.0	00.0	00.0	65	V-0-24, ≡ 0-24 * 6 ⁰⁵ 17 ⁰⁵ 10	
27	9	08	06	10	06.0	06.9	19.2	80	V-0-24, ≡ 0-23 ⁰⁵ 16-24, * 5 ⁰⁵ 20 ⁰⁵ F 21 ⁰⁵ 24, 10	
28	8	10	03	10	07.0	03.0	00.7	79	V-0-24, F-F 0-5 ⁰⁵ * 0-1 ⁰⁵ 8 ⁰⁵ 3 ⁰⁵ * 5 ⁰⁵ 24, 10	
29	8	10	03	06	05.3	03.0	00.4	79	V-0-24, * 0-6 ⁰⁵ 13 ⁰⁵ 17 ⁰⁵ ; ≡ 0-13 ⁰⁵ * 11 ⁰⁵ 19 ⁰⁵ 24; * 8-11, V 20 ⁰⁵ 21, 10	
30	0	10	10	10	10.0	00.0	00.2	78	V-0-24, F-F 0-24, ≡ 5 ⁰⁵ 24, * + 13 ⁰⁵ 24, 10	
H.										
VR.		08.0	07.6	07.7	07.6	77.5	185.1			

1	8	10	05	00	05.0	07.3	.	76	V-0-24, ≡ 0-8 ⁰⁵ F-F 0-7 ⁰⁵ * + 0-2 ⁰⁵ * 8 ⁰⁵ 13 ⁰⁵ , 10
2	9	02	08	02	04.0	05.4	.	73	V-0-1 F 4 ⁰⁵ 22 ⁰⁵ * 5-14 ⁰⁵ 10
3	9	01	02	00	01.0	07.7	.	61	F-F 3 ⁰⁵ 9 ⁰⁵ 2 ⁰⁵ 16 ⁰⁵ 10
4	9	00	01	00	00.3	08.0	.	53	F-F 2 ⁰⁵ 5 ⁰⁵ 13 ⁰⁵ 24, 10 ⁰⁵ 16 ⁰⁵ 17 ⁰⁵ 10
5	9	01	01	00	00.7	07.8	.	49	F-F 0-24, 10 ⁰⁵ 17 ⁰⁵ 5 ⁰⁵ 9 ⁰⁵ 10
6	9	06	01	00	02.3	05.9	.	44	F-F 0-16 ⁰⁵ * 13-20 ⁰⁵ 21 ⁰⁵ 10
7	9	10	00	00	03.3	06.5	.	42	≡ 5 ⁰⁵ 9 ⁰⁵ F 7 ⁰⁵ 24, 10
8	9	00	01	00	00.3	06.1	.	40	F-F 0-24, 10 ⁰⁵ 15 ⁰⁵ ≡ 11 ⁰⁵ 13 ⁰⁵ V 15 ⁰⁵ 24, 10
9	9	00	07	10	05.7	05.2	.	40	F-F 0-10 ⁰⁵ 21-24; V-0-11 ⁰⁵ 16 ⁰⁵ 24; ≡ 2-7, 15 ⁰⁵ 24, * 7-15 ⁰⁵ * 14 ⁰⁵ 14 ⁰⁵ , 10
10	2	10	10	10	10.0	00.1	00.1	40	V-0-24, ≡ 0-24, F-F 0-13 ⁰⁵ 10
11	1	10	10	10	10.0	00.1	.	39	V-0-24, ≡ 0-24, * 8 ⁰⁵ 12 ⁰⁵ 16 ⁰⁵ 24; * 20-14 13 ⁰⁵ 16 ⁰⁵ , 10
12	0	10	10	10	10.0	00.0	04.7	43	V-0-24, ≡ 0-24, * 0-24, F-F 8 ⁰⁵ 10
13	0	10	10	10	06.7	00.6	21.1	64	* 0-7 ⁰⁵ ≡ 0-13 ⁰⁵ V-0-24, F-F 13 ⁰⁵ 13 ⁰⁵ 10
14	9	00	01	10	03.7	07.4	00.1	63	V-0-24, 14 ⁰⁵ 16 ⁰⁵ 17 ⁰⁵ F-F 14 ⁰⁵ 24; ≡ 17 ⁰⁵ 24, 10
15	1	10	10	10	10.0	00.0	.	60	≡ 0-23 ⁰⁵ V-0-24, F-F 0-24, * 5 ⁰⁵ 7 ⁰⁵ 23 ⁰⁵ 24; 10
16	1	02	10	02	04.7	01.3	.	60	V-0-24, F-F 0-24, * 0-11 ⁰⁵ 15 ⁰⁵ 24; ≡ 11 ⁰⁵ 16 ⁰⁵ 10
17	9	02	08	05	05.0	04.6	.	59	V-0-24, F-F 0-24, * 0-10 ⁰⁵ 24, 10
18	9	10	05	05	06.7	05.8	.	58	F-F 0-24, * 0-10 ⁰⁵ 4 ⁰⁵ ≡ 4 ⁰⁵ 9 ⁰⁵ V 4 ⁰⁵ 13 ⁰⁵ * + 11-24, 10
19	8	08	09	10	09.0	01.9	.	58	F-F 0-13 ⁰⁵ * 0-5 ⁰⁵ * 0-14 ⁰⁵ * 13 ⁰⁵ 14 ⁰⁵ ; ≡ 13 ⁰⁵ 22 ⁰⁵ V 16 ⁰⁵ 24, 10
20	0	10	10	07	09.0	00.0	00.0	58	V-0-24, F-F 2 ⁰⁵ 24, * + 4 ⁰⁵ 20 ⁰⁵ ; ≡ 0-2 ⁰⁵ 16 ⁰⁵ * 11-13 ⁰⁵ , 10
21	0	10	10	04	08.0	00.0	02.5	60	F-F 0-24, V-0-24, ≡ 2 ⁰⁵ 16 ⁰⁵ * + 2 ⁰⁵ 15 ⁰⁵ * 1 ⁰⁵ 10 ⁰⁵ , 10
22	9	10	01	00	03.7	06.3	00.0	60	V-0-14, F-F 0-14 ⁰⁵ * 13-24; ≡ 0-13 ⁰⁵ 10
23	9	00	00	00	00.0	08.9	.	57	* 18-24, V-0-24, 10
24	9	00	02	05	02.3	08.5	.	55	* 19 ⁰⁵ 0-24, F-F 13 ⁰⁵ 16 ⁰⁵ 24, 10
25	0	10	10	10	10.0	01.8	.	53	* 0-12 ⁰⁵ F-F 0-24; ≡ 0-24, V-2-24, * + 11 ⁰⁵ 24, * 16 ⁰⁵ 24, 10
26	0	10	10	07	09.0	00.0	03.0	56	≡ 0-24, V-0-24, * 0-2 ⁰⁵ * + 0-21 ⁰⁵ F-F 0-24, * 8 ⁰⁵ 13 ⁰⁵ 10
27	1	10	10	02	07.3	00.0	03.2	59	F-F 0-24, V-0-24, ≡ 0-2 ⁰⁵ 8 ⁰⁵ 13 ⁰⁵ * 3-20 ⁰⁵ * 8 ⁰⁵ 14 ⁰⁵ * + 13-24, 10
28	0	10	10	10	10.0	00.0	03.7	63	V-0-24, F-F 0-24, * + 0-24, ≡ 2 ⁰⁵ 24, * 20 ⁰⁵ 24, 10
29	0	10	10	10	10.0	00.0	05.3	65	≡ 0-24, V-0-12 ⁰⁵ * 0-8 ⁰⁵ F-F 0-24, * + 0-12 ⁰⁵ * 22 ⁰⁵ 24, 10
30	2	10	10	10	10.0	00.0	04.2	60	≡ 0-24, F-F 0-24, * 0-6 ⁰⁵ * 6-8 ⁰⁵ * 7 ⁰⁵ 20 ⁰⁵ V 13 ⁰⁵ 24, 16 ⁰⁵ 18 ⁰⁵ * + 22 ⁰⁵ 24, 10
31	0	10	10	10	10.0	00.0	26.0	82	≡ 0-24, V-0-24, F-F 0-24, * + 0-4 ⁰⁵ 19 ⁰⁵ 24, * 0 ⁰⁵ 2 ⁰⁵ 15 ⁰⁵ 24, 16 ⁰⁵ 15 ⁰⁵ , 10
H.									
VR.		06.5	06.5	05.1	06.1	107.4	73.9		

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta C = + 1h 14 min.$

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T C°						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina vetra D, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	939.3	934.9	932.8	-05.6	-03.2	-05.2	-04.8	-03.0	-05.6	-05.8	03.2	03.1	02.9	80	65	70	72	-	0	MSW	1	-	0	
2	928.0	923.0	924.0	-07.0	-05.0	-06.1	-06.1	-04.8	-07.4	-07.5	03.2	03.7	03.7	89	87	94	90	-	0	WNW	1	WNW	1	
3	926.3	928.0	929.6	-08.0	-05.0	-08.0	-07.3	-04.8	-08.2	-08.1	03.0	02.9	02.5	90	69	73	77	WNW	1	-	0	E	1	
4	929.5	927.2	927.9	-13.8	-04.6	-10.0	-09.6	-04.5	-14.0	-16.0	01.6	02.7	02.3	74	62	80	72	E	2	WNW	1	-	0	
5	921.2	920.3	926.9	-07.0	-10.2	-11.2	-09.9	-06.0	-11.2	-11.5	03.2	02.6	02.3	89	90	90	90	SE	2	WSW	2	-	0	
6	931.7	930.4	930.5	-12.8	-11.4	-12.6	-12.4	-10.8	-12.8	-13.0	02.0	02.3	02.1	88	89	88	88	-	0	-	0	-	0	
7	930.8	929.3	931.9	-13.7	-09.5	-12.8	-12.2	-07.9	-13.7	-13.9	01.9	02.1	02.0	87	71	88	82	-	0	NSM	1	-	0	
8	935.3	933.5	933.7	-15.0	-12.1	-13.2	-13.4	-12.0	-15.2	-19.0	01.7	02.1	01.9	86	86	88	87	-	0	-	0	NW	2	
9	933.3	931.2	932.2	-13.8	-11.6	-13.2	-13.0	-11.0	-13.8	-16.8	01.8	02.1	01.9	87	83	88	86	-	0	-	0	-	0	
10	934.5	936.3	939.7	-14.4	-10.6	-12.3	-12.4	-10.6	-14.4	-15.5	01.7	01.9	01.8	87	68	77	77	-	0	WNW	1	-	0	
11	944.2	945.9	949.7	-13.3	-07.4	-14.4	-12.4	-07.2	-14.4	-15.5	01.9	02.2	01.6	85	63	80	76	-	0	MNW	2	WSW	1	
12	949.1	946.5	946.4	-17.2	-07.4	-15.0	-13.7	-07.3	-18.8	-22.0	01.2	01.8	01.4	76	50	76	67	E	2	-	0	E	2	
13	945.9	944.0	944.3	-19.8	-08.7	-13.3	-13.8	-07.7	-19.9	-22.6	01.1	01.8	01.9	82	58	81	74	-	0	MSW	1	-	0	
14	943.8	939.2	942.6	-16.8	-09.6	-11.4	-12.3	-08.5	-17.4	-20.0	01.5	01.9	02.1	89	65	84	79	-	0	-	0	-	0	
15	949.7	948.8	949.0	-13.8	-06.6	-06.0	-08.1	-05.7	-13.9	-16.0	01.9	02.5	02.8	91	67	70	76	-	0	-	0	-	0	
16	947.2	944.3	944.4	-06.0	-00.4	-05.8	-04.5	-03.2	-06.2	-08.2	03.2	04.1	03.3	81	70	84	78	-	0	-	0	NW	1	
17	940.3	937.3	935.4	-07.2	-05.6	-07.4	-06.9	-05.3	-07.5	-07.5	03.3	03.2	02.9	93	80	84	86	-	0	NW	1	-	0	
18	931.6	928.2	930.1	-08.8	-02.0	-06.7	-06.1	-01.6	-09.2	-09.6	02.9	03.1	03.3	92	59	89	80	-	0	-	0	-	0	
19	928.8	928.0	930.4	-03.8	03.0	00.4	00.0	03.4	-06.8	-09.5	04.4	04.9	06.3	94	65	95	85	E	1	-	0	E	1	
20	932.7	933.0	935.2	03.6	03.8	01.6	01.9	03.8	00.4	-00.6	06.2	06.0	06.6	97	74	97	89	-	0	-	0	-	0	
21	937.0	938.1	939.4	00.0	03.8	01.8	01.9	04.9	-00.2	-01.5	05.9	06.2	06.3	97	77	90	88	ENE	3	NE	1	-	0	
22	938.5	938.3	938.8	06.8	09.4	10.3	09.2	10.6	01.0	-01.2	06.4	07.7	08.2	65	66	66	66	S	2	SSW	2	S	2	
23	947.0	939.6	938.3	10.7	12.1	10.6	11.0	13.2	10.2	05.5	08.1	08.0	07.5	63	57	59	60	WSW	3	WSW	3	SW	2	
24	932.8	932.4	938.9	12.1	10.8	-00.6	05.4	13.8	-00.6	06.3	06.5	06.8	05.7	46	52	98	65	S	4	S	3	WNW	1	
25	941.5	938.8	939.7	-05.2	02.0	-00.6	-01.1	03.2	-05.2	-06.8	03.8	05.1	05.6	91	72	96	86	ESE	1	M	1	-	0	
26	938.1	935.4	935.2	-02.4	10.0	07.6	05.7	10.2	-02.8	-05.0	04.3	04.9	04.8	83	40	46	56	ESE	2	S	4	SW	3	
27	934.3	933.5	936.4	07.3	09.2	05.2	06.7	10.0	05.2	04.5	04.6	05.5	08.0	45	48	90	61	S	4	S	3	-	0	
28	941.3	941.1	942.1	00.6	01.4	01.0	01.0	05.6	00.5	-00.3	06.1	05.0	05.0	95	74	75	81	-	0	-	0	-	0	
29	945.3	948.6	952.3	-00.8	00.6	00.6	00.3	01.0	-01.3	-03.2	04.4	04.7	04.7	77	73	73	74	-	0	NW	1	ESE	2	
30	949.6	945.9	946.5	-03.8	06.0	-01.4	-00.2	06.7	-04.1	-06.0	03.5	03.7	04.7	77	39	85	67	ESE	2	MSW	2	MSW	1	
31	950.5	949.3	945.9	-01.0	05.2	00.2	01.2	05.6	-02.5	-04.2	05.2	04.0	05.1	92	46	83	74	-	0	WSW	1	NNE	2	
M.																								
VR	937.7	936.5	937.7	-06.2	-01.7	-04.8	-04.4	-00.9	-07.4	-08.7	03.5	03.8	03.9	83	67	82	77	0.9	1.0	0.7				

1	943.7	942.9	941.1	-00.8	10.0	05.2	04.9	11.0	-01.2	-03.0	04.6	05.6	05.3	80	46	60	62	-	0	-	0	-	0
2	939.6	936.8	937.2	01.6	07.2	05.8	05.1	07.3	01.6	-02.8	05.6	06.7	06.8	82	66	73	74	ENE	1	-	0	-	0
3	939.4	938.4	946.0	01.4	09.8	00.4	03.0	11.3	00.4	-01.0	06.3	05.1	02.8	93	42	44	60	-	0	W	2	N	5
4	949.7	950.4	950.5	-05.2	00.0	-04.2	-03.4	01.2	-05.4	-07.0	01.6	01.5	01.5	38	24	34	32	NW	2	NNW	3	-	0
5	948.3	944.6	943.4	-06.2	04.0	00.8	-00.2	05.6	-07.6	-09.2	02.0	02.1	03.2	51	26	50	42	ESE	2	-	0	-	0
6	941.5	940.4	938.9	-00.6	05.8	04.0	03.3	06.5	-00.6	-09.2	05.1	06.1	06.3	88	66	77	77	ESE	1	-	0	-	0
7	937.2	935.2	940.0	-00.8	11.6	02.4	03.9	12.2	-00.8	-03.0	05.3	05.2	05.9	93	38	81	71	ESE	1	WNW	2	ESE	4
8	940.6	939.7	936.6	00.2	06.6	04.4	03.9	06.8	00.2	-00.4	05.6	05.4	06.3	90	56	72	73	-	0	WNW	1	MSW	3
9	933.3	931.7	929.3	09.3	12.2	11.8	11.2	13.6	04.4	03.6	08.3	08.2	08.1	72	57	59	63	NW	2	S	3	SW	3
10	925.0	926.1	922.9	10.2	09.4	09.8	09.8	13.0	07.8	08.0	08.3	11.0	08.2	67	93	67	76	S	2	-	0	ESE	1
11	923.9	926.6	930.0	-03.4	-05.6	-07.6	-06.1	10.0	-07.6	-04.8	04.7	03.3	03.2	99	82	93	91	NNW	1	NW	2	-	0
12	937.8	931.0	933.2	-09.9	-08.8	-13.3	-11.3	-07.4	-13.4	-10.4	02.5	01.9	01.4	85	60	65	70	-	0	-	0	ESE	2
13	933.6	934.3	937.6	-16.8	-08.0	-13.6	-13.0	-07.0	-17.0	-18.7	01.3	01.6	01.6	81	48	74	68	-	0	W	1	ESE	1
14	941.0	940.7	940.7	-18.4	-05.0	-08.8	-10.3	-05.0	-18.4	-20.0	01.1	01.5	02.3	79	36	72	62	ESE	2	MSW	1	E	2
15	938.0	936.7	943.0	-10.2	-01.0	-04.4	-05.0	00.8	-10.7	-13.2	02.2	05.1	03.9	77	89	88	85	ESE	2	E	1	-	0
16	948.7	951.0	952.7	-09.0	-01.3	-12.0	-08.6	-00.5	-12.0	-11.4	02.4	01.7	01.4	79	31	56	55	-	0	N	3	ESE	2
17	948.3	944.0	943.6	-15.4	-05.4	-07.8	-09.1	-05.4	-16.0	-17.4	01.2	01.9	03.2	67	46	95	69	SE	2	W	1	-	0
18	944.0	943.7	947.9	-08.4	-05.8	-10.2	-08.7	-04.9	-10.4	-16.2	03.1	01.3	01.6	95	32	56	61	-	0	NW	2	NNE	1
19	946.8	946.0	949.0	-11.6	-05.5	-08.4	-08.5	-05.2	-11.6	-12.4	02.3	02.4	01.7	89	59	53	67	-	0	WNW	1	W	1
20	951.6	952.7	953.0	-10.0	-04.8	-07.8	-07.6	-04.4	-10.3	-12.4	02.6	02.4	02.1	91	57	62	70	-	0	WNW	2	-	0
21	953.7	950.9	951.7	-13.2	-01.8	-06.8	-07.2	-00.8	-13.8	-15.2	01.9	01.6	02.1	88	29	58	58	-	0	WNW	1	ESE	1
22	951.0	951.3	953.0	-11.8	00.0	-05.2	-05.6	02.5	-11.8	-16.4	01.9	01.8	01.9	77	30	46	51	ESE	1	WNW	1	E	1
23	954.5	954.6	954.8	-09.2	-02.7	-05.5	-05.7	-01.6	-10.6	-12.0	02.2	03.5	02.5	73	69	61	68	-	0	MSW	2	-	0
24	952.0	947.9	951.0	-13.1	-05.6	-04.5	-06.9	-04.5	-13.1	-14.9	01.9	03.6	04.1	85	90	94	90	-	0	WSW	1	W	2
25	956.6	955.6	954.5	-09.6	03.8	00.6	-01.2	04.2	-09.6	-09.8	02.5	02.7	04.6	86	33	72	64	SE	1	-	0	-	0
26	954.3	953.5	953.2	-02.6	05.2	00.8	01.1	07.0	-03.2	-12.0	04.7	04.5	05.8	94	51	90	78	-	0	WNW	1	ESE	1
27	952.4	953.3	953.0	-01.8	03.8	01.0	01.0	04.6	-01.8	-03.2	05.2	05.7	05.9	96	71	90	86	-	0	WNW	1	-	0
28	952.2	950.6	950.0	-02.6	03.4	02.1	01.3	05.2	-02.8	-04.5	04.7	05											

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$$H_a = 630 = H_b = 637.0 = h_c + 2.0 = h_r + 1.0 \text{ m}$$

Dan	Valjivost 0-9	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivac h cm	Razvoj vremena w
		14	7	14	21	Sred Diaz				
1	5	10*	10	10	10.0	00.0	02.7	04	* 0-11 ¹⁵ 15 ²⁰ 16 ²⁰ = 0-24, ☐	
2	5	10*	10*	10*	10.0	00.0	00.9	06	= 0-24, * 2 ²⁰ 24, ☐	
3	6	10	10*	05	06.3	00.0	05.5	11	= 0-24, * 0-4 ²⁰ , 8-19 ²⁰ , ☐	
4	6	09	06☉	00	05.3	02.4	00.4	10	= 0-24, ☐	
5	3	10*	10*	10	10.0	00.0	03.7	11	= 0-13, * 3 ¹⁵ 20, = 13-24, ☐	
6	5	10*	10*	10*	10.0	00.0	17.4	39	= 0-24, * 4 ²⁰ 24, ☐	
7	6	10	09*	10*	09.7	00.5	24.0	53	= 0-24, * 0-3 ⁰⁵ 7 ⁰⁵ 24; ☐	
8	6	05	10	10*	08.3	00.0	01.1	50	= 0-24, * 0-2 ⁰⁵ 15 ⁰⁵ 24; ☐	
9	5	09	10*	10*	09.7	00.0	02.0	45	* 0-6 ²⁰ = 0-24, * 10 ¹⁵ 24; ☐	
10	6	10	07	10	09.0	00.0	05.5	50	= 0-24, * 0-10 ²⁰ 15 ¹⁵ 16 ²⁰ ; ☐	
11	6	04*	06	05	05.0	00.0	00.5	41	= 0-24, * 0 ¹⁵ 10 ¹⁵ ; ☐	
12	6	08	09☉	00	07.7	06.2	00.0	38	= 0-24, ☐	
13	5	05	00☉	00	01.7	04.7	.	36	= 0-24, ☐	
14	4	03	08	04	05.0	00.0	.	34	= 0-24, ☐	
15	4	00	07	10	05.7	00.0	.	32	= 0-24, ☐	
16	4	10	04	10	08.0	00.0	.	29	= 0-24, ☐	
17	5	10	10	10	10.0	00.0	.	28	= 0-24, ☐	
18	5	04	00☉	03	01.3	01.4	.	27	= 0-24, 25 ²⁰ 24; = 21-23 ²⁰ ; ☐	
19	5	10*	10	10	10.0	00.0	00.0	27	= 0-20, * 6 ¹⁵ 9 ²⁰ = 20-24, ☐	
20	4	10	10	10	10.0	00.2	00.0	23	= 0-7, = 7-14 ²⁰ 17 ²⁰ 24; * 15 ²⁰ 18 ¹⁵ ; ☐	
21	6	07	10	04	07.0	00.6	00.6	20	= 0-3, = 4-17, * 8 ¹⁵ 9 ¹⁵ ; ☐	
22	8	04	10	07	07.0	01.2	00.0	16	* 2 ²⁰ 5 ²⁰ , * 9 ¹⁵ 11 ¹⁵ 17 ¹⁵ ; ☐	
23	8	05	10	04	06.3	00.8	.	07	F. # 0-11 ⁰⁰ ; ☐	
24	8	08	10*	10*	09.3	00.6	.	.	F. # 3-13 ²⁰ ; * 14 ²⁰ 19 ¹⁵ , * 19 ¹⁵ 23 ¹⁰ ; = 19 ²⁰ 24, ☐	
25	8	00	10	10	06.7	03.6	12.6	09	= 0-20, 16-24; ☐	
26	8	03	01☉	03	02.3	07.0	.	05	= 0-5 ¹⁵ , * 13 ¹⁵ 19 ¹⁵ 22 ¹⁵ 23 ¹⁰ ; ☐	
27	8	07	10	10*	09.0	00.2	.	.	F. # 0 ¹⁵ 5 ¹⁰ ; * 17 ²⁰ 24; ☐	
28	6	10*	10	05	08.3	00.0	11.2	.	* 0-4 ²⁰ , * 6 ¹⁵ 11 ¹⁵ = 11 ¹⁵ 20 ²⁰	
29	6	10*	10	10	10.0	00.0	00.2	.	* 6 ²⁰ 12 ¹⁵ ; = 8-24; ☐	
30	6	00	00☉	00	00.0	08.3	00.1	.	= 0-24, = 0-10, 13-24	
31	7	10	02☉	01	04.3	04.1	01.0	01	= 0-10 ¹⁵ , = 0-9 ²⁰ 24; * 1 ²⁰ 5 ¹⁵ ; ☐	
M.										
VR.	07.1	07.4	06.7	07.1	41.8	85.7				

1	8	10	04☉	10	08.0	07.5	.	.	☐ 0-7 ⁰⁵ = 6-13 ¹⁵ * 7 ⁰⁵ 8 ¹⁵
2	6	09	09	10	09.3	00.1	00.0	.	= 12-24, * 13 ²⁰ 20 ²⁰ 22 ²⁰ 24
3	7	05	06☉	08	06.3	06.0	07.4	.	= 0-3 ⁰⁵ = 0-2 ⁰⁵ 8-13 ²⁰ ; ☐ 22-24
4	8	01	00☉	00	00.3	09.1	.	.	☐ 0-11 19-24
5	8	09	09☉	00	06.0	05.5	.	.	☐ 0-11 ¹⁵ 13-24; = 18 ²⁰ 24
6	8	01	10	10	07.0	00.3	.	.	= 0-2 ⁰⁰ 20 ²⁰ 24; ☐ 0-9; * 12 ²⁰ 14 ¹⁰
7	7	05	00☉	10*	05.0	16.4	00.0	.	☐ 2 ²⁰ 9 ¹⁵ ; * 15 ²⁰ 21 ²⁰ = 20-24, * 21 ²⁰ 22 ²⁰
8	7	10	06☉	10	08.7	01.0	00.3	.	= 0-11 ²⁰ ; * 21 ²⁰ 24
9	8	10*	10	07	09.0	00.9	00.4	.	* 0-10 ²⁰ !
10	7	10	10*	10*	10.0	00.1	00.4	.	* 7 ²⁰ 14 ¹⁵ 18 ²⁰ 24
11	5	10*	10*	10*	10.0	00.0	05.4	.	* 0-5 ²⁰ = 1 ²⁰ 24, * 5 ²⁰ 24, ☐
12	6	10*	10*	00	06.7	00.0	22.0	24	* 0-14 ²⁰ = 0-17 ²⁰ ; ☐
13	6	06	00☉	00	02.0	07.3	04.8	21	= 11 ²⁰ 24; ☐
14	6	00	00☉	00	00.0	08.7	.	18	= 0-4 ²⁰ 8 ²⁰ 24; ☐
15	5	10	10*	10*	10.0	00.0	.	16	= 0-24, * 10 ²⁰ 24, ☐
16	6	06	00☉	00	02.0	08.8	10.8	25	* 0-5 ¹⁵ = 0-13; ☐
17	6	10	10	10*	10.0	00.0	.	24	= 0-24, * 14-22 ²⁰ ; ☐
18	7	10	05☉	07	07.3	04.9	03.2	27	= 0-11, * 23 ²⁰ 24; ☐
19	6	10*	10*	10	10.0	00.2	00.4	23	* 0-14 ²⁰ ; * 15 ²⁰ 16 ²⁰ ; ☐
20	7	10*	09*	06	08.3	00.2	01.7	25	* 0 ¹⁵ 8 ²⁰ 15 ²⁰ 16 ¹⁵ 21 ²⁰ 24; = 4 ²⁰ 8 ¹⁵ ; ☐
21	7	00	08☉	03	03.7	06.8	00.5	20	* 0-1 ²⁰ = 0 ²⁰ 13 ¹⁵ ; ☐
22	6	03	01☉	00	01.3	08.9	.	19	= 9-17; ☐
23	6	10	07	09	08.7	00.8	.	17	= 3-15, * 6 ¹⁵ 15 ²⁰ ; ☐
24	5	02	10*	10*	07.3	00.0	00.1	16	= 7 ²⁰ 22 ²⁰ ; * 8 ²⁰ 21 ¹⁰ ; ☐
25	6	00	00☉	02	00.7	07.1	05.8	23	= 5-13 ²⁰ ; ☐
26	6	10	09	10	09.7	01.3	.	18	= 4 ²⁰ 24; ☐
27	5	10	10	08	09.3	00.0	.	12	= 0-24; ☐
28	6	04	10	10	08.0	02.1	.	09	= 0-19; = 19-24, * 21 ²⁰ 24; ☐
M.									
VR.	06.8	06.5	06.4	06.6	94.0	63.2			

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. ΔG = + 1h 14 min.

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T °C							Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina vetra D, f (0-12)						
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	949.1	948.6	948.8	01.0	07.6	04.2	04.3	09.5	00.8	-00.4	06.4	06.1	07.1	97	59	86	81	-	0	-	0	-	0	
2	948.4	946.6	943.4	02.4	08.3	06.6	06.0	08.5	02.4	00.0	06.8	05.7	06.5	94	52	67	71	ESE	1	-	0	-	ENE 1	
3	938.8	939.2	942.3	05.4	08.6	04.0	05.5	09.6	04.0	03.6	06.0	07.0	06.6	66	62	81	70	ESE	2	WNW	1	-	ENE 2	
4	945.2	944.8	947.7	01.2	12.0	03.9	05.2	12.5	00.9	-01.0	06.1	07.2	06.1	93	51	75	73	-	0	W	1	-	ESE 2	
5	950.0	950.3	952.4	01.2	16.6	05.8	07.4	16.6	01.0	-00.9	05.6	04.0	05.9	84	21	64	56	ESE	4	W	2	SE	1	
6	954.1	953.3	953.9	01.8	15.4	06.4	07.5	16.0	01.8	00.6	06.0	05.2	05.9	86	29	62	59	ESE	1	WNW	2	-	ENE 2	
7	953.5	953.0	950.5	02.4	16.4	07.6	08.5	16.7	02.4	00.0	06.1	05.5	05.4	84	29	52	55	ESE	3	WNW	2	E	ENE 2	
8	951.9	951.4	954.8	02.0	10.8	06.0	06.2	13.8	02.0	00.3	05.9	06.9	07.6	84	53	81	73	ENE	1	WNW	1	WNW	2	
9	952.7	951.2	955.0	03.6	05.2	00.6	02.5	06.0	00.6	03.0	07.4	04.9	06.3	94	56	98	83	NW	2	WNW	1	WNW	1	
10	952.4	950.5	949.9	-03.2	01.2	00.4	00.5	01.5	-00.4	-00.6	05.9	06.2	06.2	98	93	98	96	-	0	NW	2	-	ENE 2	
11	947.0	945.6	946.3	-01.2	00.2	00.2	-00.2	01.0	-01.2	-03.5	05.4	05.8	06.0	96	93	97	95	-	0	-	0	-	ENE 2	
12	947.0	948.8	950.3	00.0	01.8	00.6	00.8	02.2	-00.1	-01.0	05.9	06.6	06.2	97	95	97	96	-	0	WNW	1	WNW	1	
13	948.4	945.0	942.5	-00.2	02.8	02.0	01.7	02.8	-00.2	-00.8	05.8	06.4	06.5	96	86	92	91	WNW	1	-	0	-	ENE 2	
14	938.3	935.0	934.1	01.0	04.0	03.2	02.9	04.3	00.8	-00.6	06.2	07.2	07.3	95	88	96	93	-	0	-	0	-	ENE 2	
15	931.6	931.0	932.6	02.4	06.4	04.8	04.6	08.7	02.4	01.5	07.2	08.0	08.1	98	83	94	92	-	0	SSW	1	-	ENE 2	
16	931.9	930.8	931.0	02.4	08.2	05.0	05.2	09.5	02.0	01.0	06.8	05.2	05.2	94	48	60	67	-	0	WSW	3	ESE	1	
17	926.2	923.6	923.0	05.6	08.4	01.8	04.4	09.5	01.8	01.0	03.5	05.4	05.6	39	49	81	56	W	2	S	2	-	ENE 2	
18	924.4	921.6	920.7	-00.8	07.6	03.0	03.2	08.9	-00.8	-03.5	04.6	03.8	07.2	81	37	95	71	ESE	1	-	0	-	ESE 2	
19	921.5	922.5	926.1	02.0	07.8	03.4	04.2	08.2	01.8	00.7	06.6	05.3	05.9	94	50	75	73	-	0	W	2	W	2	
20	929.5	931.2	932.8	-00.2	11.2	04.2	04.9	12.0	-00.2	-02.0	05.6	03.4	04.8	93	25	58	59	ESE	1	MSW	2	ESE	1	
21	931.9	931.3	931.0	05.0	12.0	08.2	08.4	12.8	03.8	01.9	04.6	06.4	07.5	52	46	69	56	ESE	2	WSW	1	ESE	2	
22	929.9	928.8	930.0	07.2	13.9	09.2	09.9	14.5	06.8	04.2	06.9	05.8	06.4	68	36	55	53	ESE	2	-	0	-	ENE 2	
23	929.7	929.9	932.7	06.0	10.6	06.4	07.4	12.6	05.6	03.6	08.0	07.4	07.6	85	58	79	74	-	0	ENE	1	N	1	
24	934.4	935.3	937.3	03.0	11.6	07.2	07.3	13.4	02.6	00.5	06.7	06.2	06.6	88	45	65	66	ESE	2	SW	3	-	ENE 2	
25	936.9	941.2	941.3	03.2	07.4	04.4	04.9	10.5	01.4	00.0	05.9	07.7	06.2	76	75	75	75	ESE	3	SE	1	ESE	1	
26	942.4	939.7	939.2	01.2	11.4	05.2	05.8	12.6	00.8	-00.6	06.2	04.7	04.2	93	35	47	58	ESE	2	-	0	-	ENE 2	
27	938.6	932.7	931.3	00.6	17.8	11.0	10.1	18.6	00.6	-01.4	04.7	04.5	05.0	73	22	38	44	ESE	2	W	3	S	3	
28	930.1	931.9	939.4	07.2	07.2	01.2	04.2	11.4	01.2	04.5	07.6	09.1	06.2	75	90	93	86	S	3	ESE	1	NW	2	
29	943.9	944.0	946.3	-01.0	04.0	00.4	01.0	04.6	-01.8	-03.4	05.1	04.0	04.2	89	50	66	68	WNW	1	-	0	-	ESE 2	
30	946.6	946.5	945.6	-04.0	11.4	04.2	04.0	12.3	-04.2	-05.4	03.9	02.7	05.7	86	20	69	58	ESE	2	W	1	ESE	3	
31	943.4	941.5	941.7	01.2	18.2	08.6	09.2	18.2	00.5	-01.1	04.3	02.1	03.8	65	10	34	36	ESE	3	WNW	2	SSE	1	
M.																								
VR	940.4	939.6	940.4	02.0	09.2	04.5	05.1	10.2	01.3	00.0	05.9	05.7	06.1	84	53	74	70		1.3		1.2		1.0	

1	944.7	944.7	945.7	03.6	11.8	07.0	07.4	15.0	03.0	00.5	05.6	08.3	05.1	71	60	51	61	-	0	-	0	S	1
2	945.7	942.6	941.7	01.6	19.2	12.2	11.3	19.6	01.4	-00.4	06.0	03.6	05.5	87	16	38	47	ESE	1	W	1	E	3
3	945.2	947.5	949.0	07.6	11.4	09.2	09.4	12.2	06.8	06.3	09.9	09.7	09.0	95	72	78	82	-	0	W	1	-	ENE 3
4	947.6	944.8	943.6	04.0	20.6	11.2	11.8	20.6	03.2	01.4	07.2	06.2	06.4	88	26	48	54	ESE	3	WSW	2	-	ENE 3
5	942.1	940.4	940.3	06.0	20.6	13.4	13.4	20.6	05.0	03.0	06.9	06.2	06.0	74	26	39	46	-	0	SSW	3	S	2
6	938.6	938.9	938.5	12.8	15.2	11.8	12.9	17.0	11.4	08.6	05.7	06.2	07.5	39	36	54	43	SW	2	SW	3	SSW	3
7	938.0	938.0	939.9	11.4	15.2	06.8	10.1	15.7	06.2	08.7	08.3	06.6	08.3	62	38	84	61	S	2	S	1	ESE	2
8	938.3	935.7	936.0	05.8	19.5	14.2	13.4	19.6	03.0	01.0	07.0	07.9	06.8	76	35	42	51	SW	1	W	4	S	3
9	935.4	933.1	933.5	10.0	21.6	18.0	16.9	23.2	09.0	05.6	06.6	09.1	07.7	54	35	37	42	-	0	-	0	S	3
10	935.0	932.6	935.9	18.4	24.3	17.0	19.2	24.4	16.6	12.2	06.8	05.3	06.3	32	17	32	27	SSE	6	SSW	5	-	ENE 2
11	942.3	939.7	939.0	09.2	16.4	07.8	10.3	17.2	07.8	05.5	06.1	06.2	08.9	52	33	84	56	WSW	2	W	2	ESE	1
12	936.2	932.3	929.0	05.4	12.4	06.0	07.5	14.5	03.9	01.4	07.0	05.9	08.1	78	41	87	69	ESE	1	-	0	-	ENE 2
13	933.1	937.2	936.6	03.0	08.0	05.0	05.3	10.8	02.5	02.0	07.1	05.6	06.1	94	52	70	72	-	0	-	0	-	ESE 2
14	936.8	937.7	938.5	03.6	12.2	09.4	08.7	12.8	01.4	-00.8	06.1	05.5	04.8	77	38	40	52	SE	2	SW	2	S	3
15	938.3	940.0	943.2	06.1	08.4	05.0	06.1	10.0	04.6	03.5	05.6	07.6	08.2	60	69	94	74	E	3	-	0	-	ENE 2
16	944.0	945.7	945.9	00.7	01.4	01.6	01.3	05.2	00.4	-00.1	06.1	06.3	06.4	95	93	94	94	-	0	-	0	-	ENE 2
17	943.0	941.9	942.5	00.8	03.0	00.6	01.3	03.0	00.5	00.0	06.3	07.3	06.3	97	97	98	97	-	0	-	0	-	ENE 2
18	941.5	942.6	942.8	01.6	04.7	05.0	04.1	05.6	00.4	-00.4	06.2	07.7	08.2	90	90	94	91	-	0	-	0	-	ENE 2
19	942.5	942.6	942.8	05.2	09.2	06.4	06.8	09.6	04.6	03.6	07.9	07.6	08.3	89	65	87	80	ENE	1	NE	2	-	ENE 2
20	941.0	940.3	941.1	05.2	11.2	06.6	07.4	12.4	05.0	04.0	08.4	06.0	07.2	94	45	74	71	-	0	-	0	-	ENE 2
21	941.4	942.0	944.0	04.4	17.8	10.0	10.6	17.8	02.6	00.5	07.2	04.6	06.3	86	23	52	54	E	2	-	0	-	ENE 2
22	944.4	941.0	939.0	04.8	19.0	12.0	12.0	19.2	04.6	00.5	07.6	04.9	06.4	89	22	45	52	ESE	2	NNE	1	-	ENE 2
23	935.9	932.3	932.8	06.6	19.0	12.8	12.8	19.6	05.0	02.4	07.3	05.9	05.9	74	27	40	47	ESE	3	WNW	1	WNW	2
24	933.0	932.2	938.6	08.0	17.8	06.2	09.6	19.1	06.0	04.0	08.1	07.2	07.5	76	35	79	63	ESE	2	NW	3	SSE	2
25	943.2	940.8	939.9	00.0	11.2	07.1	06.4	12.7	00.0	-00.5	05.9	02.2	04.8	97	22	47	55	-	0	-	0	-	ESE 3
26	938.9	935.2	933.5	04.4	16.8	12.8	11.7	19.2	03.8	02.0	07.1	06.4	07.8	84	34	53	57	ESE	1	SSW	2	-	ENE 2
27	936.7	934.4	934.0	07.0	15.2	12.0	11.6	15.6	07.0	06.0	09.2	10.4	07.9	92	60	56	69	-	0	-	0	-	ENE 2
28	929.6	927.6	925.2	12.4																			

Dan	Vrijeme 0-9	Oblačnost N (0-10)				Insolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
		14	7	14	21				
1	1 10	09	06	08.3	01.7	00.5	09	0-19 ³⁰ , 0-2 ³⁰ 8 ³⁰ 10 ⁴⁵ , 13 ³⁰ 24, 17	
2	7 10	10	10	10.0	00.0	00.2	04	0-2 ³⁰ , 4 ³⁰ 5 ³⁰ 17	
3	7 10	10	09	09.7	00.0	.	01	F 2 ³⁰ , 13 ³⁰ 20, 17	
4	6 09	00	00	03.0	09.6	.	.	L 2 ³⁰ 8 ³⁰ 22-24, 5-14 ³⁰	
5	7 06	04	00	03.3	09.5	.	.	L 0-8, 22-24, 8-12 ³⁰	
6	8 05	08	00	04.3	08.1	.	.	L 0-8, 20 ³⁰ 24	
7	8 00	04	04	02.7	08.6	.	.	Δ 0-8, 20 ³⁰ 24	
8	7 10	10	09	09.7	00.0	.	.	Δ 0-8 ³⁰	
9	6 10	10	10*	10.0	00.0	00.0	.	● 6 ³⁰ 17 ³⁰ , 9 ³⁰ 24, 17 ³⁰ 20, * 20-24	
10	5 10*	10*	10*	10.0	30.0	08.0	02	* 0-24, = 0-24, 17	
11	4 10	10*	10	10.0	00.0	14.6	13	* 0-1 ³⁰ 8 ³⁰ 20, = 0-24, 17	
12	6 10	10*	10*	10.0	00.0	07.2	17	= 0-24, * 1 ³⁰ 14 ³⁰ , 13 ³⁰ 21 ³⁰ , ● 14 ³⁰ 18 ³⁰ , * 18 ³⁰ 24, 17	
13	4 10*	10*	10	10.0	00.0	02.5	06	= 0-24, * 0-4, 4 ³⁰ 13 ³⁰ 14 ³⁰ 17	
14	5 10*	10*	10	10.0	00.0	00.1	01	= 0-24, ● 2 ³⁰ 13 ³⁰ , * 6 ³⁰ 7 ³⁰ 17	
15	5 10	10	09	09.7	00.3	02.4	.	= 0-1 ³⁰ 9-14 ³⁰ , = 1 ³⁰ 9, 9 ³⁰ 14 ³⁰ , H ³⁰ 14, 17 ³⁰ 19	
16	7 09	10	02	07.0	00.5	04.3	.	= 0-1 ³⁰ 3-6 ³⁰ 23 ³⁰ 24, F 11 ³⁰ 15 ³⁰	
17	7 00	09	10*	06.3	03.7	00.3	.	● 0-2 ³⁰ 7 ³⁰ 10 ³⁰ 11 ³⁰ 13 ³⁰ 19 ³⁰ 21 ³⁰ 22 ³⁰ , F 13 ³⁰ 14 ³⁰ , = 20 ³⁰ 24, * 22 ³⁰ 24	
18	7 02	10	10*	07.3	02.5	09.3	01	* 0-4 ³⁰ , = 0-5 ³⁰ F 10 ³⁰ 17 ³⁰ , 14 ³⁰ 23, 17	
19	7 10	08	10	09.3	00.6	04.7	.	= 6 ³⁰ 14 ³⁰ , 7 ³⁰ 14 ³⁰ 10 ³⁰ 14 ³⁰ 16 ³⁰	
20	8 06	02	05	04.3	09.6	00.3	.	Δ 0-3, 20-24, L 3-8, = 5-8 ³⁰	
21	8 07	10	05	07.3	00.0	.	.	Δ 0-6 ³⁰	
22	8 09	10	03	07.3	00.0	.	.	Δ 0-5 ³⁰ 20 ³⁰ 24	
23	7 10*	07	05	07.3	02.5	00.2	.	Δ 0-1 ³⁰ 13 ³⁰ 14 ³⁰ 12 ³⁰ 13 ³⁰	
24	8 01	04	07	04.0	05.0	00.2	.	Δ 0-8 ³⁰ 20-24, ● H ³⁰ 12 ³⁰ 15	
25	7 08	09	00	05.7	05.0	00.4	.	Δ 0-8 ³⁰ 18 ³⁰ 24, ● H ³⁰ 13	
26	7 07	10	00	05.7	00.0	00.6	.	Δ 0-4, L 4-7 ³⁰	
27	8 00	05	00	01.7	10.2	.	.	Δ 0-3, L 3-8 7 ³⁰	
28	7 10*	10*	10*	10.0	01.5	00.2	.	● 3 ³⁰ 19 ³⁰ , * 17 ³⁰ 19 ³⁰ , * 13 ³⁰ 24, 17	
29	6 07	07	00	04.7	00.9	25.8	09	* 0-5 ³⁰ , = 9 ³⁰ 14 ³⁰ , V 20-24	
30	8 02	00	00	00.7	10.5	.	.	V 0-9 ³⁰ , = 20 ³⁰ 24	
31	8 04	00	10	04.7	10.7	.	.	Δ 0-8 ³⁰	
M.									
VR.		07.2	07.6	05.9	06.9	101.0	81.8		

1	7 09	08	00	05.7	04.1	.	.	= 9 ³⁰ 11
2	8 03	03	02	02.7	10.5	.	.	Δ 0 ³⁰ 9 ³⁰
3	7 10*	09	10	09.7	00.0	05.3	.	● 0 ³⁰ 8, Δ 20 ³⁰ 24
4	8 00	01	00	00.3	10.8	00.4	.	Δ 0-8
5	8 00	00	00	00.0	10.9	.	.	Δ 0-8, F 22 ³⁰
6	8 05	09	09	07.7	04.6	.	.	F 7 ³⁰
7	8 09	07	00	05.3	03.9	.	.	T 9 ³⁰ 10 ³⁰ , 9 ³⁰ 10 ³⁰ 14 ³⁰ 15 ³⁰ , F 9 ³⁰
8	8 01	03	00	01.3	10.9	07.3	.	F 13 ³⁰
9	8 01	09	08	06.0	07.0	.	.	Δ 0-8, F 11 ³⁰ 14 ³⁰ 16 ³⁰ 23 ³⁰
10	8 07	07	05	06.3	08.0	.	.	F 2 ³⁰ 7 ³⁰ , H ³⁰ 14 ³⁰
11	8 05	05	03	04.3	09.1	.	.	F 17 ³⁰ 17 ³⁰ , F 17 ³⁰ 17 ³⁰ , 17 ³⁰ 18 ³⁰
12	8 05	10	10*	08.3	02.3	00.0	.	Δ 0-8, F 12 ³⁰ 14 ³⁰ , ● 18-24
13	7 10*	05	00	05.0	03.6	05.8	.	● 0-11, 13 ³⁰ 24
14	8 02	09	10	07.0	03.9	01.0	.	Δ 0-8, F 16 ³⁰ 24 ³⁰
15	8 10	10	10*	10.0	00.0	.	.	● 14-24
16	4 10*	10*	10*	10.0	00.0	19.9	02	● 0-4 ³⁰ 18 ³⁰ 24, * 4 ³⁰ 5 ³⁰ 6 ³⁰ 12 ³⁰ 18 ³⁰ = 7-24, 17
17	6 10*	10*	10*	10.0	00.0	19.1	.	● 0-1 ³⁰ 20 ³⁰ 24, * 1 ³⁰ 4 ³⁰ 19 ³⁰ 20 ³⁰ 23 ³⁰ 24, * 4 ³⁰ 6 ³⁰ 20 ³⁰ 23 ³⁰
18	4 10*	10	10	10.0	00.0	21.6	.	= 0-24, * 0-2 ³⁰ , ● 5-11 ³⁰
19	6 10	10	10	10.0	00.0	00.2	.	= 0-10, Δ 20-24
20	7 10*	10	00	06.7	02.1	00.0	.	Δ 0-5 ³⁰ 20 ³⁰ 24, = 5-8 ³⁰ , 5 ³⁰ 8
21	8 00	02	00	00.7	10.3	00.0	.	Δ 0-9, 20-24, = 6 ³⁰ 9
22	7 00	06	05	03.7	10.1	.	.	Δ 0-8, 22-24
23	8 01	06	00	02.3	09.9	.	.	Δ 0-8 ³⁰ 21-24
24	8 09	08	10*	09.0	04.6	.	.	Δ 0-7, ● 20-24, Δ 23 ³⁰ 24
25	0 04	03	00	02.3	09.6	06.7	03	Δ 0-1 ³⁰ , * 1 ³⁰ 4, Δ 20-24, 17
26	8 10*	08	09	09.0	01.4	01.4	.	Δ 0-5 ³⁰ , 5 ³⁰ 7 ³⁰ 22 ³⁰ 24, F 12 ³⁰ 12 ³⁰
27	8 10	06	08	08.0	03.4	18.9	.	● 0-4 ³⁰ 14 ³⁰ 15 ³⁰ 21 ³⁰ 24 ³⁰ , F 6 ³⁰ 22 ³⁰ 24, ● 0 ³⁰ 1
28	8 06	08	10*	08.0	08.2	02.1	.	● 0-4 ³⁰ 20-22, F 20-22, * 22 ³⁰ 24, Δ 24
29	7 10*	08	00	06.0	03.4	18.1	03	Δ 0-1 ³⁰ , ● 1 ³⁰ 2, Δ 2-3, * 3-11, 17
30	8 00	00	04	01.3	11.3	01.0	.	L 0-9, F 14 ³⁰ 15 ³⁰
M.								
VR.		05.9	06.7	05.1	05.9	163.9	128.8	

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T C°						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina vjetro- D, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	938.6	937.9	939.3	07.4	16.4	11.2	11.6	17.4	04.6	01.0	06.5	06.0	06.4	63	32	48	48	MSW	2	W	3	-	0	
2	936.7	933.9	932.7	10.4	16.8	13.6	13.6	18.6	07.5	05.0	07.9	07.5	07.0	63	39	45	49	S	3	S	5	SSW	2	
3	928.0	928.8	935.7	14.8	08.0	04.8	08.1	18.0	04.8	12.0	07.9	09.8	08.1	47	91	94	77	-	0	-	0	MNW	1	
4	935.7	935.9	935.7	05.2	11.2	08.2	08.2	11.8	04.4	03.6	08.4	07.3	09.3	94	55	85	78	-	0	ESE	2	E	2	
5	935.0	934.5	940.2	08.6	17.0	14.2	13.5	19.2	06.5	03.8	10.1	08.7	08.9	90	45	55	63	E	2	S	2	ESE	1	
6	933.3	931.4	930.9	10.0	15.0	13.6	13.1	16.0	09.6	07.0	11.1	15.4	14.6	91	90	94	92	-	0	-	0	E	1	
7	929.5	934.6	939.4	14.4	17.4	10.8	13.4	18.2	10.8	09.5	10.7	09.2	07.8	66	46	60	57	ESE	3	-	0	ESE	5	
8	940.2	942.0	941.3	11.1	15.2	13.2	13.2	16.8	09.4	07.0	08.2	06.1	07.5	62	35	49	49	MSW	2	SSW	2	SSW	2	
9	939.7	938.5	937.6	11.2	15.2	12.6	12.9	18.0	10.5	08.4	08.7	11.1	11.7	66	64	80	70	ESE	2	-	0	-	0	
10	938.4	937.7	939.0	08.6	19.0	13.4	13.6	20.4	06.8	05.0	09.7	10.1	10.3	87	46	67	67	ESE	2	E	2	E	2	
11	939.4	937.9	939.9	12.0	23.8	14.6	16.3	23.8	11.4	09.7	12.2	11.2	13.8	87	38	83	69	-	0	MNW	2	E	1	
12	941.6	940.6	941.9	11.2	26.2	18.2	18.5	26.2	09.6	08.2	11.8	06.7	11.7	89	20	56	55	ESE	1	W	1	ESE	1	
13	943.4	941.0	940.2	13.3	27.1	18.6	19.4	27.2	12.0	10.5	12.7	07.8	09.0	83	22	42	49	ESE	2	-	0	ESE	2	
14	939.4	938.5	938.4	15.4	28.6	18.0	20.0	28.6	12.8	10.6	12.5	09.6	09.5	72	24	46	47	ESE	1	MNW	1	-	0	
15	939.4	934.0	937.2	12.8	26.8	18.6	19.2	27.2	10.0	08.4	10.1	11.6	13.1	68	33	61	54	-	0	-	0	ESE	4	
16	939.7	938.5	940.8	13.8	25.0	15.4	17.4	25.0	13.2	12.2	14.8	11.8	13.0	94	37	74	68	SSE	1	MSW	1	-	0	
17	942.0	941.3	944.2	14.0	26.5	17.2	18.7	26.6	11.5	10.5	14.4	09.2	14.3	90	26	71	62	-	0	NW	2	E	1	
18	943.6	943.6	944.6	12.6	25.4	18.7	18.9	26.2	10.4	08.6	11.7	08.8	08.9	80	27	41	49	-	0	-	0	-	0	
19	945.0	942.9	942.9	14.0	23.4	19.2	19.0	24.6	11.4	09.5	12.8	11.8	10.3	80	41	46	56	ESE	1	W	3	-	0	
20	943.7	940.6	941.0	13.6	26.4	15.8	17.9	26.7	11.0	09.5	12.1	10.1	16.8	78	29	92	66	ESE	1	MSW	1	E	1	
21	938.8	935.0	936.7	13.9	24.4	17.8	18.5	25.2	12.6	11.4	13.8	10.9	12.3	87	36	60	61	ESE	2	W	2	-	0	
22	934.0	933.2	933.0	14.0	22.2	17.4	17.8	23.7	14.0	11.0	15.0	11.0	09.2	94	41	46	60	ESE	2	S	3	W	1	
23	935.3	934.8	935.9	13.0	25.0	18.8	18.9	25.0	10.6	09.0	11.6	09.2	11.7	77	29	54	53	ENE	2	MSW	2	-	0	
24	941.0	941.0	942.9	12.7	24.4	17.4	18.0	24.4	10.0	08.4	11.3	09.5	12.2	77	31	61	56	E	1	SW	1	E	1	
25	945.0	944.6	946.0	13.8	25.8	15.2	17.5	27.0	11.5	10.2	14.3	13.9	16.2	91	42	94	76	-	0	ESE	3	E	1	
26	944.3	942.5	944.3	13.8	21.4	17.2	17.4	22.4	12.6	11.0	14.5	13.0	13.0	92	51	66	70	-	0	MNW	1	-	0	
27	944.0	942.9	944.0	13.8	26.4	18.6	19.4	26.4	12.0	09.8	14.2	07.6	09.9	90	22	46	53	-	0	ESE	2	E	3	
28	943.7	941.3	941.7	13.0	26.4	18.0	18.9	26.4	10.8	08.9	11.9	09.9	13.5	79	29	65	58	E	1	MNW	2	-	0	
29	941.0	938.1	940.4	15.4	26.7	15.0	18.0	26.7	13.0	11.5	14.1	10.4	13.1	81	30	77	63	-	0	-	0	ESE	1	
30	941.1	941.1	943.0	13.4	16.2	13.2	14.0	19.5	12.6	11.5	13.9	12.2	13.9	91	66	92	83	-	0	NNE	2	-	0	
31	944.2	942.4	942.6	13.6	21.0	14.8	16.1	22.2	12.6	11.5	14.6	09.3	13.7	94	37	81	71	-	0	W	2	-	0	
M.	939.5	938.4	939.7	12.4	21.6	15.3	16.2	22.8	10.3	08.8	11.7	09.9	11.3	81	40	66	62	1.0	1.5	1.1				
VR																								

1	943.7	943.2	944.3	13.2	17.2	12.4	13.8	18.3	12.4	12.0	14.5	13.3	13.2	96	68	91	85	W	1	MSW	1	-	0
2	944.0	942.1	942.8	10.1	21.0	14.2	14.9	21.8	09.5	08.8	11.8	10.0	13.9	95	40	86	74	-	0	MSW	1	ENE	1
3	943.4	943.2	945.1	12.6	20.0	15.0	15.7	20.0	11.0	08.8	13.3	12.6	13.6	91	54	80	75	-	0	MSW	2	-	0
4	945.1	945.3	945.0	13.2	19.0	16.2	16.2	19.9	11.7	11.0	14.2	15.2	15.6	94	69	85	83	-	0	-	0	NE	2
5	945.9	943.7	944.0	13.2	26.2	18.5	19.1	26.4	11.0	10.0	13.3	09.5	13.2	87	28	62	59	E	1	MNW	1	-	0
6	944.2	943.0	943.0	14.8	27.6	20.4	20.8	27.6	12.8	11.6	13.9	11.6	11.5	82	31	48	54	ESE	1	MSW	2	-	0
7	943.6	940.8	940.7	15.8	31.4	23.8	23.7	31.4	13.4	11.6	13.9	10.4	10.5	77	23	36	45	ENE	1	W	3	MSW	2
8	939.0	936.4	937.5	18.4	26.6	20.4	21.5	27.8	15.3	13.6	13.2	09.4	14.0	62	27	58	49	E	1	S	2	MNW	1
9	939.6	941.2	945.0	15.2	20.8	13.0	15.5	22.6	12.8	12.6	16.2	12.1	12.5	94	49	83	75	-	0	MNW	1	MNW	1
10	944.8	941.2	941.2	12.2	24.2	17.1	17.7	24.2	11.0	10.2	12.8	07.2	06.5	90	24	34	49	-	0	S	3	SSW	1
11	940.7	943.0	943.4	13.4	10.9	10.2	11.2	17.1	10.2	10.2	12.5	10.6	10.2	82	81	82	82	-	0	W	2	-	0
12	944.2	940.3	940.4	07.8	20.3	15.6	14.8	20.8	05.3	05.0	09.5	07.9	09.9	90	33	56	60	ENE	2	W	1	-	0
13	940.0	939.4	940.4	11.7	23.8	18.6	18.2	23.8	07.8	05.2	10.1	09.4	08.4	73	32	39	48	-	0	SW	2	-	0
14	943.6	941.7	942.5	13.8	27.2	21.1	20.8	27.2	12.6	11.0	11.1	11.0	12.7	70	30	51	50	E	3	W	3	-	0
15	937.5	935.4	941.6	22.2	29.0	17.2	21.4	29.5	16.0	11.2	11.5	11.7	12.5	43	29	64	45	S	2	SM	2	ESE	4
16	945.0	941.9	941.1	13.2	22.0	19.0	18.3	22.2	13.0	12.5	09.4	10.6	14.2	62	40	65	56	ENE	1	-	0	-	0
17	936.6	931.4	939.6	15.2	21.2	09.2	13.7	22.6	09.0	11.0	13.8	13.4	10.8	80	53	93	75	-	0	MSW	5	MNW	1
18	942.6	941.1	942.8	08.1	15.7	11.0	11.5	17.4	06.3	05.5	08.0	05.9	06.9	74	33	52	53	-	0	-	0	ENE	1
19	944.4	942.1	940.7	08.4	19.2	12.8	13.3	19.2	07.0	05.4	10.3	06.2	08.1	94	28	55	59	-	0	SSW	2	ESE	1
20	937.0	935.4	935.4	11.6	15.4	12.3	12.9	17.0	09.5	08.2	08.9	14.1	13.5	72	81	95	83	MSW	1	E	2	-	0
21	935.7	939.9	941.6	10.4	14.8	10.4	11.5	15.0	10.0	08.2	12.0	10.7	11.5	95	64	91	83	W	1	MSW	1	-	0
22	942.6	938.9	937.7	08.2	24.2	18.8	17.5	24.2	06.1	05.1	09.7	04.4	08.2	89	15	38	47	ESE	2	-	0	SW	1
23	936.8	934.0	936.6	14.2	20.0	13.4	15.3	20.0	12.2	05.2	14.2	12.0	10.9	88	51	71	70	NW	3	MSW	2	-	0
24	937.9	937.3	940.2	12.0	20.4	11.2	13.7	21.1	10.5	09.0	13.1	08.8	12.6	93	37	94	75	-	0	MNW	1	E	2
25	942.9	942.9	945.2	09.4	20.8	15.2	15.2	21.8	07.6	07.0	11.2	12.4	10.8	95	50	62	69	E	1	MSW	1	-	0
26	948.6	947.4	946.0	11.4	23.2	16.2	16.8	23.2	09.4	08.1	11.4	07.2	12.8	85	25	70	60	-	0	-	0	ENE	1
27	945.9	941.6	945.0	13.1	25.0	12.8	15.9	26.7	11.0	08.0	12.1	15.1	14.1	80	48	96	75	E	2	W	3	MSW	1
28	941.9	942.1	944.2	13.2	14.8	12.2	13.1	16.0	12.0	11.4	14.2</												

Dan	Validnost 0-9	Oblačnost N (0-10)				Inzolucija broj sati	Padavine R mm	Snežni pokriće h cm	Razvoj vremena w
		14	7	14	21				
1	8	080	080	00	05.3	08.1	.	.	$\Delta 0-8^{20} 20-24; T 12-13^{20}, F-13^{20}$
2	8	060	060	01	04.3	10.1	.	.	$\Delta 0-8^{20}, F_{20} 0^{20} 13^{20}$
3	8	050	10	10	08.3	03.7	.	.	$F_{20} 7^{20}, H^{20} 24, F_2 20^{20} 20^{20}$
4	7	10	10	04	08.0	00.3	22.2	.	$\bullet 0-0^{20}, 1$
5	8	09	070	07	07.7	03.8	00.3	.	$\Delta 0-4^{20}, 1, 4^{20} 5^{20}, 8^{20} 9$
6	7	10	10	05	08.3	00.0	00.3	.	$\bullet 2^{20} 4^{20} 20-20^{20}, = 18-19^{20}$
7	8	10	060	10	08.7	04.1	01.1	.	$\bullet 2^{20} 9^{20} 20^{20} 21^{20}, F_2 12^{20} 16^{20}$
8	8	060	08	04	06.0	06.3	02.1	.	$\bullet 3^{20} 5^{20} F_2 11^{20}$
9	7	10	10	08	09.3	01.7	.	.	$\bullet 7^{20} 14^{20} 13^{20} 14^{20}$
10	8	08	08	00	05.3	06.9	01.6	.	$\Delta 20^{20} 24$
11	8	09	060	00	05.0	05.8	.	.	$\Delta 0-7^{20} 21-24; F_2 17^{20} 17^{20}$
12	8	000	030	00	01.0	12.8	.	.	$\Delta 0-8^{20}$
13	8	000	060	00	02.0	06.7	.	.	$\Delta 0-7^{20} 20^{20} 24$
14	8	030	060	00	03.0	09.7	.	.	$\Delta 0-7^{20} 21^{20} 24$
15	8	060	050	07	06.0	07.7	.	.	$\Delta 0-7^{20}, 16^{20} 16^{20}, F_2 20-21^{20}, F_{20} 20^{20}$
16	8	09	050	10	08.0	05.2	00.1	.	$\bullet 5^{20} 6^{20} 15^{20} 16^{20}, F_2 15-16^{20}$
17	8	000	040	10	04.7	09.9	00.3	.	$\bullet 0^{20} 0^{20} 13^{20} 21, F_2 13^{20} 20^{20}$
18	8	000	070	00	02.3	09.4	00.2	.	$\Delta 22^{20} 24$
19	8	09	09	07	08.3	04.5	.	.	$\Delta 0-7$
20	8	000	080	04	04.0	08.2	.	.	$\bullet 15-17^{20}, F_2 14^{20} 18$
21	8	07	090	08	08.0	05.1	02.0	.	$\bullet 0^{20} 0^{20}, \Delta 20^{20} 24$
22	8	10	060	01	05.7	07.6	04.4	.	$\Delta 0-2^{20} 21-24; \bullet 2^{20} 7^{20}$
23	8	040	050	00	03.0	11.5	01.0	.	$\Delta 0-7$
24	8	000	080	00	02.7	08.1	.	.	$\Delta 0-7^{20} 22^{20} 24$
25	8	000	09^{20}	10	06.3	08.1	.	.	$\Delta 0-7^{20}, F_2 13^{20} 19^{20}, \bullet 15-24, = 20^{20} 23^{20}$
26	7	070	09	02	06.0	04.8	14.5	.	$\bullet 0-4, \Delta 22-24$
27	8	000	010	00	00.3	13.4	.	.	$\Delta 0-7^{20} 22^{20} 24$
28	8	000	040	05	03.0	10.0	.	.	$\Delta 0-7^{20}$
29	8	02	10	09	07.0	07.7	.	.	$\Delta 0-9^{20} 22^{20} 24$
30	8	10	09^{20}	07	08.7	01.4	00.2	.	$\Delta 0-4, \bullet 4-5^{20} 12^{20} 14^{20} 22^{20} 24; F_2 12^{20} 15^{20}$
31	8	10	060	04	06.7	06.1	07.4	.	$\bullet 3-3^{20}, 19^{20} 20^{20}, = 6-9$
H. VR.		05.4	07.0	04.3	05.6	208.7	57.7		

1	7	10	070	01	06.0	01.9	01.5	.	$\bullet 1^{20} 2^{20} 7-11^{20}, 18^{20} 20^{20}$
2	7	10	10	00	06.7	06.9	10.2	.	$= 2^{20} 8^{20}, \Delta 20^{20} 24$
3	7	10	09	10	09.7	01.5	.	.	$\Delta 0-7^{20} 21^{20} 24; \bullet 7^{20} 9^{20}$
4	7	09	09	04	07.3	01.2	00.3	.	$\Delta 0-8^{20} 21-24; \bullet 19^{20} 19^{20}$
5	7	030	030	00	02.0	12.7	00.0	.	$\Delta 0-7^{20}, 20^{20} 24$
6	8	010	000	00	00.3	11.9	.	.	$\Delta 0-9^{20} 20^{20} 24$
7	8	030	030	00	02.0	12.7	.	.	$\Delta 0-7^{20} 20^{20} 24$
8	8	09	080	08	08.3	07.0	.	.	$\Delta 0-8^{20} 21-24$
9	8	080	020	10	06.7	06.9	04.9	.	$\Delta 0-2^{20} 22-24; F_{20} 1^{20}, \bullet 2^{20} 4^{20} 7^{20} 8^{20}$
10	8	050	090	02	05.3	11.7	00.7	.	$\Delta 0-8^{20}$
11	7	08	10	05	07.7	00.0	00.1	.	$\bullet 5^{20} H_1, \Delta 21-24$
12	8	000	060	03	03.0	11.7	02.5	.	$\Delta 0-8^{20} 21-24$
13	8	000	060	06	04.0	09.2	.	.	$\Delta 0-7^{20}$
14	8	020	040	10	05.3	10.3	.	.	
15	8	060	070	10	07.7	07.2	.	.	$\bullet 21^{20} 24, F_2 7^{20} 13^{20}$
16	8	10	060	03	06.3	04.8	00.0	.	
17	7	060	10^{20}	10	08.7	03.2	.	.	$\Delta 0-7^{20}, F_2 10^{20} 16^{20}, \bullet H^{20} 22^{20}$
18	8	020	080	03	04.3	11.2	17.2	.	$= 2-6^{20}, \Delta 20^{20} 24$
19	8	040	020	10	05.3	09.6	00.2	.	$\bullet 0^{20} 1^{20}, \Delta 20^{20} 24$
20	8	10	10	10	10.0	00.0	.	.	$\Delta 0-8^{20}, \bullet 10^{20} 24, = 20^{20} 24$
21	7	10	080	00	06.0	02.2	11.9	.	$\bullet 0-12^{20}, = 0-H^{20}, \Delta 22-24$
22	8	000	060	10	05.3	11.8	08.2	.	$\Delta 0-10^{20} 20^{20} 24$
23	8	10	09	00	06.3	02.9	02.0	.	$\Delta 0-5^{20}, \bullet 5^{20} 10^{20}$
24	8	09	060	02	05.7	06.2	08.6	.	$\bullet 2^{20} 4, 16^{20} 18, = 6-8, F_2 16^{20} 18$
25	8	040	060	00	03.3	10.8	04.1	.	$\Delta 4^{20} 7^{20}, F_2 14^{20} 14^{20}, \bullet 14^{20} 14^{20}$
26	8	030	010	00	02.0	11.1	01.1	.	$\Delta 0-8^{20} 20^{20} 24$
27	8	02	07	10	06.3	09.5	.	.	$\Delta 0-7^{20} 21-24$
28	6	10	10	10	10.0	00.0	00.6	.	$\bullet 0-2^{20} 12^{20} 14^{20}, = 6^{20} 24, \Delta 19^{20} 24$
29	8	030	030	00	02.0	13.7	01.5	.	$= 0-5^{20}, \Delta 0-18^{20}$
30	8	000	020	00	00.7	13.8	.	.	$\Delta 0-9^{20}, 20^{20} 24$
H. VR.		05.6	06.3	04.6	05.5	223.6	75.6		

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

Dan	Vazdušni pritisak P hPa			Temperatura vazduha T C°						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina veta D, f (0-12)							
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21				
1	945.1	941.9	941.3	13.2	28.8	20.8	20.9	28.8	11.8	08.4	11.6	09.8	09.9	76	25	40	47	SE	1	WSW	2	-	0	
2	942.5	940.0	945.6	16.0	24.0	14.2	17.1	25.4	14.0	12.5	15.1	09.7	15.9	83	33	98	71	-	0	NW	1	MNW	1	
3	948.0	948.0	950.3	12.0	19.8	13.8	14.9	20.4	11.2	10.2	12.8	10.1	08.5	91	44	54	63	NW	1	WSW	1	-	0	
4	950.3	947.9	947.7	09.8	22.0	14.8	15.4	23.0	08.3	07.6	10.7	09.7	10.7	88	37	64	63	-	0	SSW	1	E	2	
5	944.2	942.9	943.9	11.8	23.8	16.8	17.3	24.0	10.2	09.0	11.7	10.0	08.9	85	34	46	55	-	0	NW	2	ESE	3	
6	944.3	944.9	945.9	12.0	20.0	15.8	15.9	20.4	09.8	08.5	11.3	11.6	11.6	81	49	65	65	-	0	-	0	-	0	
7	947.0	946.8	948.4	12.6	22.9	15.6	16.7	23.2	10.4	08.6	11.8	07.8	10.2	81	28	58	56	-	0	W	2	SE	2	
8	948.3	945.5	944.8	11.3	25.1	15.8	17.0	25.1	09.5	08.0	11.3	10.2	13.2	85	32	74	64	-	0	WSW	2	-	0	
9	944.0	944.0	943.2	12.0	18.4	15.4	15.3	20.3	11.4	10.2	13.1	14.6	15.1	93	69	86	83	WSW	1	ESE	1	E	2	
10	942.0	942.3	943.3	13.2	17.2	15.7	15.5	18.2	11.3	09.6	14.1	17.4	16.6	93	89	93	92	-	0	-	0	-	0	
11	944.4	944.8	946.3	13.2	20.2	14.6	15.7	20.4	13.2	10.0	14.5	11.4	14.0	96	48	84	76	-	0	ESE	1	E	2	
12	948.3	947.9	947.9	11.2	22.6	16.6	16.8	23.0	09.9	08.7	12.4	10.6	11.3	93	39	60	64	-	0	ESE	2	E	3	
13	949.2	947.7	948.8	11.2	24.3	18.2	18.0	24.5	10.5	09.0	12.6	09.9	11.1	94	32	53	60	E	1	WSW	1	ENE	3	
14	950.0	946.9	948.0	13.8	26.6	19.4	19.8	26.8	11.5	10.0	12.2	09.1	12.9	84	26	57	56	-	0	ESE	2	E	2	
15	947.9	946.4	946.5	14.6	28.8	20.4	21.1	28.8	12.7	10.0	14.0	08.4	11.2	84	21	47	51	-	0	-	0	E	2	
16	948.0	947.0	946.6	15.6	29.5	20.8	21.7	29.5	13.9	12.5	13.7	11.4	11.7	77	28	48	51	-	0	SE	1	E	2	
17	947.0	946.8	947.4	16.7	27.0	20.7	21.3	29.5	15.6	14.4	15.6	17.8	14.4	82	50	59	64	E	1	N	2	SW	1	
18	945.6	942.8	943.0	16.0	29.6	23.4	23.1	29.6	14.7	13.5	16.4	13.4	12.1	90	32	66	63	-	0	W	2	ENE	1	
19	941.9	940.7	941.3	16.8	29.6	22.2	22.7	30.2	15.2	14.0	16.3	09.8	14.3	85	24	53	54	-	0	W	2	ESE	2	
20	943.9	941.1	941.9	17.4	31.4	23.6	24.0	31.5	16.0	14.9	14.7	12.8	14.0	74	28	48	50	ESE	2	WSW	1	E	1	
21	944.4	945.1	950.4	18.2	24.8	16.0	18.8	29.0	16.0	15.8	16.1	18.9	15.7	77	60	87	75	ESE	1	WSW	2	SSE	1	
22	954.5	952.0	951.2	13.8	25.0	16.4	17.9	25.0	12.6	11.0	12.3	07.5	09.7	78	24	52	51	-	0	E	1	ENE	2	
23	951.0	948.3	949.0	11.4	27.4	19.4	19.4	28.0	09.0	08.0	10.0	11.6	11.0	74	32	49	52	-	0	NW	1	E	3	
24	949.6	947.3	946.9	13.1	29.2	21.2	21.2	29.4	11.8	10.5	09.8	12.7	13.7	65	31	54	50	ESE	1	WSW	2	ENE	2	
25	947.4	944.4	944.8	15.0	29.2	21.2	21.7	29.5	13.9	13.0	14.5	14.4	15.5	85	36	61	61	E	1	WSW	2	-	0	
26	944.7	942.3	942.4	16.0	29.6	21.6	22.2	29.8	14.7	13.1	16.1	14.5	12.7	88	35	49	57	-	0	WSW	1	ESE	2	
27	942.6	941.3	942.4	16.6	33.4	24.0	24.5	34.0	14.2	13.5	13.9	09.1	12.8	73	18	43	45	-	0	NW	1	-	0	
28	943.3	941.6	942.0	17.4	33.6	24.0	24.8	33.6	15.3	14.2	13.2	10.5	13.5	66	20	45	44	ESE	2	NNW	1	-	0	
29	942.4	939.3	940.3	18.3	33.8	23.9	25.0	34.4	17.0	15.6	14.3	10.4	09.8	68	20	33	40	E	2	SW	2	ESE	1	
30	940.6	939.2	940.2	18.7	35.4	26.4	26.7	35.4	17.0	14.6	12.7	11.7	08.9	59	20	26	35	-	0	WSW	2	SSW	1	
31	938.4	936.8	937.7	19.9	35.0	22.6	25.0	35.0	18.4	16.4	12.3	09.6	11.1	53	17	40	37	SW	2	SSW	4	-	0	
M.																								
VR	945.8	944.3	945.1	14.5	26.7	19.2	19.9	27.3	12.9	11.5	13.3	11.5	12.5	81	35	58	58	0.5		1.5			1.3	

1	942.3	940.6	941.0	16.8	28.2	20.6	21.6	28.5	18.4	15.4	16.3	12.4	12.2	85	32	50	56	-	0	NNW	1	ENE	3
2	941.3	942.4	945.6	15.4	17.6	15.4	16.0	21.9	14.2	12.2	14.6	17.4	16.8	84	86	96	89	-	0	-	0	-	0
3	947.3	944.3	942.8	12.4	24.5	17.4	17.9	24.6	11.9	11.4	13.5	09.2	11.0	94	30	55	60	E	1	NW	1	E	1
4	939.7	937.3	942.4	13.7	27.4	19.2	19.9	28.5	11.6	10.5	12.0	09.3	13.6	77	25	61	54	ESE	2	NW	1	WSW	1
5	942.6	940.6	938.6	12.9	29.9	20.4	20.9	29.9	11.6	10.4	12.5	08.1	09.2	84	19	38	47	ENE	1	NNW	1	ESE	3
6	937.2	932.0	929.5	16.2	34.2	24.4	24.8	34.5	13.6	12.5	10.5	10.3	09.0	57	19	29	35	E	2	E	4	E	2
7	929.1	932.4	938.9	17.8	19.4	11.0	14.8	25.0	11.0	15.6	10.3	10.7	12.8	51	48	98	66	S	1	NW	1	WSW	1
8	940.6	941.6	940.8	10.6	19.0	13.4	14.1	20.6	09.5	08.5	11.0	06.5	07.8	86	30	50	55	-	0	-	0	-	0
9	940.8	940.0	941.0	11.8	23.4	17.8	17.7	23.8	10.5	08.6	11.3	09.8	10.4	83	34	51	56	-	0	WSW	2	ENE	2
10	942.3	942.3	945.2	13.7	28.2	19.4	19.4	28.4	10.5	09.5	11.1	09.0	13.3	86	23	59	56	ESE	1	WSW	2	-	0
11	947.9	946.5	947.4	13.6	30.0	21.1	21.5	30.2	12.6	11.5	12.7	09.6	14.3	82	23	57	54	ESE	1	WSW	1	ENE	1
12	948.4	946.3	946.6	15.8	32.4	22.4	23.2	33.0	13.9	12.6	13.7	09.7	10.1	77	20	37	45	-	0	ESE	2	ENE	2
13	948.0	945.7	946.9	14.8	34.1	22.4	23.4	34.1	13.9	12.4	11.4	09.4	07.8	67	18	29	38	E	1	E	1	ENE	2
14	948.4	946.0	947.2	15.6	35.1	25.0	25.2	35.1	15.2	13.6	13.4	06.4	14.4	75	11	45	44	ENE	1	NE	2	SE	2
15	947.7	945.2	946.3	17.8	33.8	24.0	24.9	34.0	16.4	15.0	15.6	09.2	10.6	77	18	35	43	-	0	SE	1	E	1
16	946.0	942.9	942.6	16.2	33.2	22.2	23.5	33.4	15.1	14.0	14.1	08.5	10.8	77	17	41	45	-	0	E	3	E	1
17	943.0	940.2	940.7	15.4	21.7	22.8	20.7	32.7	14.6	13.2	11.9	17.9	11.0	68	69	40	59	E	1	NNW	1	-	0
18	940.4	941.6	945.2	16.1	25.0	17.6	19.1	29.1	15.0	14.0	12.7	17.0	15.8	69	54	78	67	E	2	WSW	2	NW	1
19	945.2	945.2	942.4	14.4	28.9	20.2	20.9	29.5	13.8	13.7	14.7	08.3	09.5	90	21	40	50	-	0	W	1	ESE	1
20	943.6	943.0	945.6	14.6	27.8	21.2	21.2	29.8	12.8	11.9	11.8	10.8	10.2	71	29	40	47	-	0	W	2	E	3
21	949.2	948.2	948.3	14.6	28.0	19.0	20.2	29.0	13.8	12.4	11.8	10.3	09.5	71	27	43	47	E	1	NNW	1	ENE	1
22	950.4	945.5	945.3	12.0	33.4	23.2	23.0	33.4	11.6	10.5	11.0	08.2	11.2	79	16	39	45	E	1	WSW	1	E	2
23	946.0	943.7	946.3	15.4	34.0	24.0	24.4	34.0	14.5	12.5	11.0	07.8	11.8	63	15	39	39	-	0	WSW	2	E	1
24	946.0	942.4	942.9	16.4	34.6	23.0	24.3	34.6	13.2	12.6	12.5	08.4	11.0	67	15	39	40	E	3	NW	1	-	0
25	943.3	941.6	942.6	17.0	32.8	23.0	24.0	33.4	15.0	13.0	12.5	10.2	10.2	64	21	36	40	E	2	SW	1	-	0
26	941.6	937.9	937.5	17.2	31.6	22.7	23.6	34.5	15.0	13.0	10.8	08.8	11.5	55	19	42	39	E	2	S	2	W	1
27	937.1	941.0	941.1	15.8	11.4	11.6	12.6	22.7	11.2	13.3	17.1	12.9	13.4	95	96	98	96	NNW	1	NNW	1	-	0
28	940.0	942.5	943.2	10.8	11.8	12.1	11.7	12.4	10.6	10.3	12.7												

Dan	Oblačnost N (0-10)					Insolacija broj sati	Padavine R mm	Snežni pokrivak h cm	Razvoj vremena w
	Vrijeme 0-9	14	7	14	21				
1	8 02	06	10	06.0	11.1	.	.	$\Delta 0-8^{20}$ $R 15^{15}, 16^{45}, \nabla 15^{20}-15^{20}, \bullet 15^{20}-20^{20}, F 15^{25}, 15^{27}, = 20^{20}-24$	
2	8 01	09	10	06.7	07.5	.	.	$\Delta 21-24$	
3	8 08	05	00	04.3	11.0	<u>15.2</u>	.	$\Delta 0-10^{20}-21-24$	
4	7 04	06	02	04.0	11.8	.	.	$\Delta 0-8^{46}$	
5	8 03	05	09	05.7	12.7	.	.	$\Delta 0-7 21^{20}-24$	
6	8 01	10	07	06.0	04.3	.	.	$\Delta 0-7^{20}$	
7	8 05	03	00	02.7	09.4	.	.	$\Delta 0-9 20^{20}-24$	
8	7 07	06	00	04.3	11.0	.	.	$\Delta 0-6^{25}, \bullet 6^{25}, 9^{25}, = 8^{40}, 11^{20}$	
9	7 10	08	09	09.0	00.4	02.1	.	$\Delta 0-8^{20}, = 5-8^{20}, \bullet 8^{20}, 14^{20}, 22^{20}-24$	
10	6 09	10	10	09.7	01.6	04.7	.	$= 0-12, \bullet 0^{15}, 0^{20}, 5^{20}, 7^{20}, \Delta 21-24$	
11	7 10	09	00	06.3	02.7	06.7	.	$\Delta 0-10^{20}, 21-24, = 5^{20}, 9$	
12	7 00	08	01	03.0	08.1	00.0	.	$\Delta 0-8^{20}, 21-24, = 6-11$	
13	8 00	07	01	02.7	07.2	.	.	$\Delta 0-8, 23-24, = 6-11$	
14	8 00	08	02	03.3	10.4	.	.	$\Delta 0-8, 23-24$	
15	8 00	01	00	00.3	13.0	.	.	$\Delta 0-8^{20}$	
16	7 00	04	00	01.3	13.0	.	.	$\Delta 0-8^{20}, 21^{20}-24, \bullet 15^{25}, 15^{27}$	
17	7 00	10	05	05.0	06.9	.	.	$\bullet 2^{25}, 3, 13^{25}, 13^{26}, R 1-3, 13^{20}, 19^{45}$	
18	8 03	01	07	03.7	11.0	00.0	.	$\Delta 0-8$	
19	8 00	06	00	02.0	11.3	00.1	.	$\Delta 21-24$	
20	7 30	04	00	01.3	12.6	.	.	$\Delta 0-8^{25}, \bullet 15-19^{20}$	
21	8 01	09	10	06.7	07.2	.	.	$\Delta 0-7$	
22	8 00	00	00	00.0	13.2	00.0	.	$\Delta 0-7^{20}$	
23	8 00	01	00	00.3	13.3	.	.	$\Delta 0-7$	
24	8 00	05	00	01.7	13.2	.	.	$\Delta 0-7^{20}$	
25	8 00	04	00	01.3	13.1	.	.	$\Delta 0-7$	
26	8 00	03	00	01.0	12.8	.	.	$\Delta 0-7$	
27	8 30	01	00	00.3	12.8	.	.	$\Delta 0-7$	
28	8 00	01	00	00.3	13.0	.	.	.	
29	8 00	02	00	00.7	12.9	.	.	.	
30	8 00	00	00	00.0	13.0	.	.	$F 15^{20}$	
31	8 04	07	04	05.0	08.7	.	.	.	
M. VR.		02.2	05.1	02.8	03.4	310.2	29.1		

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1	8 04	04	00	02.7	11.9	.	.	$\bullet H^{20} 20^{20}$
2	8 05	10	10	08.3	02.6	.	.	$\Delta 0-8$
3	7 09	01	00	03.3	10.6	10.5	.	.
4	8 06	10	10	08.7	06.9	.	.	.
5	8 01	01	00	00.7	12.1	.	.	.
6	8 00	00	04	01.3	11.0	.	.	$\Delta 2^{20}-2^{25}, \bullet 2^{25}, 5^{45}, 7^{20}, 12^{20}, R 2^{25}, 2^{20}, 8-9^{20}, H^{20}, 12^{25}$
7	8 06	06	10	07.3	04.0	04.0	.	.
8	8 01	09	06	05.3	07.6	02.8	.	.
9	8 04	04	07	05.0	11.0	.	.	$\Delta 2-7^{20}$
10	8 00	02	00	00.7	10.9	.	.	$\Delta 2^{20}, 7^{20}$
11	8 02	02	00	01.3	09.7	.	.	$\Delta 1^{20}, 7$
12	8 00	01	00	00.3	11.8	.	.	$\Delta 4-7^{20}$
13	8 00	00	00	00.0	11.4	.	.	.
14	8 00	01	00	00.3	11.4	.	.	.
15	8 00	04	00	01.3	10.7	.	.	.
16	8 00	00	00	00.0	11.2	.	.	.
17	8 00	02	00	00.7	11.4	.	.	.
18	7 00	06	10	05.3	08.0	.	.	$= 23^{20}-24, \bullet 23^{20}-24$
19	8 10	05	00	05.0	08.0	00.0	.	$\bullet 0-7, = 8-7^{20}$
20	7 02	09	04	05.0	08.1	.	.	$\Delta 0^{20}, 7$
21	8 00	00	00	00.0	10.8	.	.	.
22	8 00	00	00	00.0	11.0	.	.	.
23	8 00	03	02	01.7	10.8	.	.	.
24	8 01	01	02	01.3	11.3	.	.	.
25	8 00	04	00	01.3	10.0	.	.	.
26	8 00	09	07	05.3	06.5	.	.	$\Delta 22^{20}-24, \bullet 22^{20}-24, R 22^{20}-24, \bullet 23^{20}-24$
27	6 10	10	10	10.0	00.0	13.5	.	$R 0-2^{20}, \bullet 0^{25}, 2^{20}, \bullet 6^{20}, 16^{20}, 20^{20}-24, = 10-20^{20}$
28	7 10	10	10	10.0	00.0	25.9	.	$\bullet 0-24, = 0-8^{20}, \bullet 6^{20}, 16^{20}, 20^{20}-24, = 10-20^{20}$
29	6 10	10	10	10.0	00.0	06.9	.	$\bullet 0-24, = 11-24$
30	6 10	10	10	10.0	00.3	12.1	.	$\bullet 4^{25}, 11^{20}, = 6^{20}, 18^{20}, \Delta 21^{20}-24$
31	7 09	10	00	06.3	00.6	00.0	.	$\Delta 0-7^{20}, 20^{20}-24, = 4^{20}, 11^{20}, 23^{20}-24$
M. VR.		03.2	04.6	03.6	03.8	251.6	75.7	

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = + 1h 14 min.$

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Dan	Vazdušni pritisak P hPa			Temperatura vazduha T °C						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina vjetro- D, f (0-12)						
	7	14	21	7	14	21	Sred. Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred. Dias	7	14	21			
1	945.7	943.7	943.7	11.8	26.4	17.2	18.2	26.6	11.2	10.4	13.2	09.1	14.3	96	26	73	65	-	0	WSW	1	E	1
2	945.3	944.7	947.4	13.0	27.0	19.3	19.7	27.2	12.3	11.5	13.7	13.9	15.2	92	39	68	66	E	1	WSW	1	ESE	1
3	946.0	945.2	944.0	13.4	28.1	20.8	20.9	28.4	13.0	12.4	14.7	10.4	13.9	96	27	57	60	E	2	E	2	-	0
4	941.1	948.2	949.0	16.2	11.9	10.0	12.0	21.4	10.0	13.8	13.9	12.7	11.8	76	91	96	88	-	0	-	0	SSW	1
5	950.6	947.9	946.6	08.2	19.9	12.2	13.1	23.5	07.5	06.7	10.3	08.8	10.0	95	38	71	68	-	0	-	0	ESE	2
6	943.9	941.1	943.3	08.4	26.0	16.8	17.0	26.4	07.8	06.6	10.5	10.3	14.2	95	31	74	67	-	0	W	1	E	3
7	949.1	946.4	946.8	10.3	19.8	10.4	12.7	19.8	10.2	09.2	10.5	06.9	09.5	84	30	75	63	-	0	ESE	3	E	3
8	945.7	941.9	940.7	06.0	23.4	14.3	14.5	23.5	05.3	04.0	08.5	05.8	09.9	91	20	61	57	ENE	2	SW	1	ESE	1
9	940.7	939.7	944.8	11.0	15.3	10.3	11.7	15.0	09.2	09.2	09.9	10.5	12.2	76	61	98	78	ESE	2	SSW	2	-	0
10	947.7	948.7	951.2	07.6	16.2	08.4	10.2	16.2	07.3	05.6	08.9	07.8	08.1	85	42	74	67	-	0	WSW	1	E	1
11	953.2	951.2	950.6	04.2	20.6	11.8	12.1	20.6	04.0	03.2	07.8	07.4	11.2	94	31	81	69	ENE	1	SW	1	ENE	1
12	950.0	947.7	948.2	06.9	21.2	13.4	13.7	21.5	06.0	04.3	09.0	08.9	10.9	91	35	71	66	E	1	-	0	-	0
13	948.0	946.1	946.3	07.0	19.4	10.0	11.6	19.4	06.5	05.5	09.5	06.4	07.9	95	28	64	62	E	1	SW	2	ESE	2
14	948.8	945.9	947.0	05.0	20.4	11.2	12.0	21.0	04.3	03.4	07.8	07.2	09.0	89	30	68	62	E	1	WSW	1	ENE	2
15	946.3	943.6	942.8	05.8	23.2	12.4	13.5	23.2	05.5	04.5	08.7	08.3	09.6	95	29	67	64	ENE	2	SSW	1	E	1
16	944.8	945.3	946.6	07.7	23.7	14.2	15.0	23.7	07.0	05.5	09.4	08.9	10.5	90	30	65	62	E	2	-	0	-	0
17	950.5	949.7	951.6	07.8	23.6	14.5	15.1	24.2	07.7	05.5	09.8	10.3	11.1	92	34	67	64	E	1	SW	2	-	0
18	953.9	953.7	954.3	13.2	26.0	16.4	17.3	26.0	09.6	08.3	11.0	11.9	13.5	88	35	72	65	ESE	1	WNW	1	E	2
19	953.7	950.6	950.1	10.6	27.6	16.4	17.8	27.6	10.2	08.2	12.0	10.0	13.2	94	27	71	64	ESE	1	NW	1	E	3
20	949.2	947.2	946.9	11.6	25.8	18.0	18.4	26.6	11.1	10.0	12.3	11.7	15.9	90	35	77	67	E	1	-	0	E	1
21	946.6	945.2	946.5	12.8	27.4	17.4	18.8	27.4	12.3	10.0	14.0	12.9	13.5	95	35	68	66	E	2	WSW	2	E	2
22	946.5	944.8	946.5	11.0	26.9	16.6	17.8	26.9	10.6	09.0	12.1	13.5	12.7	92	38	67	66	E	2	WNW	2	E	2
23	947.7	946.0	947.0	10.6	26.6	16.4	17.5	26.6	10.2	09.0	11.9	11.1	11.6	93	26	62	60	ESE	2	WSW	1	ESE	1
24	946.9	943.9	945.5	10.7	28.2	15.4	17.4	28.2	10.6	09.1	12.4	10.5	13.0	97	28	74	66	-	0	-	0	ESE	2
25	946.1	944.6	946.8	11.0	27.8	18.4	18.9	27.8	09.6	09.4	12.1	11.7	15.3	92	31	72	65	ESE	1	SW	1	ESE	1
26	948.4	950.1	952.3	13.5	19.7	14.1	15.4	21.0	13.4	12.6	15.1	10.6	11.2	98	46	70	71	NE	1	ENE	2	-	0
27	953.9	952.3	952.4	08.6	19.6	10.4	12.3	19.9	08.6	07.7	10.4	09.6	09.5	93	42	75	70	E	2	W	2	ENE	2
28	950.8	948.6	949.6	06.8	19.8	10.4	11.4	20.0	04.5	03.9	08.1	07.5	08.6	94	32	68	65	E	1	WSW	1	E	1
29	950.3	949.2	951.3	06.0	20.4	11.8	12.5	21.2	05.8	05.0	08.0	08.8	08.9	85	37	64	62	ESE	2	WSW	2	-	0
30	954.4	953.9	956.2	05.8	21.5	10.6	12.1	21.5	05.8	04.4	09.0	08.1	08.0	97	31	63	64	-	0	WNW	1	ESE	1
N.	948.1	946.9	947.9	09.2	22.8	14.0	15.0	23.3	08.6	07.6	10.8	09.6	11.5	91	36	71	66	1.1	1.2	1.2			

1985 OKTOBAR

SARAJEVO

1	956.2	954.6	954.8	05.8	21.4	12.8	13.2	22.3	05.5	04.0	08.3	10.4	10.0	90	41	67	66	E	2	WSW	1	E	2
2	954.8	952.8	953.1	07.4	24.8	14.2	15.2	24.8	06.8	05.1	09.2	08.1	09.2	90	26	57	58	ESE	1	SW	1	ENE	3
3	953.3	951.4	950.3	07.8	25.0	14.2	15.3	25.0	07.3	06.0	08.7	08.4	07.9	83	27	49	53	E	2	SW	2	ENE	3
4	950.4	946.6	946.6	07.1	25.0	14.0	15.0	25.0	05.8	05.1	08.2	11.5	07.9	81	36	50	56	ESE	2	WSW	1	E	3
5	946.0	943.3	945.1	07.8	25.2	12.8	14.7	25.5	06.6	05.0	08.5	10.1	09.1	80	32	62	58	ESE	3	-	0	-	0
6	946.8	945.9	949.2	07.4	26.2	14.9	15.9	26.2	07.2	05.5	08.0	07.4	10.7	77	22	63	54	ESE	2	WSW	1	ESE	2
7	950.1	948.2	948.3	08.6	25.2	14.8	15.9	25.2	07.9	06.0	09.0	10.5	12.3	81	33	73	62	ESE	2	W	1	ESE	2
8	945.2	939.6	940.8	08.2	23.5	12.2	14.0	23.5	08.2	06.5	10.3	11.0	07.7	95	38	54	62	ESE	2	WSW	1	ESE	1
9	942.1	941.6	943.9	09.3	21.7	13.2	14.3	21.7	08.5	06.6	10.6	10.8	12.7	93	42	83	73	ESE	1	-	0	E	3
10	946.8	948.8	951.7	07.6	15.2	13.8	12.6	16.3	07.6	06.6	09.9	10.8	12.6	95	62	80	79	-	0	-	0	E	1
11	956.7	955.0	955.6	09.5	17.5	08.0	10.8	17.5	08.0	06.0	10.5	06.4	07.7	88	32	72	64	-	0	WSW	2	ESE	1
12	954.8	951.4	951.7	03.6	19.7	12.8	12.2	19.7	03.2	02.0	07.6	08.3	13.1	96	36	88	73	ESE	1	WNW	1	-	0
13	954.5	952.3	954.4	08.4	13.2	05.7	08.3	13.5	05.7	07.0	09.4	04.6	05.9	85	30	64	60	SW	1	NNW	1	-	0
14	952.8	951.7	951.7	04.6	08.1	03.4	04.9	09.7	03.4	02.7	05.8	04.6	05.6	68	41	72	60	NNE	2	WNW	3	-	0
15	947.6	943.9	943.9	02.2	03.9	05.4	04.2	05.7	01.6	01.2	06.4	07.7	08.7	89	96	97	94	-	0	WNW	1	-	0
16	946.0	946.6	951.2	02.4	05.1	04.2	04.0	05.7	01.7	02.4	07.0	06.6	07.5	97	75	91	88	SW	2	ESE	1	NW	1
17	952.0	952.0	953.6	04.1	11.2	03.4	05.5	11.5	02.7	02.4	06.9	04.7	06.5	84	35	84	68	NW	1	N	1	ESE	1
18	951.4	948.3	946.9	03.7	14.0	05.6	07.2	14.4	03.4	01.4	07.4	06.4	08.5	93	40	93	75	-	0	-	0	ESE	1
19	945.3	944.6	945.6	03.6	11.5	08.7	08.2	11.8	01.4	00.2	07.7	06.6	06.9	97	48	61	69	E	1	M	1	WNW	2
20	947.7	948.8	952.8	06.4	07.2	06.4	06.6	08.7	06.4	06.0	09.4	09.4	07.3	97	92	82	90	-	0	-	0	ESE	2
21	952.8	953.0	953.1	06.2	11.2	08.1	08.4	11.2	06.2	05.2	08.6	08.1	10.0	91	61	93	82	-	0	ENE	2	-	0
22	951.2	950.3	949.9	06.9	10.0	09.6	09.0	10.3	06.6	05.9	09.6	11.6	11.4	96	94	95	95	-	0	-	0	-	0
23	948.8	950.5	951.9	07.4	05.4	06.5	05.5	10.2	04.4	04.1	10.2	08.4	07.9	99	93	94	95	-	0	-	0	WNW	1
24	952.4	953.9	956.3	05.5	07.8	06.2	06.4	08.1	04.5	04.3	06.7	07.5	06.5	74	71	68	71	-	0	ENE	3	ESE	1
25	956.3	954.6	955.6	01.8	14.4	03.3	05.7	14.4	01.6	00.0	05.6	04.7	06.9	81	29	89	66	ENE	2	ESE	1	E	2
26	955.9	954.5	953.9	-00.4	06.9	01.8	02.5	07.3	-00.4	-01.0	05.7	06.3	06.8	96	63	98	86	-	0	WSW	1	-	0
27	952.4	952.0	950.5	-01.2	07.7	02.8	02.8	08.1	-01.2	-02.2	05.5	06.2	06.8	98	59	94	84	-	0	SW	1	-	0
28	949.9	947.7	948.8	-05.4	08.2	04.8	04.4	08.7	-00.6	-01.4	05.8	06.8	07.0	98	63	82	81	-	0	-	0	SE	1
29	947.2	945.6	946.9	02.4	09.4	07.9	06.9	09.7	02.3	-01.1	07.0	08.3	10.3	97	70	96	88	-	0	-	0	-	0
30	946.9	945.2	944.6	05.8																			

$\varphi = 43^{\circ}52' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta t = + 1h 14 min.$

Dan	Vazdušni pritisak hPa			Temperatura vazduha T °C						Napon vodene pare e hPa			Relativna vlažnost u%				Pravac i jačina vjetro- D, f (0-12)					
	7	14	21	7	14	21	Sred Dias	Max	Min	Min 5 cm	7	14	21	7	14	21	Sred Dias	7	14	21		
1	939.7	937.7	936.6	13.3	16.9	10.6	12.0	18.1	10.0	08.9	12.1	11.9	11.6	99	62	91	84	-	0	-	0	ENE 1
2	928.6	928.4	932.3	14.6	10.9	06.6	09.7	14.8	06.6	08.1	09.2	11.7	09.2	55	90	95	80	ESE 1	NE 1	W 1	E 1	
3	934.7	934.3	937.6	05.2	15.0	07.6	08.9	15.0	04.4	03.5	08.4	08.2	09.4	94	48	93	77	-	0	E 2	E 2	
4	939.6	938.5	939.7	02.6	06.2	06.4	05.7	07.8	03.2	02.0	07.4	08.5	09.6	94	89	100	94	-	0	-	0	-
5	939.3	938.1	935.6	05.6	12.8	11.4	10.3	13.2	05.2	04.0	08.8	08.8	08.6	97	60	64	74	-	0	WSW 1	S 3	
6	924.0	925.5	933.6	15.0	08.2	05.3	08.5	15.4	05.3	04.0	10.6	08.6	07.7	63	79	89	77	S 3	NW 4	-	0	
7	936.8	936.4	939.4	-03.3	10.0	00.8	02.8	10.6	-00.4	-01.5	04.7	04.1	04.8	79	34	74	62	E 1	SE 3	E 3	E 3	
8	944.6	943.9	943.0	-02.7	10.8	06.0	05.0	11.0	-02.7	-03.5	04.4	05.1	05.5	88	39	58	62	-	0	-	0	ENE 3
9	945.6	944.6	945.0	01.7	15.4	07.0	07.8	15.5	01.7	09.5	05.2	05.8	06.5	75	33	65	58	ESE 1	WSW 1	ESE 2	ESE 2	
10	944.0	939.2	937.6	05.0	20.7	11.2	12.0	20.7	03.7	03.0	07.8	09.4	09.5	89	38	72	66	E 2	W 1	WSW 1	WSW 1	
11	935.4	934.1	937.7	14.4	20.4	05.7	11.6	20.6	05.7	03.4	09.9	10.4	07.6	60	44	82	62	S 1	SSW 2	NW 2	NW 2	
12	936.3	937.2	938.8	03.9	20.6	17.0	14.6	20.6	03.8	02.5	07.3	09.6	10.9	90	39	56	62	-	0	S 4	S 2	
13	937.3	938.5	938.6	17.4	18.4	17.0	17.5	19.0	15.9	15.2	08.8	10.8	10.9	44	51	56	50	S 4	SSE 5	S 3	S 3	
14	938.5	942.8	948.7	14.0	11.0	03.8	08.2	17.0	03.8	12.5	08.9	07.3	07.0	56	55	87	66	NW 2	W 3	WSW 1	WSW 1	
15	952.8	953.9	955.4	01.7	02.6	01.4	01.8	03.8	01.4	01.3	04.6	03.8	03.8	67	52	56	58	NW 1	NE 2	NE 2	NE 2	
16	954.1	950.0	951.6	00.2	07.9	00.4	02.2	07.9	-00.2	-00.5	03.9	04.5	05.8	63	42	91	65	E 3	ESE 2	E 2	E 2	
17	952.3	953.3	952.7	-00.6	00.1	-01.0	-00.6	03.4	-01.0	-00.6	05.5	05.9	05.6	95	97	98	97	NW 2	NW 1	-	0	
18	948.0	946.0	941.9	-01.6	-00.8	-01.0	-01.1	-00.8	-01.6	-01.6	05.3	05.7	05.6	98	98	99	98	-	0	-	0	ESE 2
19	940.7	941.1	941.6	03.2	03.6	00.8	01.4	04.0	-01.6	-01.6	06.1	06.3	06.4	98	79	98	92	-	0	-	0	-
20	937.6	933.5	933.3	00.4	06.8	04.8	04.2	05.8	-00.2	-00.3	06.2	08.1	07.9	98	82	92	91	-	0	E 5	E 5	
21	935.7	935.7	938.1	07.2	08.6	05.1	06.5	09.6	04.8	04.0	06.6	08.8	08.7	65	79	99	81	E 2	E 2	-	0	
22	941.7	941.5	942.6	02.1	10.9	02.6	04.6	11.0	02.1	00.5	05.9	06.2	06.3	83	47	86	72	ESE 2	-	0	ENE 2	
23	942.4	940.6	940.6	00.4	01.6	03.4	03.7	03.4	00.2	-00.6	06.2	06.5	06.7	98	95	98	97	-	0	NW 1	-	0
24	939.0	938.0	935.3	00.2	01.2	00.8	00.8	01.3	00.2	00.1	06.1	06.6	06.3	98	98	97	98	-	0	-	0	W 1
25	933.0	932.2	932.0	03.0	02.2	01.9	01.5	02.4	00.0	-00.2	05.9	06.4	06.6	97	89	94	93	W 1	-	0	-	0
26	930.4	928.7	923.3	01.0	00.4	-00.8	-00.1	01.9	-00.8	-00.5	06.2	06.2	05.6	95	98	97	97	-	0	-	0	SW 1
27	931.3	932.6	934.9	-01.6	00.8	00.2	-00.1	01.8	-01.6	-01.5	05.3	05.8	06.1	97	90	98	95	-	0	-	0	-
28	936.8	936.0	937.1	-00.5	02.0	00.6	00.7	02.3	-00.5	-01.0	05.8	06.6	06.2	98	94	97	95	-	0	-	0	-
29	942.8	946.8	947.6	00.0	03.0	-03.0	-00.8	03.1	-03.0	-00.4	06.0	05.9	04.0	98	77	82	86	SW 2	-	0	E 1	E 1
30	949.0	948.3	949.0	-01.6	06.6	03.5	03.0	07.0	-03.5	-04.4	04.5	05.8	07.0	82	59	90	77	E 2	-	0	-	0
M.	939.7	939.2	940.0	03.8	08.5	04.4	05.3	09.5	02.0	01.7	06.8	07.3	07.2	84	68	85	79	1.0	1.3	1.3	1.3	

1	951.2	952.2	954.3	03.4	12.4	02.9	05.4	13.0	02.6	-01.4	07.1	08.3	07.3	91	55	97	81	E 1	-	0	ENE 2	
2	954.9	956.0	954.3	-03.7	05.0	01.5	01.8	06.0	-00.7	-01.5	05.7	06.9	06.7	98	79	98	92	-	0	-	0	-
3	954.0	953.1	953.7	-00.8	03.3	00.7	01.0	03.6	-00.8	-01.0	05.7	07.6	06.3	98	98	98	98	-	0	-	0	-
4	953.7	952.4	953.6	-01.0	05.8	00.2	01.3	05.8	-01.0	-01.2	05.6	08.8	06.1	98	96	98	97	-	0	-	0	E 1
5	951.9	948.7	947.7	-00.6	12.6	04.8	05.4	13.2	-00.6	-01.8	05.5	06.5	05.3	95	45	62	67	E 1	-	0	ENE 1	
6	946.3	946.4	948.0	01.4	14.3	03.8	05.8	14.0	00.9	-00.9	05.6	06.4	06.8	82	40	85	69	ESE 1	SSW 1	E 2	E 2	
7	948.0	945.6	945.9	01.3	10.0	03.6	04.6	10.1	01.0	00.0	06.2	06.8	07.3	92	56	88	79	E 1	-	0	E 3	
8	945.9	946.1	946.0	03.2	10.7	02.8	04.1	17.6	00.2	-00.6	06.1	06.7	06.3	98	52	85	78	E 3	-	0	E 3	
9	946.4	944.4	945.5	-02.2	04.8	02.6	02.0	06.4	-02.2	-02.5	06.1	06.7	07.3	98	78	95	90	-	0	-	0	E 2
10	943.9	941.1	941.5	-02.8	05.1	02.8	02.5	05.4	-00.8	-01.6	05.7	07.3	07.0	98	83	94	92	E 1	-	0	-	0
11	941.9	943.4	945.0	02.4	04.4	03.0	03.2	04.8	02.0	00.5	07.0	07.9	07.5	97	94	98	96	-	0	-	0	NW 1
12	946.4	946.8	948.4	01.0	00.5	03.0	03.5	03.0	00.0	00.4	06.5	06.4	06.0	98	98	98	98	NW 1	NW 1	-	0	-
13	951.2	953.0	953.0	-00.6	00.6	00.1	00.1	01.3	-00.6	-00.9	05.7	06.3	05.9	98	93	97	96	-	0	-	0	-
14	949.3	950.8	953.1	00.1	01.0	00.6	03.6	01.2	00.0	-00.1	06.6	06.4	06.0	98	97	93	96	-	0	-	0	NW 1
15	951.9	951.6	950.8	00.2	02.4	01.2	01.3	03.7	00.2	-01.0	05.9	06.7	06.6	95	92	98	95	-	0	-	0	-
16	949.9	947.7	947.9	-00.2	00.5	00.2	00.2	01.2	-00.2	-00.6	05.9	06.2	06.1	98	98	98	98	ENE 1	-	0	-	0
17	943.7	941.0	941.9	-00.6	02.8	00.0	00.1	01.0	-00.6	-00.9	05.7	06.0	06.7	98	93	98	96	-	0	-	0	-
18	944.7	943.9	944.7	-00.8	01.2	03.2	03.2	01.3	-01.0	-01.0	05.6	06.6	06.2	96	98	100	98	-	0	SW 1	-	0
19	943.9	943.3	943.9	-00.6	00.3	01.2	00.5	01.2	-00.9	-01.5	05.6	05.9	06.4	96	95	97	96	-	0	-	0	-
20	944.0	944.8	946.0	00.5	02.8	-02.4	03.6	03.5	-00.4	-01.4	06.7	05.3	04.9	98	71	82	84	W 2	-	0	E 3	
21	948.3	949.7	951.6	-00.6	03.3	-01.0	00.1	03.0	-01.0	-01.0	05.7	06.4	05.4	98	85	95	93	-	0	-	0	-
22	951.6	950.1	950.1	-03.0	04.8	-00.3	03.3	04.8	-03.5	-03.0	04.7	05.3	05.7	96	62	95	84	E 1	SW 1	E 1	E 1	
23	946.8	944.6	945.0	-03.8	00.3	-01.8	-01.9	01.0	-04.0	-05.0	04.3	05.7	04.1	92	93	77	87	-	0	-	0	E 3
24	945.9	944.6	944.3	-00.4	00.7	-03.4	-03.1	01.0	-00.4	-03.6	03.3	04.3	04.4	87	67	93	82	E 3	-	0	E 1	E 1
25	944.2	942.0	941.6	-05.3	04.7	05.5	02.7	06.6	-05.8	-00.5	03.7	05.2	06.1	91	61	68	73	ENE 1	-	0	WSW 1	WSW 1
26	937.3	933.1	933.7	08.2	09.6	05.0	07.0	10.8	05.0	03.6	06.0	07.7	08.2	55	64	94	71	S 3	SSW 1	SSW 1	SSW 1	
27	933.7	936.4	930.9	01.6	03.4	01.5	02.0	05.0	01.5	00.2	06.4	07.6	06.6	94	97	97	96	E 2	-	0	-	0
28	940.8	939.2	938.3	01.2	08.9	00.8	07.7	13.7	-00.3	-01.6	06.1	04.9	06.1	98	43	57	64	E 1	S 3	S 3	S 3	
29	933.1	932.4	933.1	08.4	13.0	14.3	12.8	14.3	00.6	00.6	09.2	09.8	06.7	81	56	42	60	WSW 2	S 2	S 2	S 4	
30	933.5	937.0	936.8	10.6	-00.4	-01.8	01.7	13.4	-01.6	-00.3	13.2	05.7	05.3	80	96	98	91	-	0	SSW 2	SSW 1	
31	933.3	929.0	927.6	-01.8	00.4	03.4	-00.7	01.0	-01.6	-02.7	05.3	04.9	06.1	98	78	95	90	-	0	SW 1	-	

Dan	Vrijevnost 0-p		Oblačnost N (0-10)			Inzolacija broj sati	Padavina R mm	Snežni pokrivak h cm	Razvoj vremena w
	14	7	14	21	Sred Dias				
1	8	10	04	04	06.0	04.0	28.3	.	• 0-4, 18 ²⁰ , 19 ²⁰ , 5 ²⁵ , 8 ²⁰ , 8 ²⁰ , 10 ²⁰
2	7	08	09	10	09.0	00.3	00.8	.	• 8 ²⁰ , 17 ²⁰
3	8	07	05	09	07.0	04.0	12.3	.	• 15 ²⁵ , 17 ²⁰
4	4	10	10	10	10.0	00.0	01.6	.	• 3-24, 18-24
5	8	00	08	10	06.0	04.1	00.0	.	• 0-9 ²⁰ , 17 ²⁰ , 21 ²⁰ , 19 ²⁰ , 22 ²⁰
6	7	08	10	07	08.3	00.0	00.3	.	• 10 ²⁵ , 15 ²⁰ , 17 ²⁰ , 19 ²⁰
7	8	00	03	00	01.0	08.9	08.7	.	• 4-8, 8 ²⁰ , 10 ²⁰ , 20-24
8	8	00	07	08	05.0	07.2	.	.	• 0-9 ²⁰ , 11 ²⁰ , 13 ²⁰ , 9 ²⁰ , 11 ²⁰
9	8	01	04	00	01.7	07.3	.	.	• 4 ²⁰ , 7 ²⁰ , 24-24
10	8	06	08	00	04.7	07.1	.	.	• 0-8
11	8	06	07	10	07.7	06.2	.	.	• F 2 ²⁰ , 6 ²⁰
12	8	03	04	05	04.0	06.2	.	.	• 4-7, 7 ²⁰ , F 14-14 ²⁵
13	8	06	09	08	07.7	01.4	.	.	• 14 ¹⁵ , 15 ²⁰ , 20 ²⁵ , 22 ²⁰
14	8	05	06	08	06.3	04.8	00.2	.	• 0 ²⁵ , 1 ²⁰ , 14 ²⁵ , 15 ²⁰ , 18 ²⁰ , 22 ²⁵ , F 3 ²⁵ , 3 ²⁰
15	7	10	10	10	10.0	00.0	00.3	.	.
16	8	09	00	10*	06.3	07.2	.	.	• * 19 ²⁰ , 24
17	6	10*	10*	10*	10.0	00.0	06.2	04	• * 0-24, 8 ²⁰ , 24
18	5	10*	10*	10*	10.0	00.0	15.8	19	• * 0-16 ²⁰ , 18 ²⁰ , 23 ²⁰ , 0-24, 16 ²⁰ , 18 ²⁰ , 23 ²⁰ , 24, 15 ²⁰ , 22 ²⁵ , 22 ²⁰
19	5	10	02	10	07.3	03.8	26.1	20	• 0-1 ²⁰ , 0-24, 1 ²⁰ , 3 ²⁵
20	7	06	08	10	08.0	00.8	04.5	10	• 0-2 ²⁰ , 2 ²⁰ , 10 ²⁰ , 3-24i
21	7	06	10	06	07.3	00.0	06.4	02	• 0-1 ²⁰ , 7 ²⁰ , 20 ²⁵ , 17 ²⁰ , 20 ²⁰
22	8	01	04	00	01.7	06.4	05.9	.	• 20 ²⁰ , 24
23	5	06	10*	10*	08.7	00.0	.	.	• 0-7 ²⁰ , 1 ²⁰ , 24, 10 ²⁰ , 13 ²⁵ , 13 ²⁵ , 14 ²⁵ , 17 ²⁰ , 24, * 14 ²⁵ , 17 ²⁰
24	3	10	10	10	10.0	00.0	05.6	.	• * 0-1 ²⁰ , 0-4 ²⁰ , 4 ²⁰ , 24, 13 ²⁵ , 24
25	3	10*	10	10	10.0	00.0	00.8	.	• 0-14 ²⁰ , 0-3 ²⁰ , * 3 ²⁰ , 9 ²⁰ , 14 ²⁰ , 24
26	3	10	10*	10	10.0	00.0	00.3	.	• 0-3, 8-24, 8-8, * 7 ²⁰ , 20 ²⁰
27	5	10	10	10	10.0	00.0	19.4	20	• 0-8, 8 ²⁰ , 8 ²⁰ , 24
28	5	10*	10	10	10.0	00.0	00.2	07	• 0-13 ²⁰ , * 0-6 ²⁰ , 13 ²⁰ , 24
29	6	10	07	00	05.7	02.3	00.0	05	• 0-11 ²⁰ , 5 ²⁰ , 7 ²⁰ , * 7 ²⁰ , 11 ²⁰ , 11 ²⁰ , 17
30	6	07*	09	09	08.3	02.4	00.3	04	• * 6 ²⁰ , 7 ²⁰ , 10 ²⁰ , 15 ²⁰
M.									
VR.	06.8	07.5	07.5	07.3	84.4	144.0			

1	6	09	00	00	03.0	05.8	.	.	• 7 ²⁰ , 19 ²⁰
2	4	00	00	00	00.0	01.7	.	.	• 5 ²⁰ , 7 ²⁰ , 12 ²⁰ , 17 ²⁰ , 24
3	0	00	00	10	03.3	00.7	.	.	• 0-24, 1-8 ²⁰
4	2	10	00	10	06.7	02.7	.	.	• 0-24, 4 ²⁰ , 17 ²⁰
5	4	00	00	00	00.0	07.7	.	.	• 0-8, 20 ²⁰ , 24, 0-2 ²⁰ , 2 ²⁰ , 4 ²⁰ , 7-19 ²⁰
6	8	02	00	00	00.7	05.9	.	.	• 0-9 ²⁰ , 18 ²⁰ , 24
7	5	07	00	00	02.3	06.0	.	.	• 0-6, 20 ²⁰ , 24, 6-8, 8-20
8	5	00	00	00	00.0	07.2	.	.	• 0-9 ²⁰ , 20 ²⁰ , 24, 9 ²⁰ , 17 ²⁰
9	3	10	04	02	05.3	03.6	.	.	• 0-9, 5-6 ²⁰ , 6 ²⁰ , 19 ²⁰
10	3	09	08	05	07.3	00.0	.	.	• 0-9 ²⁰ , 7 ²⁰ , 15 ²⁰ , 17 ²⁰ , 24, 15 ²⁰ , 17 ²⁰
11	3	09	10	10	09.7	00.0	.	.	• 0-15 ²⁰ , 8 ²⁰ , 10 ²⁰ , 18-24, 15 ²⁰ , 24
12	4	10*	10	10*	10.0	00.0	05.2	.	• 0-6 ²⁰ , 13-14 ²⁵ , 0-24, 6 ²⁰ , 7 ²⁰ , * 7 ²⁰ , 24i, 19
13	5	10*	10	10	10.0	00.0	20.0	15	• 0-24, 10-23, 19
14	3	10	10	10	10.0	00.0	00.4	06	• 0-2 ²⁰ , 5-7, 2 ²⁰ , 7 ²⁰ , 11 ²⁰ , 13 ²⁰ , 13 ²⁰ , 23 ²⁰ , 19
15	6	09	10	10	09.7	01.0	00.0	04	• 0-19 ²⁰ , 19 ²⁰ , 24, 19
16	1	10	10	10	10.0	00.0	.	02	• 0-24, 19
17	2	10	10	10	10.0	00.0	.	.	• 0-24
18	2	10	10	10	10.0	00.0	.	.	• 0-24
19	3	09	10	07	08.7	00.0	.	.	• 0-13 ²⁰ , 23 ²⁰ , 24, 13 ²⁰ , 23 ²⁰ , 13 ²⁰ , 20 ²⁰
20	7	10*	09*	00	06.3	01.5	00.9	.	• 0-7 ²⁰ , 6 ²⁰ , 7 ²⁰ , 16 ²⁰ , 6 ²⁰ , 7 ²⁰ , 7 ²⁰ , 11, 12 ²⁵ , 13, 13 ²⁵ , 14, 19-24
21	5	10*	09	00	06.3	00.2	03.7	03	• 0-2 ²⁰ , 20 ²⁰ , 24, * 2 ²⁰ , 7 ²⁰ , 6-19, 19
22	3	01	00	00	00.3	04.5	00.0	.	• 0-10 ²⁰ , 4 ²⁰ , 7, 14 ²⁰ , 23 ²⁰ , 24, 7 ²⁰ , 14 ²⁰ , 23 ²⁰ , 24
23	5	00	00	00	00.0	01.8	.	.	• 0-6, 15 ²⁰ , 18, 6-15 ²⁰ , 18-24, 10-12, 0-12, 20 ²⁰ , 24
24	4	00	00	02	00.7	06.9	.	.	• 0-24, 0-17 ²⁰ , 20-24
25	5	01	03	09	04.3	06.8	.	.	• 0-11 ²⁰ , 0-24
26	8	06	10	09	08.3	00.0	.	.	• F 0 ²⁰ , 17 ²⁰ , 8 ²⁰ , 9 ²⁰ , 15 ²⁰ , 19 ²⁰
27	6	09	09	00	06.0	00.1	08.1	.	• 0-8 ²⁰ , 23 ²⁰ , 24, 7 ²⁰ , 19 ²⁰ , 9 ²⁰ , 17
28	8	05	10	10	08.3	00.0	07.5	.	• 0-8 ²⁰ , 11-19 ²⁰ , 24 ²⁰ , 24
29	8	09	09	09	09.0	00.0	03.4	.	• 0-4 ²⁰ , 11, 14 ²⁰ , 24
30	6	10	10	10	10.0	00.0	01.2	.	• F 2 ²⁰ , 0 ²⁰ , 3 ²⁰ , 5 ²⁰ , 11 ²⁰ , 11 ²⁰ , 11 ²⁰ , 11 ²⁰ , 11 ²⁰ , 24, * 11 ²⁰ , 20 ²⁰ , 13 ²⁰ , 16 ²⁰ , 17 ²⁰ , 19
31	6	10	10	10	10.0	00.0	23.4	16	• 0-24, 14 ²⁰ , 24, 19
M.									
VR.	06.6	05.8	09.6	06.0	64.1	71.0			

Mesec	Vrednosti izračunane po NF A	Temperatura vazduha °C							Cestina pravaca i srednja jačina vetra mD, Pm (0-12)																									
		7		14		21		Sred. (Danas)	Max	Min	Max	Dak.	Min	Dak.	N		NE		E		SE		S		SW		W		NW		C			
		Ø	J	Ø	J	Ø	J								Ø	J	Ø	J	Ø	J	Ø	J	Ø	J	Ø	J	Ø	J	Ø	J		Ø	J	Ø
		DUBROVNIK																			BR. ST. 96													
		$\varphi = 45^{\circ}55' N \quad \lambda = 16^{\circ}05' E \quad \Delta t = + 1h 12 \text{ min.}$																																
I	04.6	08.8	06.9	07.3	09.9	04.6	15.9	29	-03.6	12	26	02.7	19	33.0	12	32.5	16	04.2	02	04.5	04	02.8	02	02.9	12	02.1								
II	05.2	08.8	06.3	06.6	10.4	03.4	14.6	10	-34.0	19	34	03.2	14	34.0	04	02.6	12	03.3	04	03.0	05	02.3	02	02.5	08	02.1								
III	10.2	12.7	10.5	11.1	13.7	08.7	16.5	25	05.0	19	10	02.2	23	32.6	17	02.7	32	03.2	05	03.4	11	02.6	03	02.0	12	01.8								
IV	13.0	14.8	13.8	14.5	17.5	11.6	22.4	03	38.4	13	16	03.0	11	34.0	07	02.3	29	01.8	24	01.9	08	02.2	24	02.7	11	01.9								
V	18.8	29.7	18.0	18.8	21.7	16.0	28.5	26	11.1	13	06	02.3	02	32.6	11	01.9	32	03.0	13	02.2	09	01.7	11	01.9	09	01.8								
VI	21.4	23.9	20.4	21.5	26.8	18.4	27.1	33	18.5	18	14	01.9	04	32.7	08	02.5	30	03.0	11	02.4	03	02.4	25	03.1	13	01.8								
VII	24.8	27.2	23.8	24.9	28.6	21.8	33.2	22	17.0	11	15	03.0	10	33.5	04	01.7	17	01.9	18	01.6	13	01.9	08	02.3	09	01.7								
VIII	25.4	27.4	23.9	25.1	28.9	21.6	33.5	16	16.7	28	17	02.3	11	02.3	01	02.6	14	02.7	12	01.9	11	02.3	10	02.9	18	01.7								
IX	21.2	25.2	21.1	22.2	26.1	18.9	28.9	30	13.9	10	23	02.6	11	33.7	02	01.0	06	02.2	11	01.8	12	01.8	12	01.9	13	01.8								
X	16.2	20.0	16.5	17.3	21.0	14.5	26.2	08	10.4	15	29	02.6	15	03.6	03	02.3	16	02.7	10	02.6	09	02.0	04	02.2	07	01.7								
XI	12.7	15.4	13.1	13.6	16.8	10.9	19.0	01	07.4	30	23	02.2	10	02.9	06	02.6	23	04.6	11	04.4	03	02.6	03	02.2	11	01.8								
XII	10.7	14.2	11.5	12.0	15.0	09.1	16.8	07	06.3	24	30	01.9	12	01.9	02	02.1	18	03.9	05	03.8	08	01.3	24	01.6	14	01.9								
GDO.	15.6	18.4	15.5	16.2	19.5	13.3	33.9	20.0	-04.3	62.1	243	02.6	123	33.2	77	02.4	245	03.3	106	32.7	98	02.7	66	02.3	135	01.8								
		BR BOSNA I HERCEGOVINA																			BOSANSKI NOVI		BR. ST. 37											
		$\varphi = 45^{\circ}03' N \quad \lambda = 16^{\circ}23' E \quad \Delta t = + 1h 08 \text{ min.}$																																
I	-05.4	01.0	-04.2	-03.7	-00.5	-08.0	18.0	23	-23.2	12	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
II	-06.9	02.8	-02.8	-02.4	03.5	-08.6	15.0	01	-21.0	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	02.9	09.1	05.2	05.6	10.5	01.2	19.5	31	-03.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	06.4	16.4	10.0	10.7	17.3	04.4	27.0	09	-01.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	12.9	22.0	15.1	16.3	23.1	09.4	29.0	14	30.5	03	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	12.8	22.2	15.7	16.6	23.0	11.3	31.0	07	05.5	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	15.7	27.3	18.5	20.0	26.0	13.1	35.0	30	09.5	06	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	14.7	26.1	18.8	19.6	27.1	12.6	34.0	25	08.0	08	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	10.9	23.5	14.3	15.8	24.2	09.4	31.5	24	05.3	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	06.3	15.4	08.9	09.9	16.1	04.8	28.0	03	-02.0	17	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	02.8	08.4	03.2	03.9	07.1	02.3	22.0	10	-04.4	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	01.6	08.4	03.5	04.3	09.8	-00.3	19.0	29	-04.0	23	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GDO.	06.2	14.9	08.8	09.7	15.7	04.1	35.0	30.0	-23.0	62.1	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		BOSANSKA DUBICA																			BR. ST. 90													
		$\varphi = 45^{\circ}13' N \quad \lambda = 16^{\circ}38' E \quad \Delta t = + 1h 08 \text{ min.}$																																
I	-07.7	-02.7	-04.0	-05.6	-01.6	-11.0	14.6	23	-28.5	12	28	01.7	01	04.0	04	01.4																		
II	-07.8	01.7	-04.9	-04.0	02.7	-10.8	14.4	01	-23.0	13	26	01.6	03	02.3	11	01.6	01	02.0																
III	02.2	08.8	04.1	04.8	09.8	03.5	20.5	31	-02.0	05	10	02.2	03	01.7	16	01.6																		
IV	07.4	16.2	10.4	11.1	17.6	03.8	26.0	09	-02.5	25	30	02.2	03	02.9	08	01.8																		
V	14.1	22.5	15.6	17.0	23.8	09.2	29.6	14	01.4	04	21	01.5	02	01.1	14	01.4																		
VI	14.9	22.3	16.1	17.4	23.6	10.3	32.5	07	04.5	18	31	01.6	01	01.1	16	01.6																		
VII	17.9	27.6	18.8	20.8	28.4	12.4	36.6	29	08.2	04	17	01.7																						
VIII	16.5	26.8	18.8	20.3	28.0	12.4	34.6	25	07.0	19	28	01.6	02	01.1	09	01.3																		
IX	11.5	24.5	14.7	16.4	25.1	08.4	30.5	20	02.0	15	27	01.1	04	01.4	06	01.1																		
X	06.0	15.8	08.1	09.5	16.5	03.7	29.4	03	-02.0	17	31	01.5	03	01.1	06	01.1																		
XI	02.0	06.1	02.7	03.4	06.8	00.0	23.6	10	-03.5	15	17	01.4	02	01.1	05	01.9																		
XII	01.5	08.7	03.3	04.2	09.7	-00.4	19.0	29	-04.5	16	12	01.4	01	02.0	02	01.1																		
GDO.	06.5	14.9	08.5	09.6	15.9	03.2	36.6	20.0	-28.5	62.1	275	01.6	26	01.7	108	01.3	01	02.0	07	01.7	17	01.9	40	01.4	41	01.5	580							
		DERVENTA																			BR. ST. 99													
		$\varphi = 45^{\circ}00' N \quad \lambda = 17^{\circ}55' E \quad \Delta t = + 1h 12 \text{ min.}$																																
I	-08.5	-02.5	-06.6	-06.0	-02.2	-10.5	16.5	23	-23.5	12			18	01.1	08	01.1	02	01.1																
II	-07.5	01.1	-04.3	-03.7	01.7	-09.2	13.5	06	-21.0	14			22	01.8	07	01.7																		
III	02.5	09.1	04.9	05.4	09.8	01.2	21.2	31	-01.5	05	31	01.1	21	01.5	11	01.3	03	02.2																
IV	08.5	17.1	10.8	11.8	17.7	05.0	26.6																											

Mese	Oblačnost Hm (0-10)				Smetanje broj sati	Vlažnost vazduha				Padavine mm			Broj dana sa:																																					
	7	14	21	Sred.		Hm	7	14	21	Sred.	Min	Σ	Max	Dat.	F(0-12)												Σ																							
															I	II	III	IV	V	VI	VII	VIII	IX	X	XI	XII	I	II	III	IV																				
DUBROVNIK																			$H_n = 52 = H_b - 53.3 = h_c - 2.0 = h_f - 1.9 =$																															
BR. ST. 96	I	7.5	7.4	6.5	7.2	075.4	36.7	62	61	64	62	24	146	027.2	28	.	.	05	.	.	.	08	01	03	14	18	16	06	17	04	01	.	.	.	02	.	04	.	01											
II	5.9	5.3	4.1	5.1	135.9	09.9	53	50	56	53	18	055	015.4	12	.	.	06	05	01	02	18	22	17	08	22	02	02	08	.	.												
III	7.7	7.4	6.8	7.3	115.1	09.2	68	67	73	69	30	180	028.4	12	05	01	02	18	22	17	08	22	02	02	08	.	.											
IV	6.5	5.2	4.2	5.3	203.0	10.6	60	63	67	63	33	318	099.7	13	07	02	05	08	09	04	.	09	02	.	.												
V	5.5	4.6	5.0	5.2	254.4	16.0	70	71	77	73	35	035	013.1	30	.	.	.	04	.	.	03	02	.	05	05	09	04	01	09	01	05	.	.												
VI	2.8	3.2	3.8	3.3	327.5	16.6	58	62	69	63	32	056	017.2	18	.	.	16	.	.	08	02	.	10	01	08	05	01	08	01	04	.	.													
VII	1.4	1.7	1.5	1.5	377.9	17.4	47	57	59	54	25	019	018.5	11	.	.	.	31	08	26	05	.	23	.	02	01	01	02	02	01	.	.												
VIII	2.1	2.3	1.3	1.9	326.8	17.2	45	55	58	53	23	308	004.0	07	.	.	.	29	10	24	04	01	21	01	06	03	.	06	02	.	.														
IX	1.1	1.2	0.8	1.0	317.9	14.8	50	55	58	54	18	004	003.3	10	.	.	.	22	.	09	06	01	25	.	02	01	.	02	01	01	.	.													
X	3.5	3.7	3.0	3.4	208.0	11.4	52	54	61	56	08	048	036.3	31	.	.	03	.	.	09	01	15	06	06	04	01	06	02	.	.														
XI	6.9	6.5	6.4	6.5	111.0	11.0	71	64	69	68	24	322	117.0	19	10	05	02	10	19	16	07	19	07	.	.														
XII	5.4	4.7	4.9	5.0	138.8	09.5	67	63	69	66	25	135	062.7	31	04	01	09	10	09	08	04	09	02	.	04	.	.													
GDD.	4.7	4.4	4.0	4.4	2591.7	12.2	58	60	65	61	08	786	117.0	92.0	.	.	11	105	18	70	75	20	128	84	118	85	30	117	06	03	.	.	04	05	42	02	02													
ROSANSKI NOVI																			SR BOSNA I HERCEGOVINA																$H_n = 119 = H_b - - = h_c - 2.0 = h_f - 1.0 =$															
BR. ST. 97	I	9.8	7.5	7.7	8.4	-	04.8	91	84	91	89	48	050	016.0	25	13	23	27	19	12	04	32	02	11	01	30	23												
II	9.4	5.7	5.8	6.9	-	05.0	91	81	90	87	54	030	015.0	11	12	07	25	11	07	05	01	04	04	26	18												
III	9.2	6.9	7.5	7.9	-	07.8	92	74	88	85	40	109	014.0	12	.	.	05	15	19	17	03	19	07	04	26	02												
IV	7.8	5.4	6.3	6.5	-	10.0	84	63	82	77	29	127	027.4	27	.	.	02	31	10	14	10	04	19	02	21	.												
V	7.2	5.5	5.1	5.9	-	14.5	86	61	82	76	41	068	016.8	04	.	.	.	14	06	12	09	02	12	01	28	.												
VI	8.8	5.3	5.8	6.6	-	15.2	87	64	86	79	46	099	035.0	28	.	.	.	11	02	07	20	13	02	20	27	.													
VII	8.6	2.5	3.2	4.0	-	18.4	85	60	84	76	40	334	017.0	18	.	.	.	25	10	02	03	04	01	05	29	.													
VIII	9.5	3.9	3.5	5.6	-	18.4	88	65	85	79	36	086	028.5	27	.	.	.	24	13	07	07	07	04	07	31	.												
IX	9.6	2.2	2.7	4.8	-	14.9	87	65	86	79	48	019	008.5	05	.	.	.	14	01	03	04	03	.	04	29	.													
X	7.7	4.9	5.8	6.8	-	10.7	88	73	87	83	47	027	010.5	23	.	.	02	06	14	10	06	01	10	24	08													
XI	9.6	8.2	8.3	8.7	-	07.4	91	83	89	88	62	168	039.5	12	.	.	12	21	19	16	05	17	05	01	.	.	.	24	08													
XII	8.8	7.1	6.7	7.5	-	07.4	93	76	88	86	53	055	015.5	12	.	.	18	14	09	07	02	09	02	01	.	.	.	24	.													
GDD.	9.0	5.4	5.7	6.7	-	11.2	88	70	86	82	29	872	034.5	92.0	25	27	91	95	23	02	130	143	103	27	124	32	07	.	.	.	323	51												
BOSANSKA DUBICA																			$H_n = 88 = H_b - - = h_c - 2.0 = h_f - 1.0 =$																															
BR. ST. 98	I	8.9	8.1	8.4	8.5	-	-	-	-	-	-	048	013.5	25	15	20	29	03	25	09	08	02	08													
II	7.1	6.2	6.1	6.5	-	-	-	-	-	-	-	030	010.8	16	14	08	27	05	15	06	05	01	02	04	12	01											
III	8.8	8.0	6.4	7.7	-	08.0	95	82	85	90	50	075	010.0	16	.	.	17	01	17	18	17	02	18	06	06	.	.	.	12	01												
IV	6.8	6.5	6.0	6.4	-	11.4	92	70	90	84	42	108	041.0	27	.	.	03	02	05	14	09	07	04	09	01	.	.	.	01	01													
V	4.2	4.8	4.0	4.3	-	16.0	85	64	92	80	41	056	011.0	08	.	.	19	09	06	12	10	01	12	01	.													
VI	8.3	5.8	6.0	6.1	-	15.8	88	65	93	82	36	126	033.0	28	.	.	12	02	05	12	16	15	05	16	03	.													
VII	2.5	2.9	2.1	2.5	-	19.3	86	57	89	77	27	020	006.2	03	.	.	25	12	20	03	05	05	.	05	02	.													
VIII	3.4	3.8	2.3	3.2	-	19.5	87	61	93	80	40	066	018.0	27	.	.	25	13	16	06	06	06	03	06	01	.													
IX	3.8	2.5	1.8	2.7	-	16.3	93	65	94	84	50	022	008.0	04	.	.	14	02	18	03	04	04	.	04	04	.													
X	7.1	5.4	5.2	5.9	-	11.1	94	74	93	87	33	318	008.2	23	.	.	07	06	06	11	08	04	.	08	.	.	.	10	.														
XI	8.5	8.6	8.4	8.5	-	07.5	94	88	95	93	40	146	035.0	12	.	.	17	02	22	15	15	05	13	03	.	.	.	03	.													
XII	7.2	6.4	4.7	6.1	-	07.5	94	88	95	93	40	055	023.0	14	.	.	18	05	12	10	09	03	07	03	.	.	.	07	.													
GDD.	6.3	5.7	5.1	5.7	-	-	-	-	-	-	-	770	041.0	92.0	29	28	118	103	29	95	146	118	107	24	102	25	06	.	.	01	43													
DERVENTA																			$H_n = 105 = H_b - - = h_c - 2.0 = h_f - 1.0 =$																															
BR. ST. 99	I	7.1	6.8	8.2	7.4	-	03.9	89	79	90	66	57	060	019.0	25	16	21	27	04	20	11	09	02	02	10	01	.	.	.	01	02	31												
II	6.0	7.3	6.6	6.6	-	04.4	87	77	89	84	54	243	012.8	14	13	13	25	06	12	08	08	02	05	05	01	.	.	.	03	18													
III	7.9	7.3	7.2	7.5	-	07.6	94	71	92	86	24	074	020.1	20	.	.	06	01	03	17	18	16	01	18	07	05	.	.	01	07	05												
IV	5.8	5.9	5.7	5.8	-	10.1	86	55	82	74	27	105	024.4	27	.	.	01	02	06	11	13	11	04	13	01	01	.	.	01	01													
V	4.1	5.2	3.8	4.4	-	15.1	84	54	88	75	34	060	011.8	22	.	.	17	09	04	10	10	01	10	04	05													
VI	5.7	5.9	5.6	5.7	-	15.8	87	60	90	79	31	126	030.2	18	.	.	10	02	07	09	17	15	04	17	01	.													
VII	3.4	3.5	2.3	2.7	-	18.8	82	50	87	73	32	029	012.8	18	.	.	22	13	18	01	06	06	01	06	04	.													
VIII	3.4	3.9	3.6	3.6	-	18.0	87	53	83	74	31	290	030.7	28	.	.	24	15	.	.	.																													

Mesec	Vasodubni prilivak m hPa	Temperatura vazduha °C										Cestina pravaca i srednja jacina vetra nD, Pm (0-12)																	
		7m					Max	Min	Max	Det.	Min	Det.	N		NE		E		SE		S		SW		W		NW		C
		7	14	21	Sred. (dies)	z. j.							z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	z. j.	
		LIŠTICA												BR. ST. 176															
		φ = 43°27' N λ = 17°26' E Gr. ΔG = + 1h 10 min.																											
I	-	-01.9	01.9	-00.4	00.3	04.6	-04.9	14.0	31	-18.2	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
II	-	-01.4	06.8	01.4	02.0	07.4	-04.6	15.6	03	-13.4	13	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
III	-	04.9	11.5	06.8	07.5	12.2	02.6	19.0	27	-02.6	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IV	-	09.0	17.0	11.2	12.1	17.7	05.0	22.4	10	-02.0	30	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
V	-	13.6	22.7	15.2	16.7	23.5	09.6	28.9	21	03.6	01	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VI	-	15.3	24.0	16.8	18.3	25.4	10.5	29.6	07	06.2	18	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VII	-	18.4	30.5	21.0	22.8	31.1	13.1	36.7	27	09.4	25	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
VIII	-	17.7	30.3	20.1	22.1	31.6	13.1	37.4	13	08.9	08	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
IX	-	13.6	28.1	17.2	19.0	28.6	09.5	34.2	23	04.0	11	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
X	-	09.6	20.6	12.1	13.6	21.2	05.4	31.6	07	-01.0	26	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XI	-	06.9	12.6	07.1	08.4	13.2	03.6	19.4	12	-03.4	16	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
XII	-	03.6	11.3	04.9	06.2	11.8	00.7	15.8	15	-05.0	24	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
GDD	-	09.1	18.3	11.1	12.4	19.0	05.3	37.4	1500	-18.2	151	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
		PROZOR												BR. ST. 177															
		φ = 43°30' N λ = 17°27' E Gr. ΔG = + 1h 10 min.																											
I	-	-07.0	-00.5	-05.2	-04.5	01.7	-04.5	12.8	23	-22.8	12	-	-	-	-	23	02.0	01	02.0	-	-	03	01.7	-	-	-	-	-	
II	-	-06.2	02.0	-03.2	-02.4	04.2	-04.3	14.4	01	-18.6	13	-	-	-	-	19	02.2	-	-	-	-	04	01.4	-	-	-	-	-	
III	-	00.9	07.9	03.2	03.8	10.0	-01.1	18.6	27	-06.6	29	-	-	-	-	05	01.8	-	-	-	-	17	01.6	01	02.0	70	-	-	
IV	-	05.7	13.3	07.3	08.4	15.7	02.5	22.8	10	-03.6	19	-	-	-	-	13	01.9	-	-	-	-	10	01.8	05	02.5	60	-	-	
V	-	11.5	19.3	12.4	13.9	21.4	07.5	26.8	13	02.2	04	01	01.1	01	02.0	-	-	-	-	-	-	17	01.8	05	02.0	67	-	-	
VI	-	14.3	19.1	14.7	15.7	21.2	10.4	27.8	07	06.4	17	-	-	-	-	03	01.7	-	-	-	-	21	01.7	03	02.8	43	-	-	
VII	-	15.9	24.7	17.4	18.9	26.2	12.4	32.8	29	09.8	03	-	-	-	-	-	-	-	-	-	-	20	01.8	02	02.0	71	-	-	
VIII	-	14.5	25.2	15.6	17.7	27.2	10.6	33.8	14	06.4	28	01	02.0	-	-	07	02.0	-	-	-	-	20	02.4	03	02.0	62	-	-	
IX	-	10.2	24.0	13.1	15.2	26.0	06.7	30.2	25	02.6	28	-	-	-	-	01	01.1	-	-	-	-	16	01.9	01	02.0	72	-	-	
X	-	04.9	15.9	06.2	08.3	17.6	02.4	28.8	06	-02.0	28	-	-	-	-	10	02.3	-	-	-	-	10	01.9	06	02.0	67	-	-	
XI	-	01.8	07.1	02.9	03.7	08.8	-00.5	18.6	13	-05.2	16	-	-	-	-	08	02.4	-	-	-	-	03	01.7	05	02.0	74	-	-	
XII	-	-00.3	05.6	00.9	01.8	07.6	-02.9	16.6	29	-09.6	22	04	01.9	-	-	03	02.4	-	-	-	-	03	02.0	03	02.0	80	-	-	
GDD	-	05.9	13.6	07.1	08.4	15.6	02.5	33.8	1500	-22.8	151	06	01.8	01	02.0	-	96	02.1	01	02.0	-	144	01.8	34	02.2	813	-	-	
		ČAPLJINA-KLEPCI												BR. ST. 129															
		φ = 43°05' N λ = 17°43' E Gr. ΔG = + 1h 11 min.																											
I	-	-01.0	05.8	00.9	01.7	06.4	-02.0	18.1	24	-14.2	12	48	01.4	08	01.1	01	01.1	05	02.4	02	02.0	06	01.1	-	-	12	01.6	11	
II	-	00.4	08.1	03.2	03.8	09.0	-00.9	16.2	03	-06.5	21	45	02.1	02	01.1	-	-	03	01.8	05	02.4	09	01.1	-	-	13	01.1	07	
III	-	06.0	13.0	08.6	09.3	14.6	05.0	18.2	07	01.4	30	49	01.1	01	02.0	-	-	07	02.6	07	02.1	16	01.5	-	-	04	01.1	09	
IV	-	09.8	19.2	13.0	13.7	19.8	07.4	26.0	10	12.2	27	38	01.6	07	01.4	-	-	06	01.9	09	02.7	18	01.9	-	-	08	01.1	04	
V	-	15.1	24.1	17.2	18.4	24.7	12.5	30.2	25	06.4	01	24	01.1	01	01.1	-	-	09	01.9	29	02.3	18	01.3	-	-	08	01.1	04	
VI	-	17.5	26.4	18.4	20.2	26.9	13.8	30.7	15	10.5	22	33	01.4	02	01.1	-	-	03	01.4	26	02.3	19	01.7	-	-	06	01.5	01	
VII	-	20.0	31.8	22.2	24.1	32.2	15.2	36.2	30	11.5	04	14	01.5	11	01.4	-	-	21	01.7	14	02.2	21	01.1	-	-	11	01.1	01	
VIII	-	19.2	31.4	21.2	23.3	32.1	14.9	37.3	16	11.5	09	31	01.4	02	01.6	-	-	11	02.3	22	01.9	10	01.2	-	-	09	01.1	08	
IX	-	13.4	29.2	16.9	19.1	29.6	11.0	34.5	23	07.0	11	42	01.4	02	01.1	-	-	02	02.2	19	01.9	09	01.6	-	-	05	01.1	11	
X	-	09.1	21.9	12.3	13.9	22.5	07.7	31.4	07	01.2	26	33	01.3	17	02.4	-	-	02	03.1	11	01.8	08	01.2	-	-	06	01.1	16	
XI	-	08.0	14.5	08.9	10.1	15.2	06.1	22.3	01	-00.2	08	46	01.2	09	01.7	-	-	08	02.6	07	02.3	08	01.1	-	-	07	01.1	25	
XII	-	04.4	12.5	06.4	07.9	13.1	03.1	18.2	29	-02.7	24	44	01.1	17	01.2	-	-	10	01.8	-	-	08	01.4	-	-	07	01.1	07	
GDD	-	10.2	19.9	12.4	13.8	20.5	07.8	37.3	1500	-14.2	151	647	01.4	79	01.6	01	01.1	87	02.1	151	02.2	150	01.4	-	-	96	01.1	84	
		JABLJANICA												BR. ST. 129															
		φ = 43°40' N λ = 17°46' E Gr. ΔG = + 1h 11 min.																											
I	-	-04.3	00.1	-03.3	-02.7	01.1	-06.0	14.9	24	-19.2	13	02	01.1	02	01.1	03	01.1	-	-	01	03.0	01	03.0	02	01.4	05	01.3	77	
II	-	-03.4	04.2	-00.9	-00.3	05.1	-04.9	13.7	03	-14.8	13	01	01.1	07	01.7	05	01.5	01	01.1	-	-	04	01.1	01	01.1	03	01.1	62	
III	-	02.5	10.2	04.7	05.5	10.9	01.3	19.0	31	-02.8	30	-	-	-	-	02	01.1	03	01.4	01	01.1	02	01.6	03	01.7	01	01.1	80	
IV	-	08.4	16.9	11.2	12.0	18.0	06.5	25.0	10	00.4	30	01	01.1	05	01.7	06	01.3	-	-	05	01.7	10	02.2	05	02.3	05	01.7	53	
V	-	14.0	23.2	15.7	17.2	24.6	11.5	29.7	21	05.6	01	-	-	-	-	03	01.1	04	01.1	02	01.1	03	01.4	08	01.6	05	01.5	65	
VI	-	15.8	24.5	17.4	18.8	26.1	13.2	32.2	07	09.9	12	03	01.1	06	01.9	05	01.3	02	01.1	01	02.0	08	01.7	03	01.7	03	01.4	59	
VII	-	17.4	29.7	19.8	21.7	31.0	14.3	37.2	28	10.7	23	-	-	-	-	12	01.1	06	01.4	-	-	02	02.0	02	02.0	03	01.4	68	
VIII	-	17.0	29.2	19.4	21.2	30.4	14.2	36.8	24	10.7	09	-	-	-	-	03	01.7	08	01.1	01	01.1	03	02.3	03	02.2	03	01.4	01	
IX	-	11.3	25.2	14.3	16.3	25.9	10.2	31.0	21	06.2	11	01	01.1	03	01.4	06	01.9	-	-	-	-	-	-	-	01	02.0	02	01.1	77
X	-	07.6	17.5	10.2	11.4	18.2	06.6	27.8	03	01.2	27	-	-	-	-	04	02.4	05	01.9	-	-	02	01.1	-	-	05	01.3	77	
XI	-	06.3	10.3	06.8	07.5	11.2	04.5	20.4	13	-01.1	30	01	02.0	-	-	03	02.5	-	-	02	01.1	07	02.1	04	02.1	03	01.4	70	
XII	-	02.7	06.4	03.6	04.1	07.3	01.6	16.2	30	-03.0	25	04	01.6	-	-	02	01.6	-	-	-	-	01	01.1	01	01.1	02	01.6	83	
GDD	-	07.9	16.4	09.9	11.1	17.5	06.1	37.2	1500	-19.2	151	13	01.4	47	01.6	54	01.5	07	01.1	17	01.8	49	01.8	28	01.8	36	01.4	844	
		DDMANJICI												BR. ST. 130															
		φ = 43°																											

Mesec	Vandalni pristanak Pn aPa	Temperatura vazduha °C										Cestina pravaca i srednja jacina vetra m/s, Pn (0-12)																	
		Pn				Sred. (Danas)	Min	Max	Dat.	Min	Dat.	N		NE		E		SE		S		SW		W		NW		C	
		7	14	21	7							14	7	14	7	14	7	14	7	14	7	14	7	14	7	14	7		14
MCSTAR BR. ST. 131																													
φ = 43°21' N λ = 17°48' E Gr. ΔG = - 1h 12 min.																													
I	998.9	00.7	03.9	01.6	01.9	04.7	-00.5	15.2	24	-08.8	13	39	03.0	23	02.9	03	03.4	02	02.6	02	02.0	06	01.9	02	03.7	09	03.0	07	
II	111005.1	01.0	06.3	03.5	03.6	07.6	-00.2	15.8	03	-08.6	13	23	03.4	18	02.9	05	02.3	01	01.1	09	01.9	05	02.3	04	02.0	09	03.1	10	
III	111002.3	05.9	12.4	08.4	08.8	13.3	05.0	20.8	27	01.6	18	21	02.0	15	02.0	03	03.4	01	02.0	08	01.9	08	01.7	06	01.8	04	01.8	27	
IV	11000.1	10.1	18.4	13.3	13.8	19.3	08.4	26.0	10	03.2	30	28	03.4	18	03.8	05	03.5	06	02.4	16	02.1	22	01.9	05	02.9	03	01.4	07	
V	999.4	15.7	26.5	18.2	19.2	25.3	13.6	30.4	29	06.6	01	11	01.9	14	02.1	07	02.2	07	01.7	22	01.9	14	02.4	03	02.4	01	02.0	16	
VI	1001.6	17.5	25.1	20.0	23.7	27.0	14.9	32.2	07	11.3	25	11	02.8	23	02.4	11	02.3	08	01.8	15	02.2	10	02.2	03	02.4	01	02.0	08	
VII	1003.5	21.4	31.8	24.7	25.6	32.6	19.2	37.8	28	15.8	01	19	02.9	27	02.8	10	02.5	06	02.2	12	01.6	09	01.9	05	02.7	03	02.4	02	
VIII	11001.3	21.1	32.2	24.5	25.6	33.4	18.9	39.9	13	12.2	09	19	03.4	18	02.7	09	02.4	07	01.4	18	01.9	13	02.5	04	02.6	02	01.6	03	
IX	1006.3	17.5	29.3	21.1	22.3	29.9	16.3	35.8	22	12.4	16	23	03.3	26	03.2	09	02.8	04	02.2	08	01.9	13	01.9	02	02.8	.	.	05	
X	1009.3	12.5	21.4	15.2	16.1	21.9	11.4	32.5	07	04.4	26	21	03.0	31	03.3	13	03.1	13	01.8	03	01.9	02	02.0	02	03.4	03	01.1	05	
XI	1001.0	08.3	12.5	09.2	09.8	13.4	06.8	21.2	13	01.6	30	24	02.8	18	03.1	11	03.5	04	01.2	07	01.8	10	02.3	04	02.2	05	02.0	07	
XII	11007.7	05.2	10.5	07.0	07.5	11.5	04.1	14.9	29	-00.6	24	29	02.0	30	02.3	03	03.4	01	02.0	03	02.1	07	02.0	.	.	05	01.7	15	
GOD.	1003.1	11.4	19.0	13.9	14.6	20.0	09.8	35.4	27VI	-08.8	23	178	02.9	261	02.8	89	02.9	60	01.8	123	01.9	119	02.2	40	02.5	45	02.4	110	
IVAN SEDLO BR. ST. 132																													
φ = 43°46' N λ = 18°03' E Gr. ΔG = - 1h 12 min.																													
I	-	-08.8	-06.3	-07.7	-07.6	-05.4	-10.2	07.0	23	-26.2	12	13	05.4	02	01.4	39	01.7	23	01.8	07	04.0	.	.	08	03.4	06	04.1	.	
II	-	-07.1	-03.4	-04.6	-04.9	-02.0	-08.0	06.7	09	-16.5	14	08	04.9	02	01.4	33	02.4	23	02.5	06	02.8	.	.	06	03.9	08	03.5	.	
III	-	-00.2	04.4	01.7	01.9	05.1	-01.2	12.0	27	-07.0	30	25	04.0	06	01.7	21	01.9	15	02.1	03	04.4	01	03.1	09	02.6	27	02.7	06	
IV	-	04.0	09.2	05.9	06.2	10.8	02.5	19.7	10	-03.9	25	22	04.2	05	02.2	33	02.5	23	02.6	06	03.4	.	.	09	.	.	.	01	
V	-	10.4	18.0	12.0	12.6	17.8	08.9	23.6	15	-01.0	04	25	04.1	.	.	21	01.9	18	02.1	08	03.5	01	02.6	08	02.4	07	02.2	05	
VI	-	10.9	15.8	11.5	12.5	16.9	08.8	23.6	07	04.0	12	21	04.1	01	01.6	32	01.9	19	01.9	11	03.1	.	.	02	02.2	03	01.8	01	
VII	-	15.1	21.0	15.4	16.7	22.3	13.0	31.5	27	08.0	03	.	.	02	02.3	44	01.5	20	01.4	11	02.6	02	02.1	10	02.3	03	02.2	01	
VIII	-	12.8	19.9	14.6	15.5	21.8	11.7	29.2	23	04.0	08	16	03.9	.	.	26	01.9	19	01.9	15	03.4	.	.	05	02.4	06	02.5	09	
IX	-	09.7	16.2	11.8	12.4	17.9	04.7	23.0	01	04.6	28	03	02.5	03	02.2	32	02.3	19	02.3	15	02.9	.	.	03	02.4	01	01.1	14	
X	-	05.7	10.7	07.5	07.9	11.9	04.4	22.1	05	-01.0	15	14	01.8	16	01.8	10	02.8	01	02.0	.	.	07	02.8	04	
XI	-	02.2	04.5	02.6	02.9	05.7	00.4	16.4	12	-04.8	18	33	05.0	02	01.6	20	02.2	14	01.9	08	03.2	.	.	13	03.4	07	03.9	02	
XII	-	00.2	02.9	00.9	01.2	04.2	-01.3	10.0	29	-08.6	31	12	04.6	01	01.6	37	02.1	23	02.0	13	03.4	07	03.9	.
GOD.	-	04.6	09.2	08.0	06.4	10.6	05.1	31.5	27VI	-26.2	22	178	04.4	24	01.8	352	02.0	232	02.1	125	03.0	05	02.4	81	02.8	59	03.0	39	
BERKOVICI BR. ST. 133																													
φ = 43°06' N λ = 18°11' E Gr. ΔG = - 1h 13 min.																													
I	-	-02.2	02.3	-00.2	-03.1	03.3	-03.6	12.0	26	-19.2	13	26	03.2	12	02.4	03	01.7	.	.	23	01.2	04	01.8	25	
II	-	-02.2	03.2	00.0	00.3	04.2	-03.8	11.6	03	-11.2	13	35	03.7	14	01.9	01	01.1	.	.	19	01.1	01	01.1	18	
III	-	03.5	09.7	05.7	06.2	10.4	01.8	18.4	31	-01.2	29	03	04.2	29	02.0	05	01.5	.	.	21	01.1	02	02.0	32	
IV	-	07.9	15.2	09.9	10.7	16.1	04.5	23.4	10	-01.0	30	19	04.5	21	01.9	04	01.4	.	.	08	01.9	18	02.0	20	
V	-	14.2	21.0	15.5	16.6	22.5	09.9	27.8	20	00.2	04	.	.	09	01.8	02	01.6	.	.	27	01.3	16	01.9	39	
VI	-	15.5	23.3	18.4	17.9	24.4	10.1	29.2	07	00.8	12	19	02.8	04	01.6	24	01.3	09	02.1	38	
VII	-	19.4	29.1	19.7	22.0	30.2	13.5	35.2	29	10.0	06	33	02.4	03	01.1	02	01.1	.	.	12	01.3	08	01.9	35	
VIII	-	19.8	29.0	20.3	22.4	30.3	13.5	36.8	13	09.0	09	17	02.2	09	01.9	05	01.3	.	.	16	01.1	16	02.1	30	
IX	-	16.2	26.0	17.4	19.3	27.1	10.6	32.0	22	07.0	09	42	02.7	02	01.8	01	01.1	.	.	15	01.1	08	01.8	22	
X	-	08.2	18.6	11.4	12.4	19.8	04.3	24.0	04	-01.6	28	38	02.8	05	01.3	06	01.6	.	.	06	01.3	09	01.6	29	
XI	-	05.6	11.2	07.1	07.8	12.2	03.3	20.0	11	-01.2	28	15	03.2	15	02.2	13	02.0	.	.	22	01.4	25	
XII	-	03.8	10.7	05.7	06.5	11.5	01.5	15.2	05	-04.8	24	17	02.3	05	02.2	23	01.8	.	.	20	01.2	02	02.0	26	
GOD.	-	09.1	16.6	10.7	11.8	17.7	05.6	36.8	27VI	-19.2	23	163	03.0	128	01.9	85	01.7	.	.	209	01.3	93	01.9	339	
BJELASHICA BR. ST. 134																													
φ = 43°48' N λ = 18°18' E Gr. ΔG = - 1h 13 min.																													
I	779.8	-08.8	-07.6	-08.4	-08.4	-06.5	-10.6	01.0	23	-20.7	12	11	04.7	14	04.7	07	02.6	07	03.9	19	08.8	31	06.8	03	02.0	01	01.1	.	
II	784.6	-10.6	-09.3	-09.8	-09.9	-07.0	-12.6	00.3	02	-24.4	19	21	07.3	33	07.6	05	08.0	11	07.7	09	03.6	05	03.3	.	
III	788.0	-04.0	-02.7	-03.2	-03.3	-02.0	-04.7	00.8	31	-11.7	29	03	04.3	08	04.8	02	02.0	04	05.0	41	05.9	28	05.7	04	04.5	01	01.1	02	
IV	786.5	-01.8	-00.2	-00.9	-01.0	00.6	-02.6	06.4	10	-09.2	29	07	07.3	18	08.5	07	03.6	01	04.0	12	06.3	37	07.6	04	05.7	03	06.0	01	
V	789.6	05.0	07.4	05.5	05.9	08.0	03.9	13.2	20	-04.4	01	07	03.9	21	03.3	06	01.8	06	04.9	25	06.0	20	04.8	03	03.7	02	03.6	03	
VI	792.9	05.3	08.0	05.9	06.3	08.8	03.5	16.3	07	-03.1	18	25	06.0	11	04.1	02	02.6	.	.	11	05.9	28	05.6	06	03.0	05	03.2	02	
VII	797.7	09.5	12.5	10.2	10.6	13.1	08.0	20.2	27	01.4	22	30	05.3	20	04.2	02	01.6	.	.	09	06.2	18	05.6	03	02.8	05	03.5	06	
VIII	796.1	10.1	13.0	10.8	11.2	14.1	08.4	14.6	23	00.0	08	23	08.7	19	06.2	10	02.4	.	.	15	05.9	16	04.9	01	03.0	03	04.4	07	
IX	788.3	04.2	08.6	06.7	07.1	09.6	04.5	14.5	19	-02.6	10	09	05.0	44	04.6	10	03.1	03	02.7	05	04.1	12	04.4	01	02.0	02	01.4	04	
X	797.0	01.4	03.2	02.1	02.2	04.2	00.4	13.0	05	-07.0	18	25	06.0	11	04.1	02	02.6	.	.	11	05.9	28	05.6	06	03.0	05	03.2	02	
XI	786.1	-01.9	-01.1	-01.5	-01.5	00.5	-03.5	08.6	10	-10.8	18	07	05.9	14	05.1	04	04.3												

Mesec	Vazdušni pritisk hPa	Temperatura vazduha °C						Cestina pravaca i srednja jacina vetra nD, Pm (0-12)											
		Tm						N	NE	E	SE	S	SW	W	NW	C			
		7	14	21	Sred. (Dias)	Max	Min												

$\varphi = 43^{\circ}32' N$ $\lambda = 18^{\circ}26' E$ Gr. $\Delta G = +$ 1h 14 min. BR. ST. 136

I	937.3	-06.2	-01.7	-04.8	-04.4	-00.9	-07.4	13.8	24	-19.9	13	.	.	02	11.6	08	01.8	04	01.9	07	03.2	07	01.9	10	01.6	08	01.3	47
II	943.8	-06.0	01.1	-02.5	-02.5	02.7	-07.0	13.6	09	-18.4	14	04	03.2	01	01.1	10	01.6	09	01.7	02	32.6	02	02.3	12	01.6	08	01.7	36
III	940.2	02.0	09.2	04.5	05.1	10.2	01.3	18.6	27	-04.2	30	34	01.4	.	.	15	01.9	15	01.9	04	02.4	04	01.9	10	01.9	10	01.6	34
IV	938.9	05.7	14.1	09.0	09.4	15.3	04.4	24.4	10	-01.6	30	03	01.8	02	01.6	11	02.2	09	01.9	13	02.8	07	02.7	07	02.0	03	02.6	35
V	939.2	12.4	21.6	15.3	16.2	22.8	10.3	28.6	14	04.4	04	.	.	01	32.0	23	01.8	10	02.2	06	02.9	05	01.7	11	01.9	04	01.6	37
VI	941.9	12.6	21.7	15.4	16.3	22.5	10.5	31.4	07	05.3	12	01	01.1	04	01.4	14	01.7	03	01.8	03	32.4	10	01.8	17	01.8	06	01.6	32
VII	945.1	14.5	26.7	19.2	19.9	27.3	12.9	35.4	30	08.3	04	01	01.1	02	32.1	22	01.8	09	01.7	02	02.0	10	01.7	10	01.8	06	01.3	31
VIII	943.0	14.5	26.5	19.3	19.9	28.1	13.1	35.1	14	09.3	08	01	01.1	05	01.8	26	01.8	07	01.7	03	31.4	05	01.4	11	01.4	09	01.1	26
IX	947.6	09.3	22.8	14.0	15.0	23.3	08.6	28.4	03	04.0	11	.	.	03	31.6	36	01.7	08	01.7	01	01.6	10	01.4	08	01.4	03	01.9	25
X	949.6	05.5	14.5	08.8	09.4	15.1	04.8	26.2	06	-01.2	27	02	01.7	03	02.6	22	01.9	11	01.6	.	.	08	01.4	07	01.2	05	01.4	35
XI	939.5	03.8	08.5	04.4	05.3	09.5	02.0	20.7	10	-03.5	30	01	01.1	04	31.8	17	02.5	05	02.0	08	03.3	05	01.5	07	01.4	06	02.2	37
XII	945.3	00.3	06.8	01.9	02.3	05.9	-00.4	14.4	30	-06.4	24	.	.	02	31.4	20	01.9	01	01.1	07	32.6	06	01.2	04	01.6	03	01.1	36
GOD.	942.8	05.7	14.2	08.7	09.3	15.2	04.4	35.4	30.04	-19.9	12.1	17	01.9	29	01.8	224	01.9	91	01.8	56	02.7	79	01.7	114	01.7	71	01.6	404

$\varphi = 43^{\circ}31' N$ $\lambda = 18^{\circ}27' E$ Gr. $\Delta G = +$ 1h 14 min. BR. ST. 137

I	891.3	-06.0	-02.6	-05.2	-04.7	-01.5	-08.1	10.2	23	-26.8	13	.	.	06	02.3	38	02.3	05	01.1	03	21.1	06	03.7	14	02.1	03	01.1	38
II	898.1	-05.8	-01.2	-04.7	-04.1	00.2	-09.1	09.4	09	-18.4	23	01	03.0	11	02.6	28	02.2	06	01.1	.	.	11	03.6	12	02.1	03	01.4	17
III	897.1	02.6	07.0	03.6	03.9	07.7	00.3	13.5	27	-04.1	31	.	.	07	01.7	14	31.4	05	01.1	03	01.1	21	01.8	13	01.2	01	01.1	29
IV	895.9	06.2	11.4	07.1	08.0	12.6	03.5	21.4	10	-03.1	30	04	02.3	06	02.4	11	02.1	06	01.5	01	01.1	27	03.4	19	01.9	04	01.4	18
V	897.9	12.7	17.7	12.4	13.8	18.7	08.4	25.2	13	03.6	01	02	01.6	08	01.9	15	01.9	07	01.9	02	31.1	27	02.8	11	01.3	02	01.1	34
VI	900.4	12.7	17.6	12.4	13.8	18.6	08.2	26.1	07	03.4	22	05	01.9	14	02.2	09	01.7	08	01.4	03	01.1	20	03.2	18	02.1	05	01.3	36
VII	903.7	15.9	22.6	15.5	17.4	23.6	10.7	31.4	27	07.4	01	07	02.3	08	02.3	27	01.8	05	01.1	01	01.1	10	02.8	03	02.0	05	01.3	27
VIII	901.5	15.6	23.1	15.7	17.5	24.4	10.4	30.9	23	06.7	04	08	02.5	14	02.5	16	01.5	07	01.1	01	01.1	15	02.7	06	01.6	04	01.1	23
IX	905.7	10.4	19.2	11.0	12.9	20.1	06.6	26.9	19	02.1	15	02	02.6	11	02.6	26	01.8	08	01.1	01	31.1	03	01.7	06	01.6	04	01.6	37
X	906.5	05.0	12.4	05.8	07.2	13.3	02.2	24.8	05	-04.0	27	05	02.7	25	02.6	16	02.3	06	01.1	01	01.1	05	01.9	02	01.1	04	01.7	39
XI	896.1	09.9	05.0	03.7	04.3	07.7	01.3	17.3	12	-08.9	29	02	02.6	18	02.1	17	01.9	09	01.2	03	31.8	23	03.9	07	01.2	03	01.4	40
XII	901.4	02.1	06.4	02.6	03.4	07.8	-00.1	15.5	06	-04.9	23	01	02.0	06	01.7	17	01.6	04	01.1	01	04.0	15	03.0	24	02.0	02	01.1	35
GOD.	899.6	06.3	11.6	06.6	07.8	12.8	02.9	31.4	29.04	-26.8	15.1	37	02.4	134	02.1	234	01.9	76	01.2	20	31.4	183	03.0	135	01.8	40	01.4	236

$\varphi = 43^{\circ}10' N$ $\lambda = 18^{\circ}33' E$ Gr. $\Delta G = +$ 1h 14 min. BR. ST. 138

I	900.2	-06.8	-02.2	-05.3	-04.9	-00.7	-09.6	06.5	24	-34.3	13	11	02.9	39	01.8	09	01.8	13	02.1	06	02.1	05	02.1	01	02.0	04	02.8	38
II	-	-06.7	-00.9	-03.8	-03.8	01.1	-08.4	04.5	10	-18.6	17	31	03.5	18	01.6	03	01.3	06	01.7	04	05.2	04	02.9	06	03.8	11	03.0	39
III	904.9	00.4	06.0	02.7	03.0	07.4	-00.2	13.6	27	-03.5	30	08	01.9	22	01.5	16	01.6	23	01.3	08	32.3	05	01.3	03	02.4	06	01.2	37
IV	904.7	04.3	11.2	06.2	07.0	12.4	02.6	20.0	10	-02.8	30	05	02.8	30	02.7	01	04.0	18	03.0	14	02.3	13	01.6	01	03.0	05	03.0	36
V	905.5	10.5	18.1	12.6	13.4	19.4	07.8	24.7	13	-00.5	01	22	01.5	17	01.7	02	02.0	21	02.0	13	02.1	12	01.5	01	01.1	05	01.5	38
VI	907.8	11.6	18.9	12.6	13.9	20.1	07.8	24.4	07	02.2	25	07	02.8	20	02.0	02	01.7	09	02.4	14	01.8	10	01.8	02	02.4	12	02.9	39
VII	911.0	13.9	24.3	17.0	18.0	25.2	09.7	31.4	27	05.9	08	29	02.7	18	03.0	01	03.0	04	02.0	03	31.8	14	01.9	15	01.9	18	01.8	40
VIII	909.2	12.7	24.3	16.9	17.7	25.7	09.7	31.5	22	04.5	04	11	02.8	11	03.1	01	01.1	07	02.5	04	03.9	16	01.8	12	01.6	24	02.4	37
IX	912.6	08.1	21.5	13.0	13.9	22.4	06.5	28.0	22	00.5	16	20	02.9	22	03.0	04	01.4	06	01.6	02	01.6	06	01.7	12	01.9	17	01.9	40
X	913.5	03.4	14.8	07.7	08.3	15.5	02.4	24.2	04	-04.5	27	22	03.0	23	03.1	03	02.3	10	02.5	04	02.5	06	01.7	11	01.8	11	01.8	41
XI	904.5	02.9	07.3	04.0	04.6	08.5	01.4	15.2	10	-04.2	30	13	02.6	11	02.8	01	01.1	24	02.5	12	03.7	10	02.7	07	01.8	11	01.8	42
XII	909.9	00.0	06.3	01.6	02.4	07.3	-01.7	11.0	04	-08.0	24	09	02.3	13	02.4	.	.	16	02.4	14	03.3	13	01.7	13	01.4	12	01.8	43
GOD.	-	04.5	12.4	07.1	07.8	13.7	02.3	31.5	22.04	-34.3	40.1	179	02.8	244	02.4	43	01.7	157	02.2	100	02.8	122	01.8	82	01.9	136	02.1	38

$\varphi = 43^{\circ}14' N$ $\lambda = 18^{\circ}36' E$ Gr. $\Delta G = +$ 1h 14 min. BR. ST. 139

I	860.8	-07.4	-04.3	-06.0	-06.0	-02.6	-08.8	05.8	24	-19.5	12	13	02.0	08	32.3	16	02.0	06	01.6	09	03.6	18	03.1	08	01.8	04	01.2	39
II	866.6	-07.7	-03.2	-06.2	-05.8	-01.6	-09.7	06.0	03	-18.5	14	04	02.2	09	01.7	17	02.3	14	02.9	04	32.6	16	03.2	17	02.3	03	01.7	40
III	866.1	-00.7	03.1	00.9	01.0	04.1	-01.4	09.4	31	07.6	30	02	02.2	10	01.8	07	01.7	07	02.3	13	02.5	26	03.0	11	02.3	02	01.2	41
IV	866.0	02.9	07.4	04.0	04.6	08.8	01.2	16.2	10	-04.6	30	03	02.1	01	02.2	07	02.2	05	02.1	13	02.6	29	03.7	21	02.7	01	02.3	42
V	868.0	09.9	14.8	10.8	11.6	16.1	07.5	21.6	13	-00.2	01	01	01.1	03	01.6	07	01.6	07	01.7	07	02.7	23	02.9	10	02.7	04	02.8	43
VI	870.1	10.4	15.2	10.7	11.8	16.7	07.5	22.7	07	03.6	18	02	01.6	04	01.9	10	01.7	09	01.8	02	33.0	18	03.0	17	02.5	06	01.8	44
VII	873.6	13.6	20.5	14.7	15.9	21.6	10.8	27.9	27	06.5	04	04	01.8	05	01.8	10	02.5	09	03.0	03	02.0	16	02.5	13	02.2	02	02.1	45
VIII	872.0	13.4	20.4	15.1	16.0	22.3	11.0	27.5	24	05.4	08	06	02.0	06	01.7	13	01.7	11	02.0	06	02.5	19	02.6	20	02.1	08	01.9	46
IX	875.1	08.9	17.5	11.6	12.4	18.5	07.3	23.2	10	02.0	14</																	

